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A Genetic Link Between Transform and Hyper-Extended Margins

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Abstract

The similarity between the geometry of the West African and South American coastlines is among one of the strongest natural observations supporting the plate tectonic paradigm. However, using classical plate tectonic approaches to model these conjugate transform margins results in a high degree of variability in palaeogeographic reconstructions. Using state-of-the-art 3D coupled thermo-mechanical numerical models, we simulate for the first time, crustal deformation at the onset of oceanisation along large offset oblique margins. Our models show that obliquity causes oceanic rift propagation to stall, resulting in an apparent polyphased tectonic evolution, and in some circumstances leads to the formation of hyper-extended margins. As a result, conjugate margins located at the edge of future fracture zones are highly asymmetric from rifting to spreading, with their lengths differing by a factor of 5 to 10, before the the final phase of break-up occurs. Accounting for this discrepancy should ameliorate future palaeogeographic reconstructions.

Keywords: continental rifting, passive margins, polyphasing, palaeogeography, geodynamic modelling

1. Introduction

The conceptual model of a transform margin (Fig. 1) is an adaptation from the kinematic model of a transform plate boundary of Francheteau and Le Pichon (1972). In this model, the interior of the plates are assumed to be rigid, except along diverging boundary segments (dark grey regions in Fig. 1). Even in deforming areas, the direction of transport is everywhere parallel to the relative plate motion. This model was subsequently adopted by marine geologists to understand the dynamics of extremely oblique passive margins (Mascle and Blarez, 1987).

Extending this idea, Basile et al. (1993) recognised that the edge of the divergent and transform

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9 segments display different morphologies and vertical displacement history. They introduced the
10 terms of concave and convex transform divergent segments based on the shape of the of oceanic
11 domain (Fig. 1A). Within the rigid transform margin models, these differences are explained by the
12 interaction of the margin with the ridge during the early stage of drifting (Fig. 1B) which causes
13 a secondary heat pulse and uplift (Rüpke et al., 2010). This process also affects the transform
14 margin between the stages depicted in Fig. 1B and Fig. 1C, and according to the rigid kinematic
15 model, without resulting in any horizontal deformation.

16 Using the transform margin model to reconstruct plates motion is known to fail at large offsets.
17 Attempts to geometrically match conjugate margins typically lead to isolated pockets of oceanic
18 crust along rifted segments (Bullard et al., 1965; Rabinowitz and LaBrecque, 1979; Unternehr
19 et al., 1988), or overlapping regions of continental blocks (Moulin et al., 2009). The failure of the
20 classical model is most frequently explained by pre break-up deformation (Torsvik et al., 2009),
21 or, as suggested by Vink (1982); Turner et al. (2003), by a delay in the break-up along the oblique
22 segment. Both explanations clearly indicate that tectonic plates deviate from the rigid kinematic
23 block theory outlined in Fig. 1.

24 Paleogeographic reconstructions can account for distributed strain, but they require quantita-
25 tive constraints on the rate of deformation, and the obliquity of the structures which accommo-
26 date the strain. Recently, high-resolution two-dimensional dynamic models of break-up have been
27 utilised to better understand the syn-rift deformation and provide constraints for paleogeographic
28 reconstructions (Brune et al., 2014, 2016). Nevertheless, the conclusions drawn from such models
29 need to be demonstrated in oblique rifting context. Modelling oblique setting naturally mandates
30 the usage of three-dimensional dynamic models.

31 To date, two classes of 3D rift models have been considered. The first class have been designed
32 to focus on the localisation of the deformation within large oblique weak zone (Tron and Brun,
33 1991; Mart and Dauteuil, 1999; McClay, 1990; van Wijk, 2005; Brune, 2014; Heine and Brune,
34 2014), whilst the second class focus on the strain localisation within the transfer zone between two
35 en-echelon grabens by using two offset weak zones (Vendeville and Le Calvez, 1995; Gerya, 2010;
36 Allken et al., 2011, 2012, 2013; Liao and Gerya, 2015).

37 Performing dynamic numerical models of large offset (100's km), magma poor, oblique passive
38 margins such as Rio Muni in West Africa (Turner et al., 2003), Alula Fartak in the Gulf of Aden
39 (Leroy et al., 2012), or the Ghana transform margin (Basile et al., 1993), requires three-dimensional

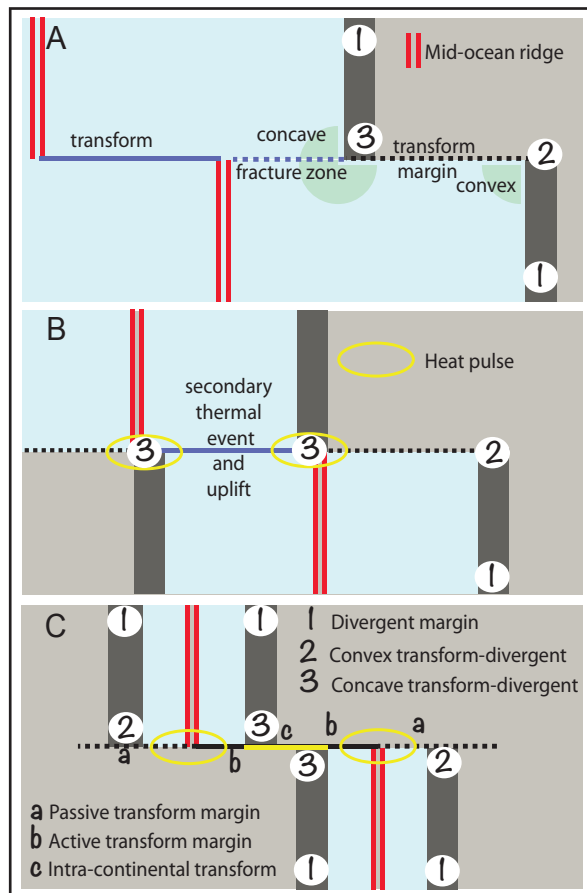


Figure 1: **Illustration of the kinematic model of transform margin formation.** Modified from Francheteau and Le Pichon (1972) and Basile et al. (1993). Light grey represents normal thickness continental crust, dark grey regions represent the thinned continental crust and light blue regions indicate oceanic crust. A) Post rift stage illustrating the location of concave and convex transform divergent margins; B) Latest stage of transform margin activity showing that the mid-ocean ridge interacts thermally with the concave transform margin, long after break-up; C) Formation of the transform margin.

40 experiments which include: full thermo-mechanical coupling, large deformation spanning at least
 41 30 Myr of evolution and sufficiently high spatial resolution to capture accurately the deformation
 42 across a $300 \text{ km} \times 200 \text{ km}$ transfer zone.

43 Due to technical limitations, none of the previous 3D numerical studies could simultaneously
 44 satisfy all of these requirements. Time scales of evolution rarely exceeded 5 Myr (Choi et al., 2008;
 45 Gerya, 2010, 2013; Allken et al., 2011, 2012, 2013), and the offset across the diverging segments
 46 reached, at maximum 50 km, within a model domain (in map view) of $100 \text{ km} \times 100 \text{ km}$ (Choi
 47 et al., 2008; Gerya, 2010, 2013; Allken et al., 2012; Liao and Gerya, 2015). Heine and Brune
 48 (2014) modelled oblique rifting at the scale of the equatorial Atlantic, however their models did
 49 not have sufficient spatial resolution to resolve fault patterns in the crust. In this work, we utilise

50 a newly developed, state-of-the-art massively parallel computational framework for studying 3D
51 lithospheric deformation to surmount all of the aforementioned technical challenges required to
52 simulate models of oblique passive margins.

53 **2. Method**

54 *2.1. Model set-up*

55 The original kinematic model (Masle and Blarez, 1987) supports that transform margins are
56 expected form at bridging rift segments, therefore we adopted the model design which includes
57 two offset weak zones. We consider a lithosphere scale model domain (Fig. 2A) representing
58 $600 \times 150 \times 1200 \text{ km}^3$. Apart from the dimensions of the physical domain, the model configuration is
59 similar to other models designed to simulate strain localisation of oblique transfer zones (Vendeville
60 and Le Calvez, 1995; Gerya, 2010; Allken et al., 2011, 2013, 2012; Liao and Gerya, 2015) and
61 incorporates a minimum amount of complexity.

62 All models consist of an initially horizontally layered hypothetical lithosphere which includes
63 mantle, lower crust and upper crust (Fig. 2A). The Moho is originally located at 40 km depth and
64 the boundary between lower and upper crust is located at 20 km depth. To simulate extensional
65 systems, we impose a normal velocity with magnitude 1 cm/yr, along each face whose normal
66 points in the x direction. This magnitude of velocity is quite standard for modelling continental
67 extension and was previously used by Watremez et al. (2013) to model the opening of the Gulf
68 of Aden, a young example of oblique continental extension. Material leaving the domain across
69 these faces is compensated by a constant infilling normal velocity (2.5 mm/yr) at the base of
70 the models. Both the inflow and outflow boundaries prescribed that the shear stress is zero. Zero
71 normal velocity and shear stress (free slip) are prescribed on the domain faces with normal pointing
72 in the z -direction. The top boundary of the domain is defined to be a free surface (i.e. zero stress).

73 The initial crustal density structure is the same in all the models and corresponds to a density
74 of 2700 kg/m^3 in the upper crust and 2800 kg/m^3 in the lower crust. The initial geotherm we
75 used corresponds to a half-space cooling model after 300 Myr (see Fig. 2C). All three regions
76 employ an approximate Arrhenius type flow law (see Appendix A, Eq. (A.7)). The reference
77 viscosity of the lower crust was varied in order to test whether lithosphere previously involved in
78 orogenic processes reacts differently from a regular (REG) lithosphere. The Post Orogenic (PO)
79 lithosphere assumes that the lower crust constitutes sedimentary material that has previously been

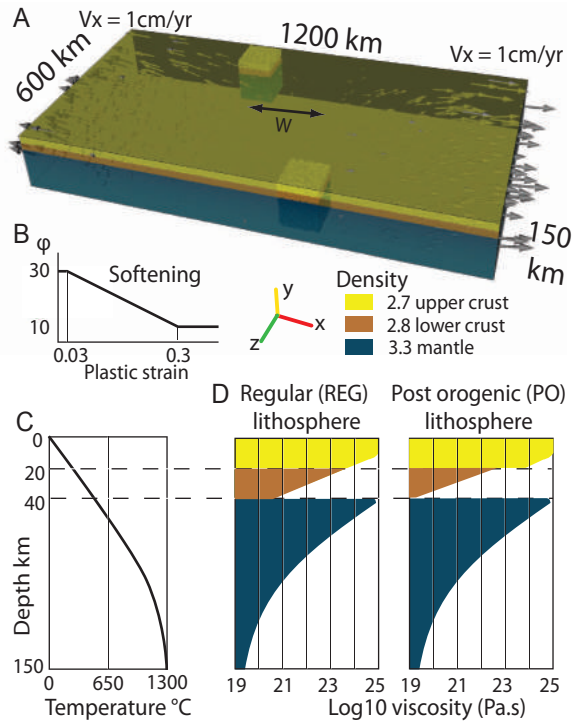


Figure 2: **Model definition.** A) 3D domain with extensional boundary conditions and the outline of pre-existing weak zones offset by a distance W ; B) Rheological softening law in the crust; C) Initial geotherm; D) Viscosity profile for the coupled (REG) and decoupled (PO) lithosphere obtained using the initial geotherm.

80 buried underneath a regular crust (Huet et al., 2011) and therefore possesses a viscosity lower than
 81 that in the regular lower crust. This produces an inverted rheological stratification of the crust
 82 (Fig. 2D). The viscosity profiles obtained for the REG and PO lithosphere models are shown in
 83 Fig. 2D

84 In order to avoid unrealistically high stresses and topography, material strength is limited by
 85 frictional brittle failure with an additional plastic yield strength set to 300 MPa (Watremez et al.,
 86 2013). Localisation is enhanced by frictional softening with strain (Fig. 2B). Softening is enhanced
 87 in the mantle (see Table 1) to approximate the effect of serpentinisation on the brittle behaviour.
 88 Initially, each material point in the domain is assigned a random plastic strain value between 0
 89 and 0.03. In the domain, we impose two weak zones, offset by a distance W , each defining a
 90 $100 \times 120 \times 100 \text{ km}^3$ volume (depicted in Fig. 2A). Within each weak zone, the amplitude of the
 91 initial random plastic strain is ten times larger (i.e. varies between 0 and 0.3) compared with the
 92 initial damage defined throughout the rest of the domain. All parameters are listed in the Table
 93 1.

94 We will first present the results of 8 simulations, examining how: (i) the initial offset W

quantity	name	unit	REG crust	PO crust	mantle
η_0	reference viscosity	Pa s	10^{27}	10^{26}	10^{30}
θ	char. temperature	$^{\circ}\text{C}^{-1}$	2×10^{-2}	2×10^{-2}	1.8×10^{-2}
ϕ_0	friction angle	$^{\circ}$	30	30	30
C_0	cohesion	Pa	2×10^7	2×10^7	2×10^7
τ_{mms}	maximum strength	Pa	2×10^8	2×10^8	3×10^8
ϕ_{∞}	min. friction angle	$^{\circ}$	6	6	6
ε_{∞}^p	softening char. strain	–	0.3	0.3	0.15171
ρ_0	density	kg m^{-3}	$2.7/2.8 \times 10^3$	$2.7/2.8 \times 10^3$	3.3×10^3
α	thermal expansion	$^{\circ}\text{C}^{-1}$	2×10^{-5}	2×10^{-5}	2×10^{-5}
β	compressibility	Pa^{-1}	0	0	3×10^{-12}
κ	thermal diffusivity	$\text{m}^2 \text{s}^{-1}$	10^{-6}	10^{-6}	10^{-6}

Table 1: **Physical properties of the different materials.** Regular (REG) crust is more viscous than Post Orogenic crust (PO). The relationship between parameters listed and the equations solved by the thermo-mechanical numerical model are elaborated upon in Appendix A.

95 between the weak zones (see Fig. 2A); and (ii) the initial mechanical coupling between the crust
96 and lithospheric mantle (REG versus PO in Fig. 2B) influences the linkage between rift segments.
97 Following that, we concentrate on the dynamics of divergent segments which link at moderate to
98 large offset values.

99 2.2. Modelling

100 This study uses pTatin3D (May et al., 2014, 2015) – a highly scalable, massively parallel
101 implementation of the finite element method which employs an Arbitrary Lagrangian Eulerian
102 discretisation, together with the material point method. The equations governing viscous flow (see
103 Appendix A) together with a free surface boundary condition are accurately resolved through the
104 use of high order stable elements (Q_2 - P_1). Material properties and history variables are assigned
105 to material points contained within the computational domain. Material points are allowed to exit
106 (or enter) the model domain according to boundary conditions. Details related to the non-linear
107 solver are provided in Appendix B.

108 Owing to this new generation code, it has become possible to discretise a $600 \times 150 \times 1200 \text{ km}^3$
109 lithosphere domain using $128 \times 32 \times 256$ elements, leading to spatial resolution of 5 km . This
110 discrete system of algebraic equations defines a highly non-linear problem (due to the rheology
111 used) with over 29×10^6 degrees of freedom. Each simulation integrates deformation over a time
112 span of 25 to 35 Myr, which corresponds to ~ 2000 time steps on average.

113 *2.3. Post-processing*

114 In this study, we are interested in the obliquity of tectonic structure with the stretching di-
115 rection. Hence, we have chosen to represent the simulation results primarily in map view. The
116 results are presented in terms of surface elevation, Moho elevation and active fault trends map.
117 As the models have a free surface, the topography is simply the elevation of the nodes located at
118 the surface of the model relative to the upper right corner of each map.

119 The different lithologies are stored on markers in the code and used to compute effective
120 viscosity and density (see Appendix A). In order to reduce the amount of data per stored time step
121 to approximately 500 MBytes (250 GBytes per simulations), we only store the density, viscosity
122 and plastic strain averaged over each element.

123 In order to extract the Moho, we examine all cells with an average density larger than 3200
124 kg/m^3 and extract the cells average y coordinate. For a given column in the $x - z$ plane, the
125 Moho is defined via the maximum of these y coordinates (refer to Fig. 2A for coordinate system
126 used). As the models include neither melt nor, true oceanic crust, we define the ocean-continent
127 boundary by attributing a continental affinity to all surface cells in which densities are lower than
128 3200 kg/m^3 .

129 Faults in these numerical models are shear bands with a finite thickness, typically on the order
130 of one to two elements. Here we split the components of shear that corresponds to vertical direction,
131 i.e. the dip slip component ($\dot{\epsilon}_{xy}$ and $\dot{\epsilon}_{yz}$) from the component of shear in the horizontal direction,
132 i.e. the transform component ($\dot{\epsilon}_{xz}$) and we only visualise the zones where these components are
133 larger than the background strain rate ($5 \times 10^{-16} \text{ s}^{-1}$) as these regions correspond to locations
134 where strain rate has localised.

135 3. Results and discussion

136 3.1. Rift linkage

137 To first order, models with a weak lower crust (PO) display distributed normal faulting with
138 faults trending orthogonal to the direction of stretching while this distributed small wavelength
139 deformation is absent in the strong lower crust models (REG). This contrasting behaviour is
140 predicted by previous 2D numerical models (Huismans and Beaumont, 2007). More surprising is
141 that the propagation of divergent rift segments occurs faster in the decoupled lithosphere (Fig. 3,
142 see PO models at 10 Myr), compared to the coupled lithosphere model (Fig. 3, see REG models
143 at 10 Myr).

144 The final outcome of the models considered fall into one of four cases outlined by the different
145 colours of the small insets panels in Fig. 3. At small (100 km) and extremely large initial offset
146 (400 km), the rheology of the lower crust does not greatly influence the results within the first
147 25 Myr of evolution. With an offset of 100 km, oblique margins form rapidly, followed by oblique
148 spreading. For offsets of 400 km, propagating rifts do not interact mechanically.

149 Obliquity is quantified as the angle between the strike and the stretching direction, a low angle
150 therefore corresponds to a high obliquity. For moderate to large initial offsets, the rheology controls
151 the transition from an oblique margin (45°), to an extremely oblique margin ($< 30^\circ$), and a failed
152 oblique rift (Fig. 3). For an offset of 200 km, the obliquity of the transfer zone is higher when
153 using a PO lithosphere, compared to when using a REG lithosphere. The maximum offset between
154 two linking weak zones increases with the strength of the lithosphere (compare the models with
155 300 km offset in Fig. 3).

156 Examining the snapshots of the models at 25 Myr (Fig. 3), it is clear that, the larger the
157 offset, the longer it takes to localise the deformation on the oblique segment. As a result, the delay
158 between the break-up on the propagating divergent rift segment, measured as the first break-up
159 time in the pre-existing weak zones and the final oblique break-up, increases from 6 Myr for 100
160 km offset to 25 Myr for a 300 km initial offset (see supplementary movies of the experiments).
161 During this period, mid-ocean ridge propagation is stalled, but distributed continental extension
162 accommodates the divergence at the tip of the ridge.

163 The models in which early faults (those active at 10 Myr in Fig. 3) strike perpendicular to the
164 stretching direction result in a larger final obliquity than models which develop early structures
165 that are oblique to the stretching direction. In all the models, the orientation and existence of

166 early structures (those active at 10 Myr in Fig. 3) is controlled by the rheology of the lower crust,
 167 and, to a lesser extent, by the initial offset. This led us to speculate that, in nature, pre-existing
 168 structures reactivated during the early stages of rifting (Bellahsen et al., 2006) could possibly

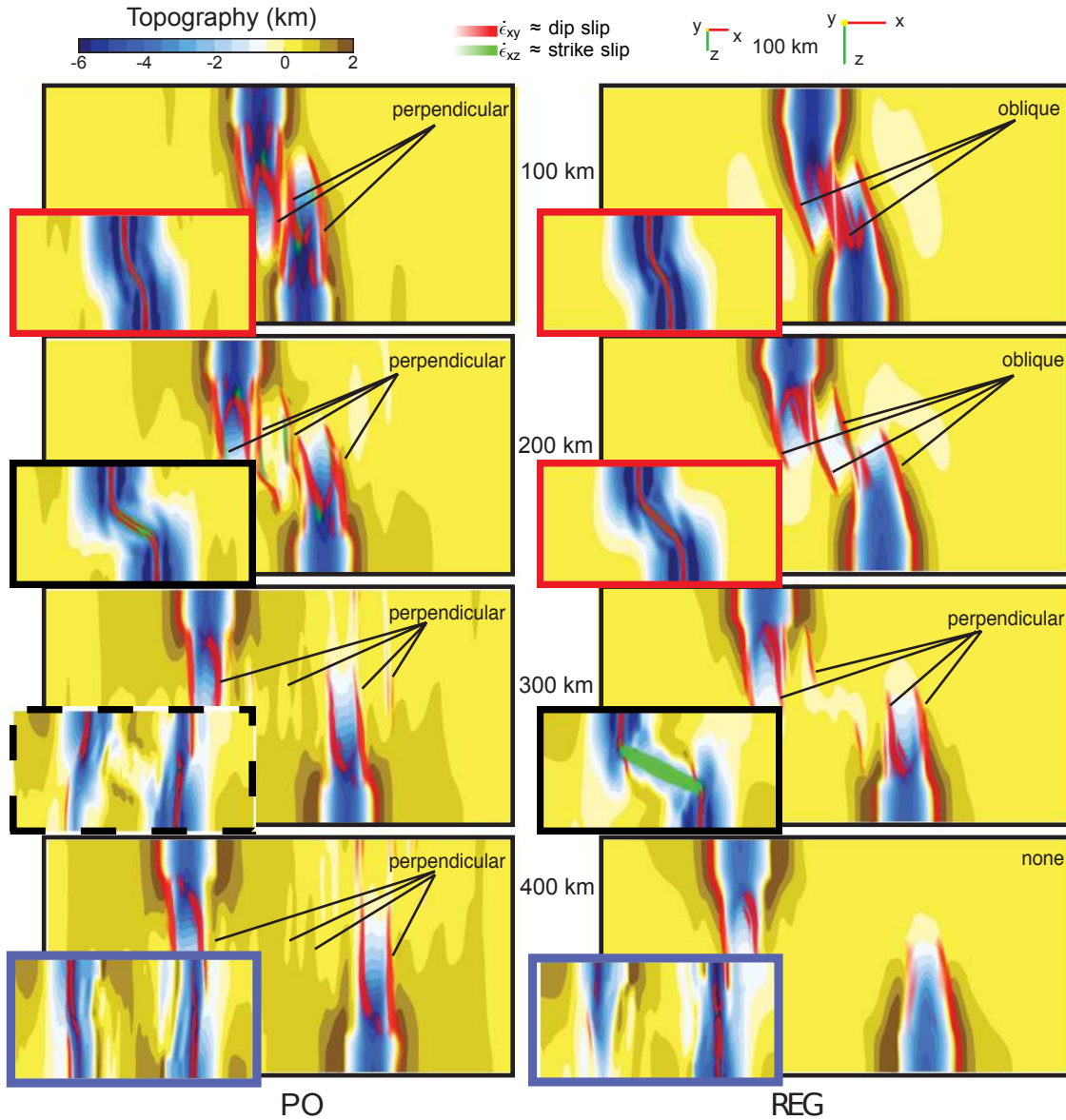


Figure 3: **Results of the parametric study.** Map view of the topography of all the models after 10 Myr (large insets) and 25 Myr (small insets) with major active faults outlined as shade of red (dip slip kinematics) and green (strike slip kinematic). At 10 Myr, distributed small wave length faults striking perpendicular to the direction of stretching forms in the post orogenic models (Left) while large oblique normal faults forms in the regular crust models (Right). At 25 Myr, coloured boxes indicate models with oblique margins (45° , red), with extremely oblique margins ($< 30^\circ$, black), abandoned transfer zone (dashed) and in which segments did not link at all (blue). Supplementary movies are provided for experiments REG-100 km, REG-300 km and PO-100 km, PO-300 km using the same colour scales as this figure.

169 influence the final obliquity of the margin.

170 *3.2. Initial weak zones spacing and linkage*

171 Previous studies with no thermal coupling have reported that linkage does not occur when
172 notch spacing exceeds the thickness of the brittle layer (Vendeville and Le Calvez, 1995; Allken
173 et al., 2012). At lithospheric scale, this limit would correspond to $W \leq 100$ km. In our models
174 which account for thermal coupling, the linkage between divergent segments is obtained for much
175 larger offsets, upto 3–4 times the thickness of the brittle layer.

176 In analogue models, the interactions between grabens has been found to be less efficient when
177 the weak zones overlap, but no significant differences were observed between models with non-
178 overlapping weak zones and models with underlapping weak zones (Le Calvez and Vendeville,
179 2002). Using dynamic numerical models to study these geometrical effects in more details, Allken
180 et al. (2013) showed that a larger amount of underlap favours linkage because more diffuse strain
181 can occur in the transfer zone before the imposed rift segment propagates. In a previous study,
182 Allken et al. (2012) showed that linkage occurs with a larger offset if a weak and thick ductile
183 layer is present at the base of the crust. With our lithospheric scale models, we find that it is
184 easier to link lithospheric scale rift segment when the lower crust is resistant. This is somewhat
185 contradictory to Allken et al. (2012) conclusions. Yet, we note that their models neglected the
186 strain localisation in the lithospheric mantle and were devoid of any thermo-mechanical coupling.
187 The two studies can be reconciled by recognising that at the scale of our models, the weak lower
188 crust of Allken et al. (2012) corresponds to our weak asthenosphere. The final strain rate and
189 linkage pattern of our models actually always occurred within the low viscosity lower crust class
190 defined in Allken et al. (2012), independently of the viscosity of the lower crust. We now focus on
191 the dynamics of models in which linkage occur at large off-set in our parametric study.

192 *3.3. Dynamics of large offset break-up*

193 Before oblique localisation occurs (Fig. 4A), the two divergent segments are always separated
194 by *en-echelon* deep intra-continental basins as clearly indicated by the topography. Depending
195 on the dynamics of break-up, oblique or extremely oblique, their thermal and tectonic histories
196 are different. The vertical loads associated with the presence of hot asthenospheric mantle and
197 lateral variation in crustal thickness result in the flexural bending of plates. Where crustal thinning

198 does not coincide with lithospheric mantle thinning, a topographic ridge forms at the moment of
 199 break-up.

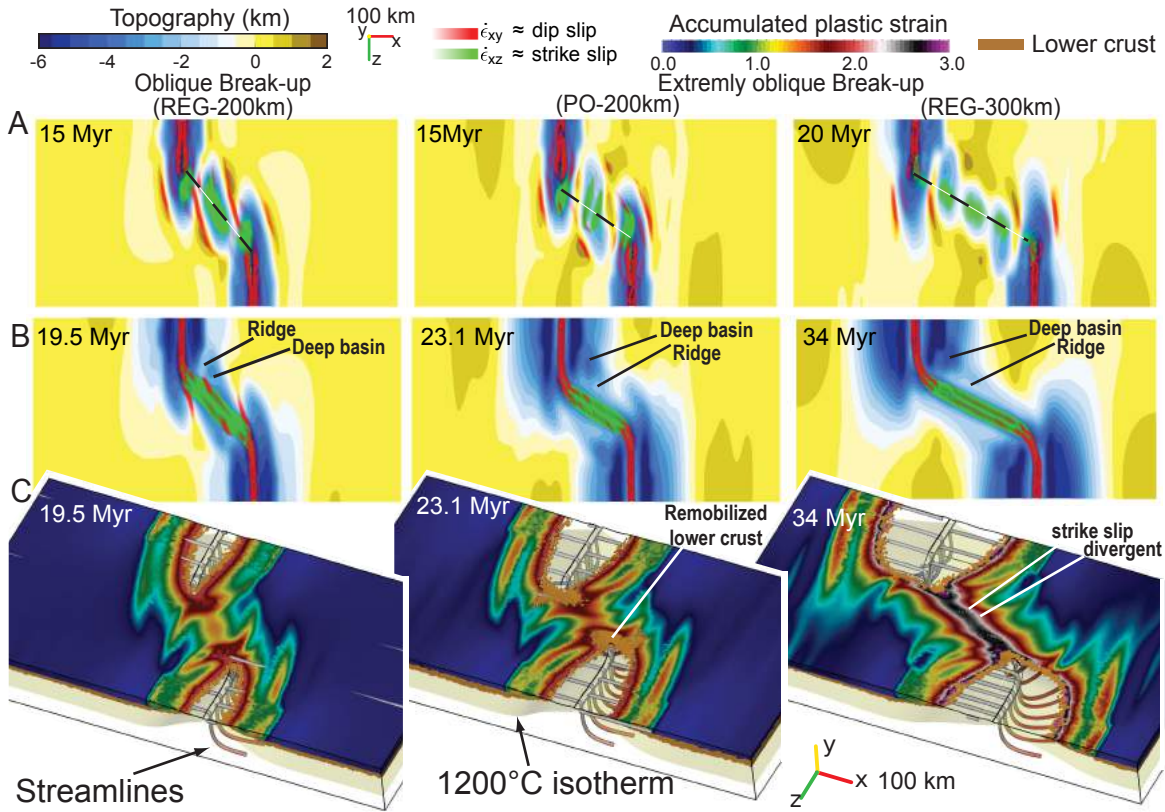


Figure 4: Map view of the topography with major active faults outlined via a shade of red (dip-slip kinematics) and green (strike slip kinematic). Timing corresponds to A) onset of strike slip strain localisation in the transfer zone and B) incipient break-up. C) Accumulated plastic strain (main faults) in the upper crust. The oceanic lithosphere has been removed to outline the ocean-continent boundary and to highlight the asymmetry in asthenospheric flow line feeding the mid-oceanic ridges. Exhumed lower crustal material is shown in brown.

200 For the model which results in oblique break-up (REG-200 km) in Fig. 4, the latest stage of
 201 oblique localisation occurs within the center of the early oblique basin. Looking at the accumulated
 202 plastic strain as a proxy for major fault orientation, one observes that the oblique break-up does
 203 not cut across any pre-existing structures with a different orientation. The rotation of the active
 204 structure with time (Fig. 4A,B and supplementary movie REG-200km) shows that the early struc-
 205 tures rotated continuously between the two diverging segments to reach their final orientations.
 206 As a result, the remnants of the early deep basins forms an oblique margin which is separated from
 207 the divergent segment by topographic ridges which are orthogonal to the direction of extension.

208 In models which result in extremely oblique break-up (PO-200 km and REG-300 km) in Fig.
 209 4, strike slip localisation occurs along a strike slip structure, which cross-cut the initial en-echelon

210 basins (Fig. 4B). The supplementary movies (PO-200km and REG-300km) clearly indicate, this
211 structure did not form by continuous rotation of the earlier structures. At the onset of localization
212 in the mantle, no oblique structures are visible at the surface (Fig. 4A), yet small portion of the
213 early basins deforms with strike slip kinematics. These local spots of green shades outline the
214 direction of the still deep seated mantle necking structure which will reach the surface at the stage
215 depicted on Fig. 4B.

216 The accumulated plastic strain (Fig. 4C) show that extremely oblique break-up segments cut
217 across the early rift structures. For the REG-300 km model, the shade of white in the plastic strain
218 highlights the orientation of the structures during break-up and indicates that break up occurs
219 on pure transform segments separated by divergent segments. As crustal thinning, inherited from
220 the earlier phase, is not parallel to lithospheric thinning, a topographic ridge forms parallel to the
221 oblique margins.

222 The delay between the divergent margin break-up and the onset of oblique break-up causes the
223 formation of a large oceanic domain prior to complete break-up. They are displayed as transparent
224 on Fig. 4C. Their size increases with increasing initial offset and decreasing lower crustal strength.

225 All the models show that these oceanic domains are unevenly distributed across the mid-
226 oceanic ridge and that the asthenospheric flow feeding these ridges is also asymmetric (Fig. 4C).
227 This suggests that early spreading is not purely divergent in the model. The magnetic anomalies
228 from the Gulf of Aden (Fig. 5A) and West Africa (Fig. 5B) show the presence of oblique stripes,
229 and ductile shear indicators such as S-C structures, in good agreement with the prediction of our
230 models.

231 For strong lower crustal rheology (REG-models, Fig. 4C) the asymmetric spreading occur in
232 the oceanic domain. For weak lower crustal rheology (PO-model, Fig. 4C), the lower crust is re-
233 mobilized and spreads to accommodate the asymmetry. This suggest that the rheology of the lower
234 crust controls whether re-mobilized crustal material (Ranero and Pérez-Gussinyé, 2010; Unternehr
235 et al., 2010), or exhumed mantle material (Pérez-Gussinyé et al., 2001), accommodates the latest
236 stage of deformation.

237 The Moho is very shallow at the tip of the oceanic domain (Fig. 6A), highlighting a large
238 amount of continental extension. The 3D models show that large initial offset causes an asymmetry
239 in extension and the formation of hyper-extended margins. However, these hyper-extended basins
240 only mark the tip of *en-echelon* diverging rift segments which have stalled during the long-lasting

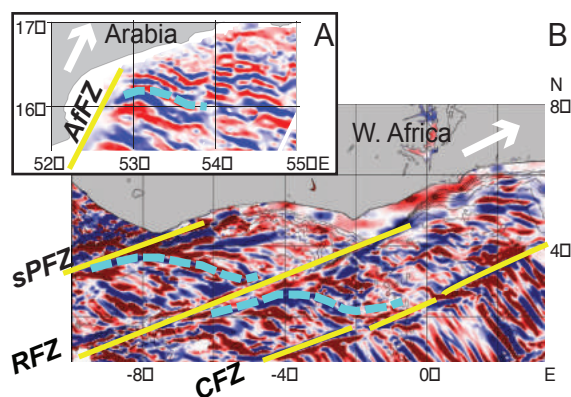


Figure 5: Map view of the gradient of magnetic field. A) In the Gulf of Aden at the Corner of Alula Fartak fracture zone (AfFZ) (Leroy et al., 2010). B) Along the West African margin (Maus et al., 2009) nearby the Saint Paul Fracture Zone (sPFZ), the Romanche Fracture Zone (RFZ) and the Chain Fracture Zone (CFZ). In both cases that the magnetic anomalies (dashed cyan line) are not perpendicular to the direction of spreading (white arrow), nor to the fracture zone (yellow line) close to the transform margin.

241 strain localisation along the oblique segments. They do not indicate the direction of propagation
 242 of oceanisation as suggested in the Gulf of Aden (Manighetti et al., 1997).

243 3.4. A new model for transform margins

244 Fig. 6A highlights the coastlines (cyan lines) from the conjugate convex (3) and concave (2)
 245 transform divergent margins produced by model REG-300 km at the end of continental break-up.
 246 The coastlines are of very different length. The concave margin is only a few tens of kilometers
 247 long, whilst its convex conjugate can be as long as 200 km. Fig. 6B represents a hypothetical
 248 passive margin that would result from model REG-300 km. Combining the ~ 250 km of the
 249 oblique segment (yellow line) and the 200 km segment of the convex margin, the coastline which
 250 trends extremely oblique to the direction of stretching, reaches a length of ~ 450 km. This is
 251 comparable in length to the transform margins in the equatorial Atlantic (Fig. 5B).

252 Due to the anti-symmetric extension occurring on the opposite segment, a coastline of similar
 253 length exists on the right block. However, trying to reassemble the left and right blocks using
 254 the rigid transform margin model (Fig. 6C) shifts the location of the early deep basins, while our
 255 models indicate these features were aligned during the 15 to 25 Myr of extension that preceded
 256 oblique break-up (Figs. 4 and 6A).

257 In order to perform the reconstruction correctly, the initial conditions, the pre-rift and the early
 258 normal faults located on the transform segment must be used to restore the onset of break-up stage
 259 which is displayed in Fig. 6A.

260 This should leave behind large remnants of divergent oceanic domain, exhumed lower crustal
 261 domain and hyper-extended margins, which can be overlapped based on the magnetic anomaly
 262 of the purely divergent segments. From the results of our numerical models, a good proxy for
 263 the timing of the final break-up is the formation of the marginal ridge which cross-cut the early
 264 basins. The flexural uplift should be marked by an unconformity between the syn-rift and post-rift
 265 sediments in the deep basins located at its back.

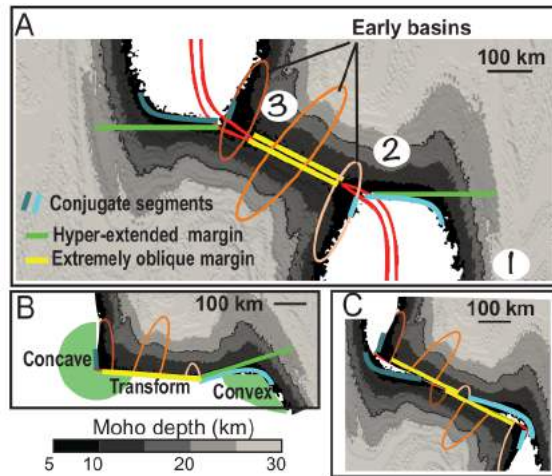


Figure 6: A) Map view of the Moho depth for the REG model with a 300 km offset with the main structures; 1, 2 and 3 indicate respectively the divergent, convex and concave transform divergent margins; B) Representation of the anticipated passive margin, long time after continental rifting with annotations corresponding to the original model represented on Fig. 1A; C) Schematic reconstruction using the rigid plate kinematic model and showing the misfit of the early rift structures if one does not first reconstruct the break-up stage displayed in A)

266 The deep basins formed in the early stage of rifting present a good potential for hydrocarbons
 267 because they were tectonically isolated from the well oxygenated water that fills the basins forming
 268 along the pre-imposed divergent segments. However, this potential also depends on the dynamics
 269 of the break-up, i.e. oblique or extremely oblique. In the first case, they rotate to align with the
 270 oblique mid-oceanic ridge. In the second case, some of these basins are preserved in the intrado
 271 of the topographic ridge, protecting them from heat and promoting very early migration. As a
 272 result, the concave transform divergent margin (zone 3 in Fig. 1 and 6A) is constituted by deep,
 273 potentially hydrocarbon rich, basins formed in the early stages of rifting which are absent from
 274 the convex divergent margins.

275 **4. Conclusions**

276 Using modern, state-of-the-art, high performance computing tools has allowed us to simulate
277 dynamic, 3D lithospheric scale oblique rifting scenarios with the necessary spatial resolution. Our
278 results show that simple set-up with cylindrical and constant boundary conditions produce a
279 level of complexity in term of asymmetry and poly-phasing of deformation that could only be
280 obtained with more complex model configurations or boundary conditions in 2D (Brune et al.,
281 2014; Huisman and Beaumont, 2011, 2007).

282 Our models predict that the break-up of extremely oblique segments occurs 10 to 25 Myr after
283 the break-up of the divergent segments. During this period, stalling normal rift propagation leads
284 to the formation of deep anoxic basins, along with micro continental ribbons which form patterns
285 similar to those observed in northern Atlantic profiles (Péron-Pinvidic and Manatschal, 2010) and
286 in Angola-like hyper-extended margins (Unternehr et al., 2010).

287 Natural fracture zones and transform margins are not defined by line segments, but rather a
288 100 km diffuse zone of deformation (Fig. 5) where significant asymmetry can be accommodated by
289 exhumation of lower crustal material, and/or asymmetry of the spreading. These deformation zones
290 record the temporal history of several phases of deformation occurring prior to oblique break-up.
291 Consequently, attempting to reconstruct plate motions with rigid plate transform margin model
292 is impossible. Our new high resolution 3D dynamic models can help predict where, and when,
293 significant amounts of stretching and wrenching are expected to occur. Such results will help to
294 further improve the reliability and accuracy of future paleogeographic reconstructions.

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300 **Appendix A. Governing Equations**

301 The mechanical component of pTatin3D solves the conservation of momentum for incompress-
302 ible, highly non-linear viscous fluids. The conservation of momentum for such a fluid is given

303 by

$$\left[2\eta \dot{\epsilon}_{ij}(\mathbf{u})\right]_{,j} - p_{,i} = f_i, \quad (\text{A.1})$$

304 where \mathbf{u}, p are the fluid velocity and pressure, η is the shear viscosity, f_i is the body force and the
305 strain rate operator $\dot{\epsilon}_{ij}$ is given by

$$\dot{\epsilon}_{ij}(\mathbf{u}) := \frac{1}{2} (u_{i,j} + u_{j,i}). \quad (\text{A.2})$$

306 The total stress σ_{ij} is given by

$$\sigma_{ij} = \tau_{ij} - \delta_{ij}p, \quad \text{where } \tau_{ij} = 2\eta \dot{\epsilon}_{ij}. \quad (\text{A.3})$$

307 Simplified mass conservation is achieved through assuming incompressibility

$$u_{k,k} = 0. \quad (\text{A.4})$$

308 The forcing term in the momentum equation reflects changes in buoyancy associated with thermal
309 contraction/expansion (Boussinesq approximation), or compositional variations between different
310 rock types following

$$\mathbf{f} = \rho_0(1 - \alpha(T - T_0) + \beta(p - p_0))\hat{\mathbf{g}}, \quad (\text{A.5})$$

311 where ρ_0 is the compositional density of the rock as measured at the reference temperature T_0 and
312 pressure p_0 , $\hat{\mathbf{g}}$ is the gravity vector, α, β are the coefficients of thermal expansion and adiabatic
313 compressibility respectively and T is the temperature. The evolution of temperature is given by
314 the following conservation equation

$$\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T = \frac{\partial}{\partial x_i} \left(\kappa \frac{\partial T}{\partial x_i} \right), \quad (\text{A.6})$$

315 where $\kappa = k/(\rho C_p)$ is the thermal diffusivity.

316 Thermally activated creep mechanisms defining the viscous strength of rock, η' are approxi-
317 mated by the Frank-Kamenetskii flow rule

$$\eta' = \eta_0 \exp(-\theta T), \quad (\text{A.7})$$

318 where the parameters η_0, θ account for the local chemical composition of the rock. These coefficients
319 are also carried by the markers. Pressure and strain rate dependence are introduced by limiting
320 the effective viscosity so that stresses in the model do not exceed the Drucker-Prager yield stress

$$\tau_y = \min [p \sin \phi(\epsilon^p) + C_0 \cos \phi(\epsilon^p), \tau_{\text{mms}}], \quad (\text{A.8})$$

321 which is limited a maximum Mises stress, τ_{mms} . The cohesion C_0 is regarded to be constant,
 322 however the internal friction angle ϕ is assumed to decrease as a function of the accumulated
 323 plastic strain ϵ^p according to

$$\phi(\epsilon^p) = \max\left(\phi_\infty, \phi_0 - \frac{\epsilon^p(\phi_0 - \phi_\infty)}{\epsilon_\infty^p}\right). \quad (\text{A.9})$$

324 Eq. (A.9) defines an empirical softening relation which reduces the friction angle linearly with
 325 accumulated plastic strain. Here ϕ_0 defines the initial friction angle. ϵ_∞^p represents the measure
 326 of plastic strain after which complete softening is achieved and internal friction angle reaches ϕ_∞ .
 327 Plastic strain represents an integrated, tensorial invariant measure of the deformation which has
 328 occurred due to plastic yielding. Thus, the quantity ϵ^p can be regarded as a simplified measure of
 329 material damage. The evolution of plastic strain is given by;

$$\frac{D\epsilon^p}{Dt} = \begin{cases} \dot{\epsilon}_{II}, & \text{if } \eta' > \tau_y/2 \dot{\epsilon}_{II} \\ 0, & \text{otherwise} \end{cases}, \quad (\text{A.10})$$

330 where $\dot{\epsilon}_{II} = \frac{1}{2} \sqrt{\dot{\epsilon}_{ij} \dot{\epsilon}_{ij}}$. The effective viscosity η is computed on markers and account for both the
 331 parametrised creeping of viscous rocks and brittle behaviour following

$$\eta = \min\left[\eta', \frac{\tau_y}{2 \dot{\epsilon}_{II}}\right]. \quad (\text{A.11})$$

332 Appendix B. Numerical Aspects

333 pTatin3D employs an inf-sup stable mixed Finite Element method with an Arbitrary La-
 334 grangian Eulerian description to solve the discrete incompressible Stokes problem given by Eqs. (A.1)
 335 and (A.4). The velocity field is discretised via a Q_2 (tri-quadratic) basis, whilst the pressure field
 336 is discretised via a P_1^{disc} (piece-wise linear) basis which is discontinuous across element boundaries.

337 The material-point-method is used to discretise different material regions. In the material-
 338 point-method, Lagrangian particles are introduced within each finite element. The particles are
 339 advected with the velocity computed from the solution of the discrete Stokes problem. Each
 340 particle stores an indexing used to identify to which material region it belongs to. This index is
 341 used to determine the value of the rheological constants and coefficients related to Boussinesq.
 342 The particles are also used to store the plastic strain ϵ^p .

343 At each material point we evaluate the viscous flow-law and the Drucker-Prager yield stress.
 344 The effective viscosity (see Eq. (A.11)) is also evaluated at each material point. We define an

345 average viscosity over each Q_2 element using the harmonic average of the effective viscosity asso-
346 ciated with all material points contained in a given element. The element density is computed in
347 a similar manner, but use the arithmetic average of marker densities.

348 We apply the Flexible-GMRES (Saad, 1993) Krylov method to solve Eq. (A.1). The system
349 is right preconditioned using an upper block triangular preconditioner (Elman et al., 2005). The
350 viscous block is preconditioned using a hybrid geometric multigrid implementation (May et al.,
351 2015).

352 The temperature T in Eq. (A.6) is discretised using Q_1 finite elements which overlap the Q_2
353 velocity space. The advection-diffusion equation is stabilized via SUPG (Brooks and Hughes,
354 1982). The Stokes problem and energy equation are solved in a de-coupled manner, thus the
355 temperature dependence in the rheology (Eq. (A.7)) and forcing function (Eq. (A.5)) does not
356 introduce an additional non-linearity.

357 Support for all parallel linear algebra, in the form of matrices, vectors, preconditioners, Krylov
358 methods and nonlinear solvers is provided by PETSc (Balay et al., 2013b,a). Parallelism is achieved
359 by spatially decomposing the structured finite element (FE) mesh containing $M \times N \times P$ elements,
360 into structured sub-domains containing $m \times n \times p$ elements. The underlying mesh data structure
361 we uses is defined by DMDA object provided by PETSc.

362 The simulation results were performed using 512 cores an SGI ICE 8200 with compute nodes
363 consisting of 2×6 Intel Xeon (Series 5600) cores running at 2.8 GHz. Each model required ap-
364 proximately 2000 time steps summing to approximately 2 days of computation time for a mesh
365 resolution of $256 \times 32 \times 128$ Q_2 elements. The multigrid preconditioner was configured with three
366 levels, from the coarsest to the finest level: $32 \times 16 \times 16$, $128 \times 32 \times 64$, $256 \times 32 \times 128$. We
367 used conjugate gradient and incomplete LU as the coarse grid solver. The coarse grid solver was
368 terminated after 25 iterations, or if the initial residual was reduced by a factor of 10^4 . The non
369 linear solver uses picard iterations with $\text{rtol } 10^{-2}$ or $\text{atol } 10^{-4}$.

370 pTatin3D (May et al., 2014, 2015) is an open source code copyrighted under GNU General Pub-
371 lic License v.3 and may be accessed ¹ at <https://bitbucket.org/jedbrown/ptatin3d>. pTatin3D heav-
372 ily leverages functionality from PETSc, which can be freely downloaded at <http://www.mcs.anl.gov/petsc>.
373 Input files are available upon request from the corresponding author.

374 References

¹upon request during review process, when the paper gets accepted the code will be accessible with no restrictions

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