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Suppressing structural colors of photocatalytic optical coatings on glass: the critical role of SiO₂

Ronghua Li¹, Mickael Boudot^{1,2}, Cédric Boissière¹, David Grosso³, Marco Faustini^{1}*

¹ Sorbonne Universités, UPMC Univ Paris 06, CNRS, Collège de France, UMR 7574, Chimie de la Matière Condensée de Paris, F-75005, Paris, France.

² Institute for Materials Chemistry and Engineering, Kyushu University, 6-1 Kasuga-Koen, Kasuga, Fukuoka 816-8580, Japan.

³ IM2NP, Faculté des Sciences et Techniques, Campus de Saint Jérôme, Avenue Escadrille Normandie Niemen, 13397 Marseille, France

KEYWORDS

Interference, structural color, photocatalytic, optical coatings, mesoporous

ABSTRACT

The appearance of structural colors on coated-glass is a critical esthetical drawback toward industrialization of photocatalytic coatings on windows for architecture or automobile. Herein we describe a rational approach to suppress the structural color of mesoporous TiO₂-based coatings preserving photoactivity and mechanical stiffness. Addition of SiO₂ as third component is discussed. Ti_xSi_(1-x)O₂ mesoporous coatings were fabricated by one-step liquid deposition process through the evaporation induced self-assembling and characterized by GI-SAXS, GI-WAXS, electron microscopies and in-situ Environmental Ellipsometry Porosimetry. Guided by optical simulation, we investigated the critical role of SiO₂ on the optical responses of the films but also on the structural, mechanical and photocatalytic properties, important requirements to go toward real applications. We demonstrate that, adding SiO₂ to porous TiO₂ allows tuning and suppression of structural colors through refractive index matching and up to 160% increase in mechanical stiffening of the films. This study leads us to demonstrate an example of “invisible” coating, in which the light reflection is angle- and thickness- independent, and exhibiting high porosity, mechanical stiffness and photoactivity.

1. INTRODUCTION

Glass is an outstanding material, massively employed in everyday life such as in optical devices, architecture, automobile and arts.¹ In addition to its transparency and insulating properties it is mainly appreciated to be chemically inert. However, additional functionalities can be integrated in standard glasses by applying optical coatings. Among them, photocatalytic coatings allow the glass surface to be “reactive”, enabling decomposition of organic species under light irradiation.² Two main properties have been targeted: (i) self-cleaning capabilities, allowing decomposition of non-volatile organic species from the surface (dirt, contaminations)³ that affect the glass appearance; (ii) air depollution of volatile organic compounds especially in the case of odorous and harmful molecules.⁴⁻⁶ Among the requirements demanded to be applied on glass, this “reactive” coating must be highly photoactive with high surface area, non-light absorbing and non-light scattering light in the visible range and must exhibit good mechanical, chemical and thermal stability. In such domain, TiO₂ based mesoporous coatings have been considered as most serious candidates.⁷⁻⁸ Optical quality nanocrystalline TiO₂ mesoporous films can be obtained by sol-gel process in presence of templating agents⁹⁻¹⁰ and can be easily applied by liquid deposition techniques on large surfaces making this material appealing for industrial production.¹¹

Despite the fact that massive research was conducted in the field of porous photocatalytic films, the lab-to-market transition is still hindered.¹²⁻¹³ One of the main reasons is related to the esthetical appearance of the coated-glass. Indeed, when the refractive index dispersion of the coating differs from that of glass substrate, structural colors are observed due interference phenomena taking place at air/coating/glass interfaces.¹⁴⁻¹⁵ Coatings having homogenous thickness produce an angle-dependent shade that is not suitable for design conception in many applications especially for architectural windows or automobile windshields. This (un) esthetical effect is even more problematic when the coating’s thickness is not homogenous over the surface. In fact, thickness fluctuations result in color fluctuation visible at naked eye.¹⁶

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5 Thickness fluctuations can be produced during the film deposition due to not controlled process
6 conditions, dust or to edge effects;¹⁷ thickness inhomogeneity can also appear within time due to
7 damaging of the films by delamination, dissolution or scratching. There is thus a strong need for
8 the development of high surface area, photoactive films exhibiting “invisibility” on glass. The
9 most straightforward way to suppress the structural colors consists in applying coatings that
10 match the refractive index of glass all over the visible range of wavelengths. Due to the intrinsic
11 high refractive index of TiO₂ (n = 2.2- 2.5 in the visible range) as compared to commercial glass
12 (n ≈ 1.5 in the visible range), one option to approach the refractive index matching would
13 consist in increase the porosity %vol of TiO₂ coatings up to 60%; however this solution would
14 lead to mechanically fragile films. Alternatively, a low refractive index material, such as silica,
15 can be added in the network. Nanocomposite SiO₂-TiO₂ mesoporous coatings have been already
16 proposed in the literature mainly to target anti-reflectivity and photocatalytic capabilities;¹⁸⁻¹⁹
17 however even anti-reflective interferential coatings always exhibit angle-dependent structural
18 colors. In addition, compared to anti-reflection, the conditions required for “invisibility” are
19 stricter since the refractive index dispersion law should precisely match the one of glass in all
20 the range of wavelengths. The development of such invisible coatings is challenging since
21 addition of silica induces not only a decrease of refractive index (to reach invisibility) but also a
22 modification of the structural, mechanical and photocatalytic properties of the porous layers,
23 important requirements to go toward real applications.
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44 In this work, we report a rational approach to design mesoporous photoactive, invisible coatings
45 and we discuss the critical role of SiO₂ on the structural, optical and photocatalytic properties of
46 the films. Starting from the experimental refractive index dispersion law, the formation and the
47 suppression of the reflected structural colors could be systematically predicted by using
48 simulation. Guided by these results, photocatalytic TiO₂-SiO₂ mesoporous coatings were
49 fabricated by a one-step liquid deposition process using the evaporation induced self-assembly
50 method, using F127 block copolymer as an organic template mixed with various TiO₂ and SiO₂
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5 molecular precursors' ratios in ethanolic solution. We experimentally confirmed that such
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7 composite mesoporous coatings perform as colored antireflective and reflective coatings and
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9 only a precise combination of the three phases (TiO₂, SiO₂ and air) allows obtaining invisibility,
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11 improved mechanical stiffness and high photocatalytic activity. Importantly, we highlight the
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13 critical role of silica on the final porous structure, stiffness and photocatalytic performances of
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15 the films as characterized by GI-SAXS, GI-WAXS, SEM-FEG, TEM and in situ Environmental
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17 Ellipsometry Porosimetry (EEP).
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20 21 **2. Experimental details**

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25 *Chemical Solutions.* Absolute ethanol (EtOH) was purchased from Normapur while TEOS
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27 (tetraethylorthosilicate), TiCl₄ (titanium IV chloride), hydrochloride acid (2M HCl), F127
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29 Pluronic (EO₁₀₆PO₇₀EO₁₀₆) were purchased from Aldrich. All products were used as received.
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31 TiO₂-SiO₂ composite mesoporous thin films were prepared from solutions composed of
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33 TiCl₄/TEOS/F127/EtOH/H₂O with respective molar ratios of 1-x/x/0.006/30/10 with 0 ≤ x ≤
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35 0.98. Pure silica mesoporous films solutions were prepared from solutions composed of
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37 TEOS/F127/EtOH/H₂O/HCl with respective molar ratios of 1/0.006/40/5/0.005. Solutions were
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39 obtained by dissolving the inorganic precursors in ethanol and water followed by addition of
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41 F127. In case of mesoporous pure silica films, 2M HCl was added to hydro-alcoholic phase to
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43 ensure the hydrolysis of the precursor.²⁰⁻²¹
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48 *Films Processing.* The oxide films were prepared by dip coating, using an *Acedip* dip coater,
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50 onto silicon wafer or glass at room temperature (≈ 22°C), at low relative humidity (RH < 2%)
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52 and at a typical withdrawal speed of 3 mm.s⁻¹.²² As-prepared composite films were then aged in
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54 humid atmosphere (RH = 75%, 37°C) for 10 min. After the aging, TiO₂-SiO₂ and pure silica
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5 films were calcined for 10 min underneath a curing IR lamp at 600°C on silicon substrates and
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7 glass substrates whatever the chemical composition of thin films.
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11 *Characterization.* For grazing incidence small-angle X-ray scattering (GI-SAXS), a Rigaku S-
12 max 3000 apparatus equipped with a microfocus source $\lambda = 0.154$ nm and a 2D Gabriel type
13 detector placed at 1480 mm from the sample was used. The angle of incidence was 0.2°.
14
15 Diffraction patterns were interpreted using Igor software 13. Wide-angle X-ray scattering (GI-
16 WAXS) used the same setup as for GI-SAXS except that diagrams were obtained by radial
17 integration of the signal obtained on an image plate placed at 5 cm from the sample center.
18
19 Microscope images showing the film structure were collected using a field-emission gun
20 scanning electron microscopy (SEM-FEG) Hitachi SU7000 instrument. Ellipsometry
21 measurements were performed on a UV-visible (from 245.5 to 998.86 nm) variable angle
22 spectroscopic ellipsometer (VASE-2000U Woolam). The data analyses and optical simulations
23 were performed with Wvase32 software using a Cauchy models. Porous structures were
24 assessed by Environmental Ellipsometry Porosimetry (EEP) that was carried out through
25 capillary condensation of water into the porosity with a controlled atmosphere cell in which
26 relative humidity was controlled by mass flow controllers.
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41 *Photocatalytic Tests.* Photoactivity of the composite systems was investigated in controlled
42 environmental conditions (RH = 40%, T = 22 ± 2°C) by monitoring the refractive index of the
43 contaminated layers under UV irradiation. Lauric acid (LA) was chosen as model contaminant
44 to fill the mesoporosity of composite films and deposited by dip coating from a 0.5wt% LA
45 solution in ethanol. The polluted samples were then placed into the ellipsometer environmental
46 chamber 4 cm under the UV lamp (365 nm/41.1 mW. cm⁻²). In situ ellipsometry measurements
47 of the polluted films were recorded every 20s to assess the optical density changes at controlled
48 humidity.²³
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3 RESULTS AND DISCUSSION

Structural interferential colors can be observed in the optical photograph in Figure 1(a) showing of a typical TiO₂ mesoporous film applied on glass in which thickness fluctuations and defects were induced on purpose. The colors are caused by a difference in refractive index between the glass substrate and the TiO₂ mesoporous coating.

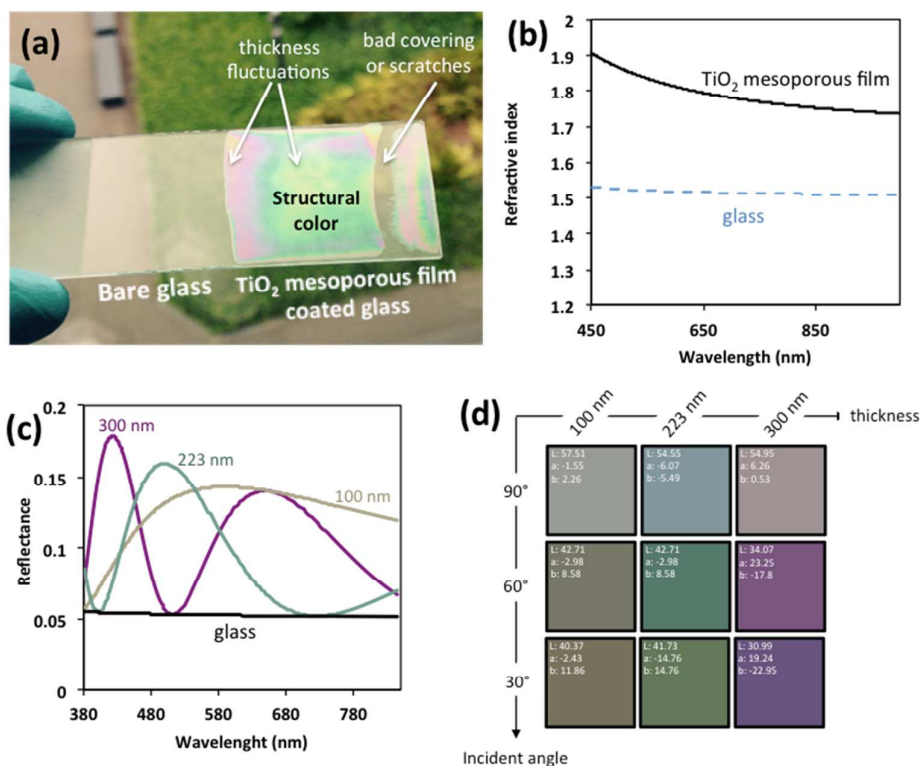


Figure 1: (a) Optical photograph of a typical TiO₂ mesoporous film applied on glass exhibiting structural colors (thickness fluctuations and defects were induced on purpose); (b) Refractive index dispersion of glass substrate and TiO₂ mesoporous film measured by ellipsometry; (c) Simulated reflectance spectra at 90° of TiO₂ mesoporous films (with variable thickness) on glass; (d) Simulated reflected colors (expressed in L*a*b* coordinates) as function of thickness and incidence angle.

This difference can be quantified by the plots of refractive index dispersions of the glass substrate and of the coating that have been obtained by ellipsometric measurements as shown in Figure 1(b). The specific shade depends on the thickness of the layer (and on the incident light angle). This effect is highlighted in Figure 1(c) and (d) in which starting from the refractive index dispersion of the substrate and of the coating, the reflectance curves and the reflected color (for different thicknesses and light incident angles) have been simulated by using the Wvase32 software.

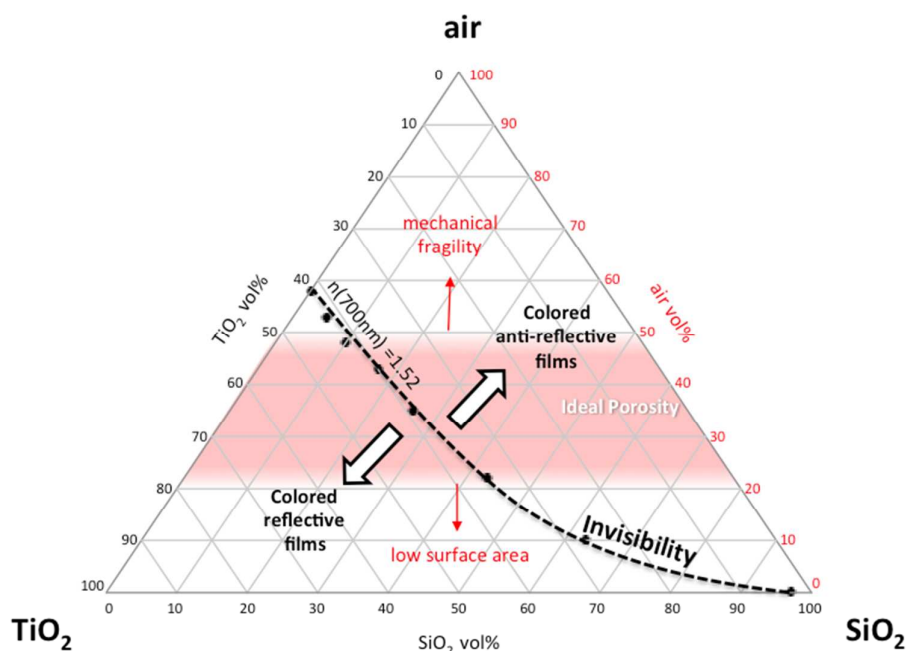


Figure 2: Simulated ternary phase diagram of SiO_2 - TiO_2 mesoporous films. The dotted line indicates the “invisibility” conditions on glass calculated from experimental data of refractive index.

In order to match the refractive index of the substrate in addition to TiO_2 and air, SiO_2 can be added as component. For this purpose a ternary phase diagram $\text{TiO}_2/\text{SiO}_2/\text{air}$ was built as shown in Figure 2. The conditions for invisibility on glass, highlighted by the dotted line (at 700nm),

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5 were obtained by different TiO₂/SiO₂/air mixtures and simulated by using Bruggemann effective
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7 medium approximation (BEMA) model:
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$$10 \quad f_{air} \frac{\epsilon_{air} - \epsilon}{\epsilon_{air} - 2\epsilon} + f_{wall} \frac{\epsilon_{wall} - \epsilon}{\epsilon_{wall} - 2\epsilon} = 0 \quad (1)$$

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16 in which ϵ_{air} and ϵ_{wall} represent the dielectric constant of air and of the solid wall that is
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18 composed by SiO₂ and TiO₂. Since air, SiO₂, and TiO₂ do not absorb light in the considered
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20 range of wavelengths (400-1000 nm), the dielectric constants are taken to be the square of the
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22 refractive index values (real part of the dielectric constants). Depending on the concentration
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24 and thermal treatment the sol-gel based SiO₂ and TiO₂ are not necessarily phase separated but
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26 can be mixed as solid solution. For our simulation, the values of refractive index of solid wall
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28 (corresponding to the nanocomposite TiO₂-SiO₂ materials) was taken from real measurements in
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30 the case of dense films (treated at 600°C).²⁴
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32 The targeted % vol porosity must be fixed in an “ideal” range (20%-50% as highlighted in
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34 Fig.2) in order to consider two opposite technological constrains. First, films with low porous
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36 volume % are characterized by low surface area, low pore’s accessibility and thus lower
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38 photocatalytic activity, a critical drawback for air-decontamination applications for instance.
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40 Second, since the mechanical stiffness (Young modulus) of a mesoporous coating is directly
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42 related to its density,²⁵ high % porosity will result in mechanical fragile layers. For these
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44 reasons, as starting point for our study, we decided to fix the inorganic/organic molar ratio to
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46 1/0.006 in order to obtain, *a priori*, a porosity %vol in the “ideal” range. Instead, in order to
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48 identify the best candidate (able to ensure invisibility, photoactivity and stiffness) we
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50 systematically varied the SiO₂/TiO₂ ratio and we investigated the role of SiO₂ on the evolution
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52 of the structural, optical, mechanical and photocatalytic properties.
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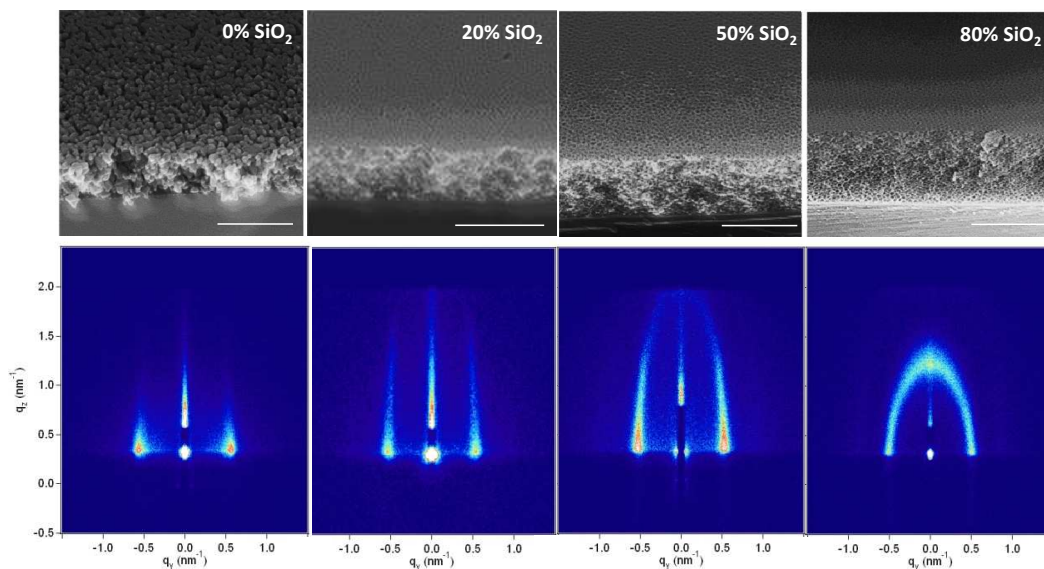


Figure 3 SEM-FEG cross section pictures and corresponding GI-SAXS patterns of selected composite TiO₂-SiO₂ mesoporous films with SiO₂ content of 0%, 20%, 50%, and 80%. Scale bars represent 250 nm.

3.1 Film Structure

Figure 3 shows the SEM images of four representative TiO₂-SiO₂ films made with 0%, 20%, 50%, and 80% of silica and their corresponding GI-SAXS patterns. Pure titania film picture exhibits the characteristic morphology of an open and highly accessible grid-like porosity, confirmed by the two parallel intense diffraction peaks of the GI-SAXS pattern at $q_y = 0.052 \text{ nm}^{-1}$ coming from the domains composed of periodical planes oriented perpendicular to the substrate with a period of about 12 nm. This TiO₂ grid-like mesostructure originates from the thermally induced transformation of the amorphous titania into crystalline phase. Indeed it has already been reported that the crystallization of the initial cubic structure is accompanied by matter migration through diffusing sintering and pore merging along the [111] directions, leading to the open grid-like structure.²⁶

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5 For composite thin films, networks of well-defined elliptical pores with short-range
6 organization are observed by SEM for SiO₂ content over 20%. Diffraction patterns obtained by
7 GI-SAXS reveal a progressive porous structure evolution from grid-like to elliptical pores with
8 the increase of SiO₂ ratio from 2% to 100% (detailed in S1) which suggests that the previously
9 described grid-like formation mechanism is almost not affected for low silica contents (typically
10 below ≈20%). For higher ratios, influence of silica precursors in the inorganic matrix becomes
11 preponderant on the resulting porous structure after annealing. Indeed, increasing siliceous
12 species during the first ageing step at RH = 75% and 37°C induces the formation of a growing
13 number of Ti-O-Si oxo bonds which tend to stabilize the Ti-based oligomers. Then, as already
14 demonstrated for dense TiO₂-SiO₂ films, the short thermal treatment at 600°C is expected to
15 induce the crystallization of small particles of anatase whose growth by Ostwald ripening is
16 prevented by silica that plays the role of barrier and hinders diffusive sintering.²⁴ Such barrier-
17 like silica effect was observed even at 900°C in mesoporous powders.²⁷ Less elongated
18 diffraction patterns in the z direction of the reciprocal space are observed for the lower TiO₂.
19 This feature indicates a decrease of the anisotropy of the elliptical pores since addition of SiO₂
20 induces a lower out-of-plane contraction of the films. The integration of the intensity profiles of
21 GI-SAXS scattered signals recorded for TiO₂-SiO₂ porous films with SiO₂ ratios from 2% to
22 98% and pure silica porous films are given in Supporting Information (see S2). The position of
23 the peak accounting for the correlation distance only slightly varies, indicating that the
24 periodicity of the structure is globally the same regardless the SiO₂ composition and the
25 crystallinity of films (as discussed in the following parts). The corresponding structural
26 periodicities are calculated to be in the range 11-13.5 nm in agreement with previous reported
27 values (between 11 nm and 14 nm) for F127-templated mesoporous films.²⁸
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29 Further investigation of the porous structures was performed by Environmental Ellipsometry
30 Porosimetry analysis (EEP).²⁹ Water adsorption-desorption isotherms recorded for TiO₂-SiO₂
31 films with SiO₂ ratios varying from 0% to 100% are displayed in Figure 4(a). The shapes of
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5 adsorption-desorption hysteresis loops are significantly different indicating a clear evolution of
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7 the porous morphology related to the inorganic network composition. Indeed mesoporous pure
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9 titania film (0% SiO₂) is characterized by a narrow adsorption-desorption hysteresis suggesting
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11 that mesopores are highly interconnected through large pore windows in agreement with a grid-
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13 like mesostructure. Addition of SiO₂ to the inorganic framework leads to a gradual broadening
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15 of the hysteresis loops; this is caused by a progressive decrease of the porous interconnection
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17 sizes resulting in cage-like porosity, i.e. large pores connected through smaller pore windows,
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19 which is supported by SEM images in Figure 3. In addition to the mesoporosity, the presence of
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21 micropores can be observed at low water vapor pressure (< 10%) for composites with silica
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23 content over 50%. Such microporosity, typical of silica mesoporous materials templated by
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25 PEO chains, is indicative on the formation of relatively extended silica-rich nanodomains within
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27 the composite network and in contact with F127 at the surface of pores. The pore size
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29 distributions of mesoporous TiO₂-SiO₂ films were determined from adsorption and desorption
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31 curves, using the Kelvin equation:
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$$\ln \frac{P}{P_0} = -\frac{\gamma V_l \cos \theta}{r_p R T} \quad (2)$$

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41 where (P/P₀) is the water relative pressure and r_p, γ, V_l, θ, R, and T are the Kelvin pore radius,
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43 the surface tension, the molar volume of liquid, the contact angle, the gas constant and the
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45 temperature, respectively. Pore sizes distributions taken from adsorption and desorption
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47 branches that are representative of the pore sizes and interconnected pore sizes (bottle-neck)
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49 respectively are plotted in S3 for silica ratios of 0%, 40%, 80%, and 100%. They show a relative
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51 broad distribution for pure titania films that tends to narrow when silica ratio increases.
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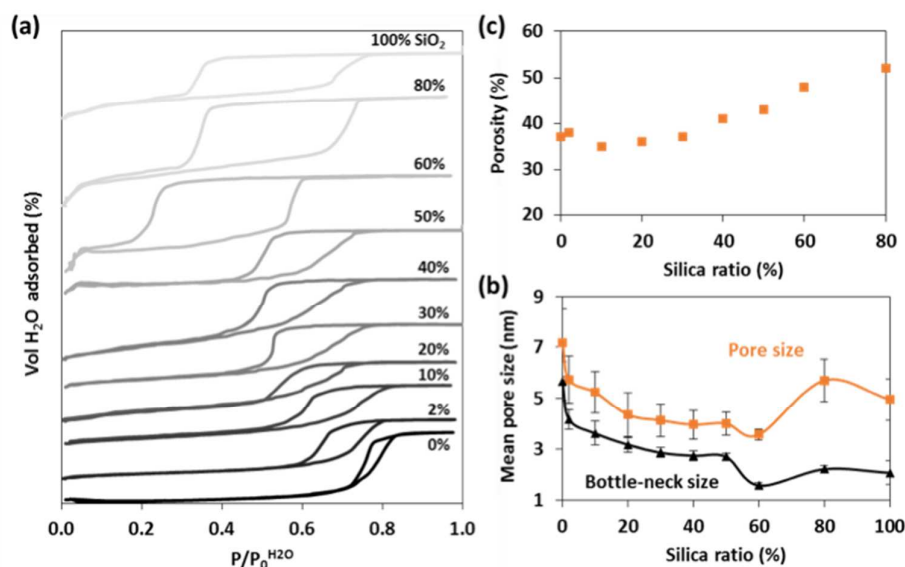


Figure 4. (a) Adsorption-desorption isotherms, (b) mean pore diameter and (c) porous volume depending on silica ratio obtained by EEP for various TiO₂-SiO₂ mesoporous films.

Evolution of average pore size and bottle-neck size as function of the silica content ($0\% \leq \text{SiO}_2$ ratio $\leq 100\%$), are reported in Figure 4b. The highest values, 7.2 nm and 5.7 nm for pore and interconnection sizes respectively, are observed for pure TiO₂ film due to the pore merging caused by diffusive sintering in agreement with SEM picture (Figure 3). The progressive incorporation of silica hinders diffusive sintering and pore merging, resulting in gradual and important decrease of pore and bottle-neck sizes. The pore and bottle-neck sizes decrease down to 3.6 and 1.3 nm at 60% SiO₂ respectively. The same way, average pore size slowly decreases from 4.3 nm at 20% SiO₂ to 3.6 nm at 60% SiO₂. Over 60% SiO₂ content, an increase in pore size is observed, probably due to a morphological modification of the porous network (from grid-like to elliptical) in absence of crystallization (and thus in absence of migration of matter by diffusive sintering).

The film porosity% has been evaluated by using Bruggemann effective medium approximation (BEMA) model from EEP measurements²⁹ and reported in Figure 4(c). Films show a stable

porous volume around 35% for silica ratio inferior to 20%, then it increase progressively to reach the value of 51% for silica fraction of 80%. This %vol porosity behavior as a function of silica confirms that: (i) the diffusive sintering, induces the partial collapse of the network, followed by densification and partial loss of the porosity during the high temperature crystallization of TiO₂-rich films and (ii) amorphous silica does prevent diffusing sintering and thus avoids the collapse and large shrinkage of the porous network during thermal annealing.

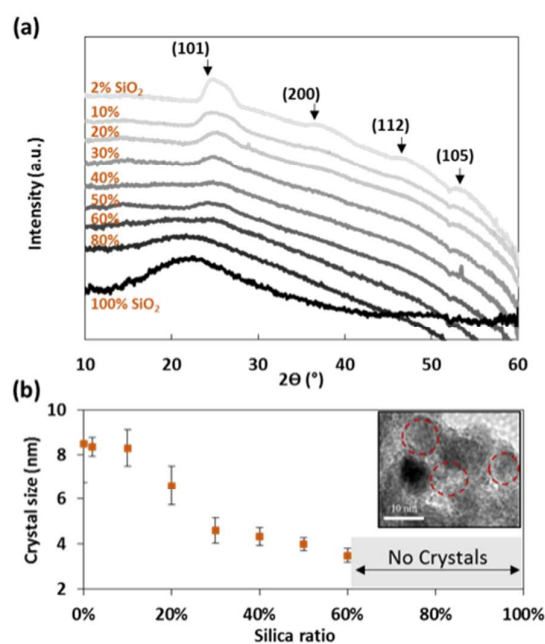


Figure 5 (a) GI-WAXS patterns of mesoporous composite TiO₂-SiO₂ films with various silica ratios in logarithm of the intensity. (b) Particle size evolution obtained by HR-TEM pictures of TiO₂ anatase nanocrystals, inset the HR-TEM image of the 2% SiO₂ sample (anatase crystals are circled in red).

3.2 Crystallinity

Porous TiO₂ layers to be photocatalytically active require the presence of anatase crystalline phase. Due to the low amount of crystalline matter and the small size of the crystallites in the films, especially for highest SiO₂ loading, X-ray diffraction analysis with conventional Bragg-

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5 Brentano configuration does not permit to extract the diffraction signals from the background.
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7 For this reason GI-WAXS was chosen as an analytical tool for its higher sensitivity. Figure 5(a)
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9 shows the GI-WAXS plots of mesoporous composite films for various SiO₂ ratios. In particular,
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11 the intensity (in logarithmic scale) is plotted as a function of 2 Θ . Plots exhibit four broad
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13 diffraction peaks characteristic of anatase phase evidencing the formation of TiO₂
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15 nanocrystallites. The major peak at 2 Θ = 25.4° corresponds to the (101) reflection of the anatase
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17 phase, which is present in most of the mesoporous TiO₂-SiO₂ composite films except for pure
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19 SiO₂ and 80% SiO₂ samples.

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21 The other peaks in GI-WAXS patterns are respectively related to the (200), (112), and (105)
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23 planes of the anatase phase. The peaks relative intensity decreases with the increasing
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25 composition in SiO₂ (from 2% to 60%) suggesting the diminution of crystallinity in the films.
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27 This trend, observed in a previous study for dense films,²⁴ can be attributed to a lower TiO₂
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29 content in the film but also to the fact that the crystallization temperature increases with the
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31 silica content in the TiO₂ matrix due to fact that silica network, if intimately mixed with
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33 titanium oxo species, acts as a barrier to their diffusion which tends to inhibit the nucleation-
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35 growth of TiO₂ crystallites. Crystallite size evaluation by Scherrer method cannot be used with
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37 the present XRD diagram because the grazing incidence geometry used for the analysis induces
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39 a diffracted beam broadening that is directly dependent on the sample size.³⁰ High-resolution
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41 transmission electron microscopy (HRTEM) images of mesoporous composite films with SiO₂
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43 ratio from 2% to 80% were recorded and are available in Supporting Information (S4). HRTEM
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45 micrographs evidence the presence of a nanoporous network, the average pore size was
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47 estimated in the range of 5 nm to 8 nm in agreement with the previous EEP characterization.
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49 Moreover nearly spherical TiO₂ anatase nanocrystals can be distinguished (dark spots). For
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51 samples with the highest silica content, TiO₂ crystals are embedded into SiO₂ (and TiO₂)
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53 amorphous matrix as in the case of 50% SiO₂ (see S4). The inset HR-TEM image of 2% SiO₂
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55 sample in Fig 5 (b), single crystals (circled in red) with plane distance of 3.5 Å were measured,
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5 which corresponds to the (101) plane of the anatase crystal in agreement with GI-WAXS
6 results. No particles were observed for 80% SiO₂ sample which is also consistent with the GI-
7 WAXS results. The average particle size was determined by image analysis from several tens of
8 particles from HR-TEM micrographs. The evolution of the average crystal size depending on
9 SiO₂ molar ratio is shown in Figure 5(b). It can be seen that crystal size decreases with SiO₂
10 content from 8 nm to 3.5 nm.
11

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13 Based on the characterization of the crystallization and the previous structural analysis, a
14 proposition of film formation is illustrated in Fig S5. The formation of mesostructured TiO₂-
15 SiO₂ nanocomposite films with variable Ti-Si ratio were successfully synthesized via
16 evaporation induces self-assembly process involving amphiphilic triblock copolymer F127
17 together with titanate and silicate oligomers. In a large excess of HCl, such as in our conditions
18 due to the use of TiCl₄ precursor, it has been demonstrated previously that final nanocomposites
19 have a uniform and homogeneous framework with well dispersed silicates, in which both
20 silicate and titanate oligomers can cross-link together, forming Ti-O-Si nanoclusters, and
21 contributing to the mesostructured networks without phase separation. Upon deposition and
22 self-assembly, the template F127 starts to decompose at 350°C and the mesopores are liberated.
23 Simultaneously, the titanate species are aggregated and the homogeneous amorphous
24 framework starts to crystallize because of the thermodynamic metastability of titania during
25 thermal treatment. The crystallization occurs above 300°C depending on the composition in
26 silica as shown by Louis *et al.*²⁴ The nuclei and nanocrystals of TiO₂ are formed in the pore
27 walls. At this moment phase separation happens and anatase nanocrystals are randomly
28 embedded in SiO₂ and TiO₂ amorphous matrixes. Phase separation continues to progress
29 through TiO₂ nanocrystals further growth by prolonging thermal curing time. During this stage,
30 the silica-rich formed matrix located around the anatase crystallites further cross-links,
31 stiffening at the same time the whole structure. Supplementary growth of TiO₂ crystallites
32 through Ostwald ripening (diffusive sintering) is then quenched by the presence of the silica
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5 matrix that inhibits the diffusion of titania-oxo species. The amorphous silica part of the matrix
6 is thus responsible of nanocrystal size, the more the silica content, the smaller the size of anatase
7 crystals, and also prevents the framework from collapsing.
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10 11 12 13 **3.3 Mechanical stiffness**

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15 The intrinsic mechanical properties of the films have been probed using EEP analysis, where the
16 transversal deformation induced by the capillary condensation of water in the pores can be
17 deduced from thickness evolution during water desorption.²⁹ Figure S6 displays the
18 superimposed plots of the variation of thickness upon water desorption for 5 representative
19 samples at different % SiO₂. From the relative thickness curves, the transversal Young's moduli
20 (E/GPa) were calculated using the method described in detail elsewhere.²⁹ The calculated values
21 of E as function of the SiO₂ % contents are reported in Figure 6. Pure TiO₂ films, characterized
22 by grid-like network of stacked nanocrystals, exhibits a Young modulus of 5.3 GPa, that is
23 consistent with previous investigations.³¹ Addition of small amount of SiO₂ in the network
24 induces an impressive increase in stiffness with E = 14.8 GPa for the system 90%TiO₂-
25 10%SiO₂. As shown in the scheme in Figure, the origin of this +160% increase in E can be
26 attributed to the "brick and mortar" structure of the nanocomposite films in which SiO₂
27 mechanically stabilizes the percolating TiO₂ nanocrystals network. For %SiO₂ > 10%, Young
28 moduli progressively decrease toward the E values typical of pure SiO₂ mesoporous films. This
29 progressive decrease is due to a morphological re-organization of the porous network (from-
30 grid-like to isolated elliptical pores) and to the fact that TiO₂ nanocrystals become isolated in a
31 pure SiO₂-based amorphous matrix.
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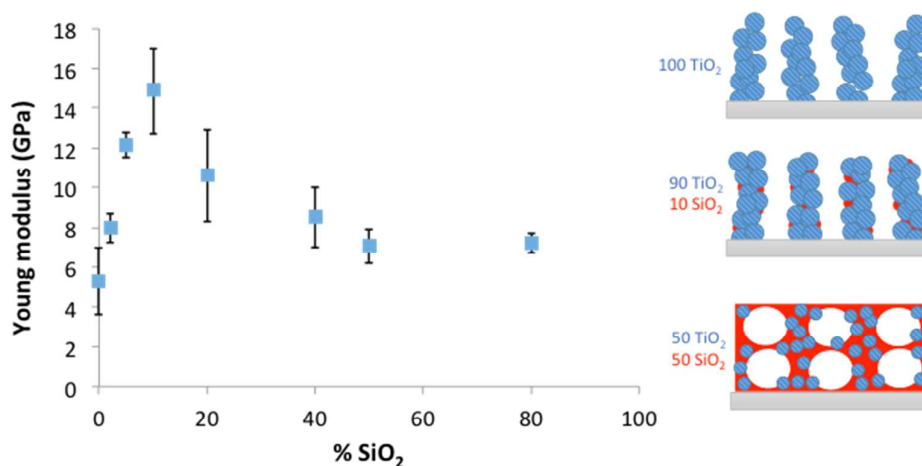


Figure 6 Evolution of the Young moduli obtained from EEP experiments as function of the SiO₂% content; inset: schematic illustration of the expected porous structures

3.4 Photocatalytic Activity

The photocatalytic activity of TiO₂-SiO₂ mesoporous films in air was assessed by in situ ellipsometry. For these investigations lauric acid (LA) was used as model contaminant. LA alcoholic solution with the concentration of 0.5 wt% was infiltrated into the porosity by dip coating. The UV-lamp irradiation at 365 nm (41.1 mW.cm⁻²) was operated in a closed chamber with a controlled atmosphere maintained at constant 40% humidity and room temperature ($T = 22 \pm 2^\circ\text{C}$). The humidity atmosphere was chosen at RH = 40% because, as reported in our recent work,³² similar photocatalytic degradations of lauric acid were obtained for conventional encountered atmospheric humidity rates (between 20% and 60%). Photocatalytic activities were deduced from the variation of the film refractive index during the photo-induced decomposition of infiltrated lauric acid. Speeds of LA decomposition were compared for each SiO₂ ratio, by plotting the evolution of the normalized LA/LA₀ depending on the time of irradiation, where LA is the composition of lauric acid at the irradiation time (t) and LA₀ is the initial concentration.

Concentrations of LA (t) were deduced from the refractive index values applying the BEMA model.³²

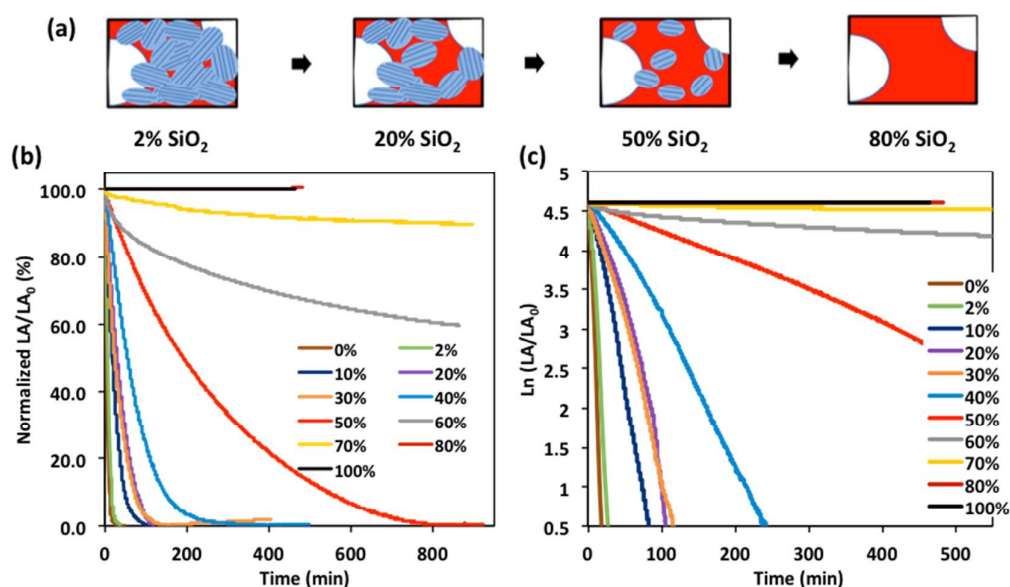


Figure 7 (a) Schematic of the TiO₂-SiO₂ nanocomposite evolution, blue particles represent TiO₂ crystals and the red part is the silica (and titania) amorphous matrix. (b) Plots of normalized LA/LA₀ depending on the time of UV irradiation and (c) the corresponding first-order kinetic curves (Ln(LA/LA₀) vs time) for mesoporous TiO₂-SiO₂ nanocomposite films with various silica ratio.

As observed in Figure 7(b), the elimination of lauric acid takes place for all samples except the ones containing 80% and 100% of SiO₂ for which LA content doesn't change with time. This lack of photoactivity is consistent with the previous GI-SAXS and HR-TEM analyses, indicating the absence of anatase nanocrystals. Good photoactivity can be observed for samples containing silica up to 40% of silica; as general trend, the efficiency of the photocatalysis decreases with SiO₂ content, as expected. Schematic of the structure evolution is given in Figure

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5 7(a), where blue particles represent titania nanocrystals and the red part is the amorphous phase
6 of silica and titania matrix. For low SiO₂ ratio, the fraction of TiO₂ nanocrystals, and their
7 accessibility, are higher leading to a higher photoactivity (higher TiO₂ surface area for the
8 radical generation and a higher surface of contact between pollutant and nanocrystals).
9 Inversely, for higher silica content, a lower photocatalytic activity can be explained by the lower
10 global TiO₂ amount and to the fact that the nanocrystals are partially embedded in the
11 amorphous silica network (thus less accessible to the LA molecules). Other critical factors that
12 likely play a role on the global efficiency are: (i) the decrease of the crystal size with the
13 increasing SiO₂ content which is known to modify the photocatalytic efficiency³³, (ii) the
14 constrictions of the porosity are more pronounced in presence of SiO₂ as showed in Figure 4(b),
15 affecting probably the mobility of LA molecules, and (iii) photoactive species and products of
16 the redox reaction (carbonated residues are known to form stable coordination bonds with TiO₂)
17 into the porosity.
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31 The corresponding first-order kinetic tendencies ($\ln(LA/LA_0)$ vs t) were plot in Figure 7(c). It is
32 observed that globally, the LA degradation evolutions follow pseudo- first-order kinetics, at
33 least in the case of the most active samples (%SiO₂ <50%). However, the first order kinetic
34 behaviors ($\ln(LA/LA_0)$ vs t) of the composite mesoporous TiO₂/SiO₂ film are not always linear
35 suggesting that the degradation rates is not only due to the progressive consumption of LA at
36 the pore surface but also to other factors that evolve during the experiment such as water
37 adsorption on the pore surface.²³ In order to better analyze these trends, the evolution of the
38 kinetic constant vs time is plotted in Figure 8(a); the kinetic constant of the first order
39 degradation reaction (k) can be determined by using the corresponding derivatives –
40 $d(\ln(LA/LA_0))/dt$ vs t . It is clear that different $k(t)$ absolute values and tendencies result from
41 different film compositions. As environmental conditions (RH = 40%, 20% of O₂, and room
42 temperature) and concentration of impregnated LA are all controlled to be similar, discrepancies
43 in $k(t)$ are mainly governed by the film structure and composition. In general (and as expected)
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TiO₂-rich samples provide the higher absolute values of $k(t)$. Other considerations can be made here. First, the initial activity, k at $t = 0$ min, can be attributed to the initial presence of OH and O₂ scavengers intrinsically adsorbed during handling and impregnation with LA.

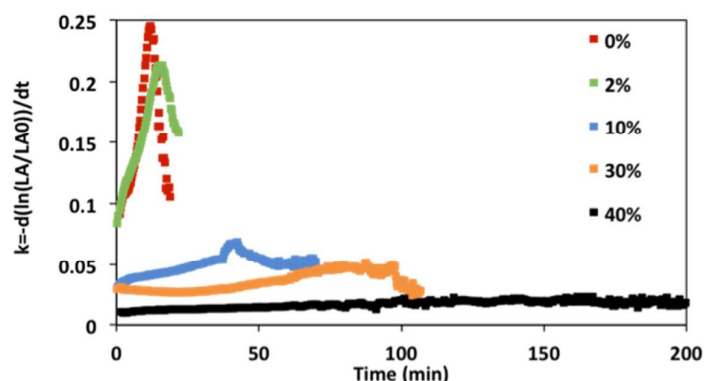


Figure 8 Curves of $-d(\ln(LA/LA_0))/dt$ vs time, which represent the evolution of the kinetic constant k (min^{-1}) all along the experiment for various ratio of silica.

Only the scavengers that are in direct contact with the active anatase surface will contribute to the initial decomposition reactions. Thus the increase of the silica content, which is logically accompanied by a decrease of the active surface into the pores, explains the lower initial k value at high silica content. Second, at short times the kinetic constant progressively increases since LA is decomposed at the anatase surface and liberates sites where H₂O and O₂ can adsorb. This induces an increase of scavenger concentration with time, causing an acceleration of the global decomposition reaction rate. After reaching a maximum, $k(t)$ goes down progressively due to the progressive consumption of LA pollutant. Third, the $k(t)$ maxima (which stand for the nearly end of decomposition reactions) shift to longer times with the increasing percentage of SiO₂. This behavior is obviously related to the fact that less active films required more time to totally decompose LA molecules. Fourth, $k(t)$ values are almost constant with time for 40% SiO₂ sample that is characteristic to a nearly perfect first-order kinetic.

3.5 Optical properties

Optical properties of mesoporous TiO_2 - SiO_2 composite layers were accessed by spectroscopic ellipsometry. Recorded data were fitted by a Cauchy model allowing the determination of the dispersion of the refractive index in the visible range (from 450 nm to 1000 nm). Figure 9 presents the optical properties of the layers as a function of the silico-titanate composition, the dispersion curve of a bare glass substrate was added for comparison. Figure 9 (inset) summarizes the trend refractive index (at 700 nm) of mesoporous TiO_2 - SiO_2 nanocomposite films as function of the SiO_2 %.

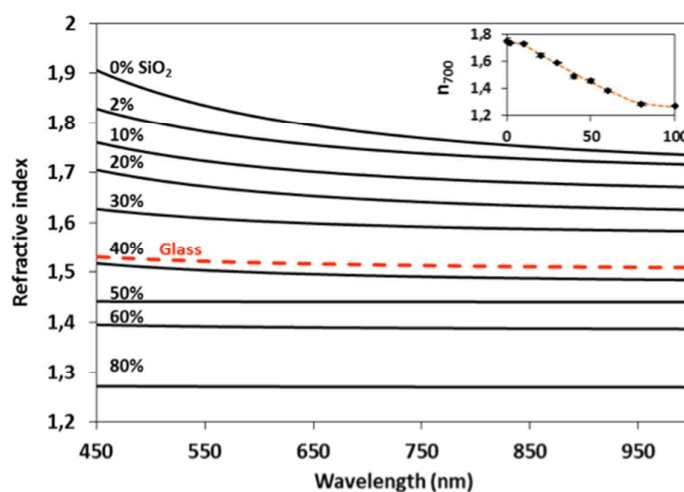


Figure 9 Evolution of the dispersion of refractive index for mesoporous TiO_2 - SiO_2 composite films depending on silica content and for bare glass. (inset) Mesoporous TiO_2 - SiO_2 composite films refractive index at 700 nm depending on silica content.

From the experimental results it is clear that the refractive index could be tuned from 1.74 to 1.27 (at 700 nm) with increasing silica ratio. One notes that evolution is also partially caused by the porous volume that slightly increases as SiO_2 ratio increases at constant porogen agent molar ratio due to the thermal-induced framework restructuring as discussed previously.

From these results, we can evaluate the optical behavior of the composite layers if applied on glass substrate. Samples having dispersion of refractive index higher than bare glass will behave

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5 as reflective coatings, typically for layers with SiO₂ ratio superior to 40%. At the opposite,
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7 layers with lower refractive index (SiO₂ < 40%) will behave as (poor) antireflective coatings. In
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9 both cases, a structural color, resulting from destructive and constructive reflections, always
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11 appears. Interestingly, the 40% SiO₂ coating exhibits a very similar refractive index dispersion
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13 as respect to the bare glass substrate. In this case, the coating will likely behave as an optically
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15 “invisible” layer on glass.
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20 **3.6 Invisible, photocatalytic films on glass**

21 To validate the concept of “invisible” photocatalytic layer, glass substrates were coated with
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23 the 60%TiO₂-40%SiO₂ layers, the most promising candidate for “invisibility” according with
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25 the optical analyses. The same experiments were conducted with the pure mesoporous titania
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27 films as reference. In order to better evaluate the appearance/suppression of the structural
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29 colors, in both cases, three different thicknesses were obtained by tuning the withdrawal speed
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31 during dip-coating (3, 5 and 15 mm s⁻¹). The corresponding transmittance spectra of both types
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33 of stacks and of a bare glass substrate are plotted in Figure 10(a) for wavelength comprised
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35 between 400 nm and 800 nm and different thickness of coatings. Pure titania mesoporous layers
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37 exhibit the typical behavior of reflective coatings with decrease of transmittance values up to
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39 more than 20% and fluctuations that depend on the layers thickness. Starting from the
40
41 experimental transmission curves, the simulated reflected colors of pure mesoporous TiO₂ films
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43 are shown in Figure 10 (b). As expected, a structural color appears and its shade depends
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45 significantly on the thickness and the incident angle. Oppositely, the transmittance curves of the
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47 mesoporous 60%TiO₂-40%SiO₂ layers are nearly identical to the one of the bare substrate. The
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49 efficiency in suppression of the structural colors can be visually observed in Figure 10 (b) in
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51 which no shade is present, with a low dependency towards coating thickness and incidence
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53 angle.
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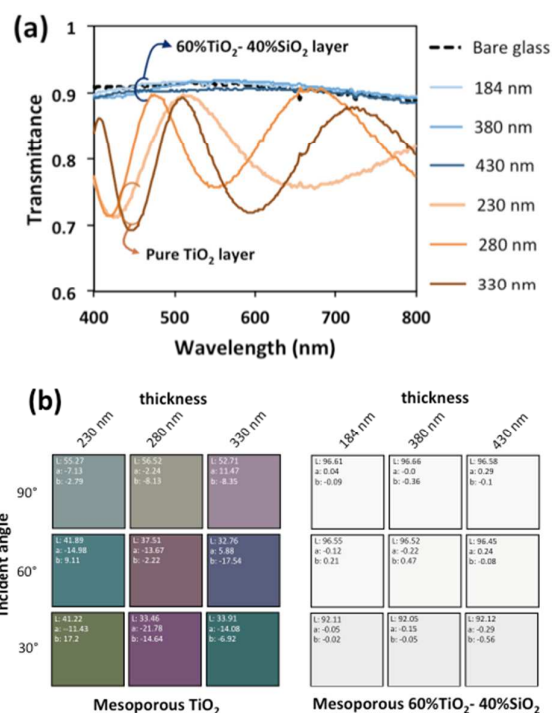


Figure 10 (a) Transmittance of mesoporous pure TiO₂ and 60%TiO₂-40%SiO₂ one side coated glass substrates with various thickness recorded in visible spectrum. (b) Simulated reflected colors (expressed in L*a*b coordinates) as function of thickness and incidence angle.

The photocatalytic activity of the 60%TiO₂-40%SiO₂ “invisible” film on glass was confirmed by monitoring its transmittance spectra along a pollution/depollution cycle. The film was first artificially polluted with lauric acid, following the same procedure of the ellipsometric analysis. As shown in Figure 11 after infiltration by lauric acid, the increase in refractive index of the coating results in a decrease in transmittance. The sample was then exposed to UV light (365nm) for 3 hours; after UV irradiation, the sample re-gains its initial transmission performances indicating that the pollutant was efficiently decomposed.

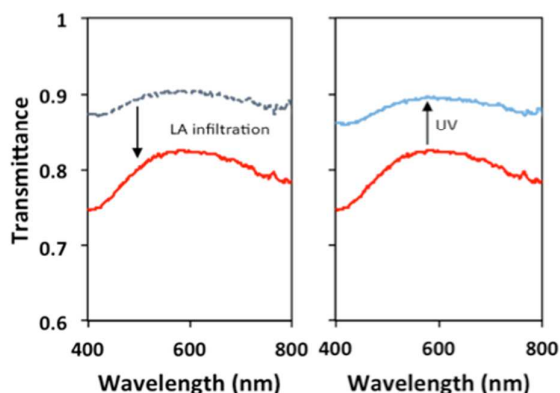


Figure 11 Transmittance curves of mesoporous 60%TiO₂-40%SiO₂ film infiltrated by Lauric Acid (red curve) and after UV irradiation

4 CONCLUSIONS

Summarizing, in this work we investigated the role of SiO₂ to suppress the structural color of mesoporous TiO₂-based coatings on glass. Nanocomposite SiO₂-TiO₂ mesoporous films were fabricated by liquid deposition route and systematically characterized. We highlight that addition of SiO₂ on TiO₂-based coatings resulted in a progressive porous network reconfiguration from “open” grid-like structure to more “isolated” elliptical pores. We also revealed that 10% of SiO₂ leads to an impressive improvement (+160%) in stiffness as respect to pure TiO₂ mesoporous layers. Supported by optical simulation, it is shown that depending on the composition, such mesoporous coatings normally behaved as colored antireflective and reflective coatings. Importantly, we demonstrated coatings characterized by a precise composition (60%TiO₂-40%SiO₂) and porosity volume (40%vol) performed as invisible layers with improved mechanical stiffness and still high photocatalytic activity.

ASSOCIATED CONTENT

Supporting Information.

GI-SAXS and pore size distribution data as well as HR-TEM pictures of TiO₂ nanocrystals and optical simulations of mesoporous TiO₂-SiO₂ composite thin films. These materials are available free of charge via the internet at <http://pubs.acs.org>.

AUTHOR INFORMATION

Corresponding Author

* E-mail: marco.faustini@upmc.fr

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Table of Contents

