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1 **Inversion of calcite twin data for paleostress orientations and magnitudes: a new**
2 **technique tested and calibrated on numerically-generated and natural data**

3

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11 **Abstract**

12 The inversion of calcite twin data is a powerful tool to reconstruct paleostresses sustained by
13 carbonate rocks during their geological history. Following Etchecopar's (1984) pioneering work, this
14 study presents a new technique for the inversion of calcite twin data that reconstructs the 5 parameters
15 of the deviatoric stress tensors from both monophasic and polyphasic twin datasets. The uncertainties
16 in the parameters of the stress tensors reconstructed by this new technique are evaluated on
17 numerically-generated datasets. The technique not only reliably defines the 5 parameters of the
18 deviatoric stress tensor, but also reliably separates very close superimposed stress tensors (30° of
19 difference in maximum principal stress orientation or switch between σ_3 and σ_2 axes). The technique
20 is further shown to be robust to sampling bias and to slight variability in the critical resolved shear
21 stress. Due to our still incomplete knowledge of the evolution of the critical resolved shear stress with
22 grain size, our results show that it is recommended to analyze twin data subsets of homogeneous grain
23 size to minimize possible errors, mainly those concerning differential stress values. The
24 methodological uncertainty in principal stress orientations is about $\pm 10^\circ$; it is about ± 0.1 for the
25 stress ratio. For differential stresses, the uncertainty is lower than $\pm 30\%$.

26 Applying the technique to vein samples within Mesozoic limestones from the Monte Nero

27 anticline (northern Apennines, Italy) demonstrates its ability to reliably detect and separate
 28 tectonically significant paleostress orientations and magnitudes from naturally deformed polyphase
 29 samples, hence to fingerprint the regional paleostresses of interest in tectonic studies.

30 1. Introduction

31 Defining deformation mechanisms in the upper crust as well as their driving stresses are key
 32 scientific and technical issues. Quantifying stresses allows to better understand the mechanical be-
 33 havior of geological materials and to decipher tectonic mechanisms, from those related to plate mo-
 34 tions at a large scale to those causing jointing and faulting or even microstructures at a smaller scale.
 35 However, the way stress orientations and magnitudes actually evolve in naturally deforming rocks
 36 over time scales of several tens of millions of years is still a pending question, and even sophisticated
 37 geomechanical models require stress constraints in order to be accurately calibrated.

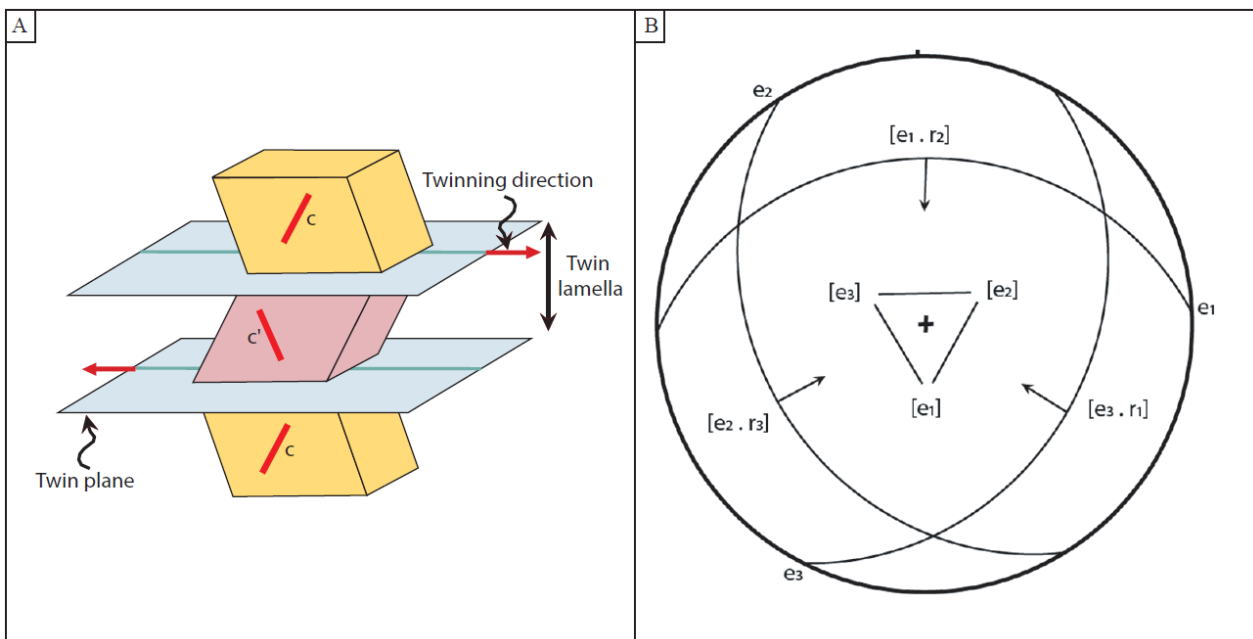


Figure 1: Scheme of a twin lamella (pink) in a calcite crystal (yellow). B) Stereographic projection (lower hemisphere, equal area) of the e-twinning system of the calcite crystal. The optical axis C is vertical at the center of the diagram. The poles of the three twin plane sets are [e1], [e2] and [e3]. The planes of twinning are the large circles; they contain the twinning direction [e_i : r_j]; for each twin plane, the arrow is parallel to the twinning direction; its head indicates that the upper part of the crystal moves upward, toward the C axis, as a reverse microfault (After Turner et al., 1954).

38 In order to decipher the tectonic evolution and to provide constraints on the past states of
39 stress, methods of paleostress reconstructions based on the mechanical interpretation of various struc-
40 tural or petrographic elements in natural rocks have been set out. Among these methods, those based
41 on the microstructural study of twinning in minerals have proven to be efficient in reconstructing
42 stress (orientations and/or magnitudes) sustained by rocks during their tectonic history. These meth-
43 ods make use of the property that twinning depends on the magnitude of the shear stress which has
44 been applied to them (Tullis, 1980). E-twinning is a common mechanism of plastic deformation in
45 calcite aggregates deformed at low pressure and low temperature. E-twinning occurs in the host crys-
46 tal by an approximation to simple shear in a particular sense and direction along specific crystallo-
47 graphic ϵ planes (Fig. 1). Since calcite is widely encountered in sedimentary basins and mountain
48 belts and is among the most sensitive mineral for twinning, it can be seen as an important paleostress
49 indicator for the upper crust (e.g., Lacombe, 2010). Inversion of calcite twins for paleostress is thus
50 a well-established approach to reconstruct paleostress orientations and magnitudes of differential
51 stresses (Amrouch et al., 2010; Arboit et al., 2015; Kulikowski and Amrouch, 2017; Lacombe, 2001;
52 Lacombe et al., 2009, 1990; Lacombe and Laurent, 1992; Rocher et al., 2000, 1996) in nature and is
53 a promising tool to estimate principal stress magnitudes when combined with fracture analysis and
54 rock mechanics (Amrouch et al., 2011; Arboit et al., in press; Lacombe, 2007, 2001) or stylolite
55 roughness paleopiezometry (Beaudoin et al., 2016). Among the available techniques, the Calcite
56 Stress Inversion Technique, CSIT (Table 1) (Etchecopar, 1984) allows the determination of the five
57 parameters of the deviatoric stress tensor, i.e., principal stress orientations and differential stress mag-
58 nitudes, the latter being strongly dependent on the (still debated) existence of a Critical Resolved
59 Shear Stress (CRSS) for twinning (Burkhard, 1993; De Bresser and Spiers, 1997; Newman, 1994;
60 Rowe and Rutter, 1990; Tullis, 1980).

61 Despite a wealth of successful regional paleostress reconstructions in polyphase tectonic
62 settings (see Lacombe, 2010, and references therein), the application by Gaęala (2009) of the CSIT
63 to numerically generated calcite aggregates has cast some doubt on the ability of the technique to

64 efficiently separate superimposed tensors with close principal stress orientations. Moreover,
 65 methodological uncertainties in stress parameters as determined by CSIT have never been properly
 66 stated and remain to be better defined.

CSIT	Calcite stress inversion technique
CRSS	Critical resolved shear stress
τ_s	Applied resolved shear stress
τ_a	Critical resolved shear stress
$\sigma_1, \sigma_2, \sigma_3$	The principal stress
Φ	The stress ratio
F	The penalization function
τ_s^{min}	The smallest resolved shear stress applied on the last twinned plane taken into account by the inversion method
τ_s^j	The resolved shear stress applied on the jth untwinned plane
L ² -norm	Distance calculated between two tensor in MPa
Δ_{1-3}	Maximum differential stress

Table 1: List of symbols used.

67 The goal of this study is to present and test a new scheme of inversion, called CSIT-2, partly
 68 inspired by the CSIT. The newly developed technique and its ability to efficiently separate
 69 superimposed stress tensors are tested on numerically-generated and naturally deformed monophasic
 70 (only one tensor applied) and polyphase (two tensors applied) twin datasets. The results demonstrate
 71 the reliability of such an approach to derive the stress parameters of interest, hence to provide an
 72 efficient toolbox for tectonic studies.

73 2. A brief review of existing methods to derive stress from calcite twins

74 Since the pioneering work of Turner (1953), several methods of stress reconstruction have
 75 been developed on the basis of the analysis of calcite twin data (Etchecopar et al., 1981; Jamison and
 76 Spang, 1976; Laurent et al., 1990, 1981; Nemcok et al., 1999; Pfiffner and Burkhard, 1987; Yamaji,
 77 2015a, 2015b).

78 The basis of the widely used paleopiezometric method of Jamison and Spang (1976) is that,
 79 in a sample without any preferred crystallographic orientation, the relative percentages of grains
 80 twinned on 0, 1, 2 or 3 twin plane(s) depend on the applied differential stress value ($\sigma_1 - \sigma_3$). Since

81 this relationship has been experimentally calibrated, knowing these relative percentages in a sample
82 and under the hypothesis of a constant CRSS for twinning, the order of magnitude of $(\sigma_1 - \sigma_3)$ can be
83 estimated. The severe limitations of this method are that (1) it does not take into account the grain
84 size dependence of twinning, (2) it applies only to uniaxial stresses, (3) it does not check before
85 calculation whether twin data are related to one or more superimposed stress tensors and (4) it does
86 not make it possible to relate differential stress estimates to a given stress regime since principal stress
87 orientations are not determined (Lacombe, 2010).

88 Rowe and Rutter (1990) determined empiric laws between twinning incidence, twin volume
89 fraction, twin density and experimentally applied differential stress to derive a calcite twinning
90 paleopiezometer. The two first parameters are dependent on the grain size. The twin density is more
91 easily used to calculate the differential stress because it does not depend on grain size. However, the
92 law has been calibrated for temperature above 400°C and clearly overestimates the differential stress
93 values when applied to samples deformed at low temperature (Ferrill, 1998). In addition, this method
94 shares the same limitations as the Jamison and Spang (1976) technique, which consists in not
95 checking whether twin data are related to one or more superimposed stress tensors and not making
96 possible to relate the differential stress estimates to a given state of stress.

97 Laurent et al.'s technique (1981) was the first to take into account both twinned and untwinned
98 planes to find 5 parameters of the stress tensor. This technique uses the deviatoric stress tensor (based
99 on the nearly null dependence of twinning on isotropic stress) and relies upon a Boolean calculation
100 to determine the solution tensor. This method was seldom used because it is time consuming (Laurent
101 et al., 1990). Laurent et al. (1990) also proposed a new method which determines the 5 parameters of
102 the deviatoric stress tensor. This technique uses a non-linear equation to determine the deviatoric
103 stress tensor and is faster than Laurent et al. (1981) technique. These methods have not given rise to
104 numerous applications in the literature.

105 The CSIT (Etchecopar, 1984) method is to date the most used technique to retrieve the past

106 stress tensors (e.g., Amrouch et al. 2010; Beaudoin et al. 2012, 2016; Lacombe and Laurent 1992;
107 Lacombe 2001, 2007; Lacombe et al. 2009; Rocher et al., 1996, 2000). The inversion process is very
108 similar to the one used for fault slip data (Etchecopar, 1984), since twin gliding along the twinning
109 direction within the twin plane is geometrically comparable to slip along a slickenside lineation within
110 a fault plane. The basic assumptions are: (1) the existence of a Critical Resolved Shear Stress (CRSS)
111 for twinning and (2) a potential twin plane is twinned (respectively, untwinned) if the resolved shear
112 stress applied on it is greater (respectively, lower) than the CRSS. The inversion process takes into
113 account both the twinned and untwinned planes and provides the 5 parameters of the deviatoric stress
114 tensor, i.e., principal stress orientations and differential stress magnitudes. It should be noted that the
115 value of the CRSS depends on grain size as well as on internal grain deformation since calcite hardens
116 once twinned (Newman, 1994; Tullis, 1980; Turner et al. 1954). However the evolution of CRSS with
117 grain size has not been well constrained yet. The CSIT technique has been successfully tested on
118 experimentally deformed natural samples (Lacombe and Laurent, 1996; Laurent et al., 2000) and the
119 results have shown maximum deviations of computed principal stress orientations compared to
120 experimentally applied ones of 5-7° for monophasic and 7-11° for polyphase cases. In 2009, Gaḡała
121 questioned the ability of this technique to reliably reconstruct the orientations of the principal stress
122 axes and the stress ratio of close superimposed stress tensors. The penalization function used to refine
123 the tensor solution is considered to be too restrictive by Rez and Melichar (2010) and Yamaji (2015b),
124 especially when dealing with natural samples where optical measurement bias may occur. For Rez
125 and Melichar (2010), the penalization function of CSIT (see section 3.1) is strongly dependent on the
126 compatible twinned and the incompatible untwinned planes with the stress tensor solution. In addition,
127 the space of solutions with a penalization function of 0 is too large. So, they proposed a new
128 penalization function with sharper maxima, depending on the number of compatible twinned planes,
129 the number of compatible untwinned planes and the number of incompatible untwinned planes. Note
130 however that the CSIT with this refined penalization function has never been applied to polyphase
131 twin datasets.

132 Nemcok et al. (1999) technique works for both calcite twin and fault-slip data. The approach
133 consists in searching all 3D tensors which can activate or re-activate a twin plane. They analyze
134 clusters of twin data to group them in sets based on their response to one or multiple stress tensors.
135 Each subset is tested to establish monophasic solution twin datasets. Polyphase sets are divided into
136 monophasic subsets. Each subset is analyzed to obtain the reduced stress tensor (orientation of
137 principal stress axes and stress ratio). The study of Gaḡała (2009) demonstrates that this method is
138 however not suitable for treating polyphase data.

139 The most recent stress inversion technique to date has been proposed by Yamaji (2015b). This
140 technique, based on the generalized Hough transform, provides like CSIT, the 5 parameters of the
141 deviatoric stress tensor. The preliminary exploration of the extent to which calcite twinning may
142 constrain stress (Yamaji, 2015a) demonstrates that twinned planes better constrain the stress tensor
143 than untwinned planes and that differential stress estimates are poorly resolved for differential stresses
144 greater than 50-100 MPa. This technique seems to separate superimposed stress tensors only if the
145 intersection between their spherical caps is nonexistent or small. Spherical caps correspond to the
146 data points on a unit sphere based on the five-dimensional stress space; the deviatoric stress tensors
147 responsible for twinning are thus denoted by the size and position of the spherical cap (see Yamaji,
148 2015a for details). Comparing his new technique to existing ones, Yamaji (2015a) states that the CSIT
149 appears to be unstable, mainly due to the selection method of the solution tensors, which is only
150 dependent on the last twinned plane taken into account in each solution tensor tested (see the theory
151 of CSIT below). The limitation of Yamaji's technique is that it has not to date been tested on
152 experimentally or naturally deformed samples.

153 An outcome of this short review is that the analysis of calcite twin data makes it possible to
154 reliably obtain the 5 parameters of the deviatoric stress tensor under specific assumptions in
155 monophasic twin datasets. However, the challenge of all techniques is to reliably separate and
156 reconstruct superimposed stress tensors as from polyphase datasets. There is especially a consensus
157 toward the difficulty to detect and separate tensors which are very close in terms of principal stress

158 orientations and differential stress magnitudes. These questions are addressed hereinafter through the
159 setup and calibration of a new inversion scheme, CSIT-2. Its application to synthetic (numerically
160 generated) calcite twin data allows to define the methodological uncertainties and the applicability
161 domains of the new technique as well as the influence of heterogeneities commonly found in natural
162 samples. The technique is finally applied to a naturally deformed polyphase sample to check its ability
163 to reconstruct the regional paleostresses.

164 **3. A new calcite twin inversion scheme (CSIT-2): methodology**

165 **3.1 Theory and basic equations of CSIT (Etchecopar, 1984)**

166 As said above, the principle of CSIT is to invert a calcite twin dataset for stress. The basic
167 underlying hypothesis is that a potential e-twin plane is twinned if and only if the resolved shear stress
168 applied on the direction of the twinning exceeds the critical resolved shear stress value τ_a (CRSS):

- 169 • If $\tau_s \geq \tau_a$, then the plane is twinned. (1)
- 170 • If $\tau_s < \tau_a$, then the plane remains untwinned. (2)

171 with τ_s , the resolved shear stress applied along the gliding direction of the e-plane. The optimally
172 oriented twin plane will be activated if the applied differential stress is equal to, or greater than, $2\tau_a$.

173 The basic assumptions are that strain and stress are coaxial (low strain conditions), the stress
174 field is homogeneous at the grain scale and twinning is a non-reversible process.

175 The principle of the inversion of calcite twin dataset is to find a stress tensor (or several stress
176 tensors) which verifies these two inequalities for the largest number of twinned planes and the whole
177 set of untwinned planes. The solution has the form of a reduced stress tensor with 4 parameters: the
178 orientations of principal stress axes ($\sigma_1, \sigma_2, \sigma_3$) and the stress ratio (Φ):

$$179 \quad 1 \geq \Phi = \frac{\sigma_2 - \sigma_3}{\sigma_1 - \sigma_3} \geq 0 \quad (3)$$

180 The differential stress ($\sigma_1 - \sigma_3$) is normalized to 1, so the normalized resolved shear stress applied

181 on each twin plane varies within $[-0.5 ; 0.5]$.

182 The inverse problem consists in finding the stress tensor that best explains the spatial
183 distribution of measured twinned and untwinned planes. The first step consists in an arbitrary choice
184 of a percentage of twinned planes to be explained. The resolved shear stresses are calculated on the
185 twinned and untwinned planes, which are ranked as a function of the decreasing resolved shear stress.
186 In theory, the solution tensor should meet the requirement that all the twinned and untwinned planes
187 should be consistent with it. Thus, all twinned planes should sustain a resolved shear stress (τ_s) larger
188 than that exerted on all the untwinned planes. The sorting allows to determine rapidly whether some
189 untwinned planes are incompatible with the tensor (i.e., the resulting resolved shear stress is greater
190 than that for some compatible twinned planes).

191 The second step of the process therefore consists in calculating a penalization function, f ,
192 ideally equal to 0, which is defined as:

$$193 \quad f = \sum_{j=1}^{j=n} (\tau_s^j - \tau_s^{min}) \quad (4)$$

194 where τ_s^{min} is the smallest resolved shear stress applied on the twinned planes compatible with the
195 tensor, and τ_s^j is the resolved shear stresses applied on the j untwinned planes such that $\tau_s^j > \tau_s^{min}$.
196 The penalization function increases if incompatible untwinned planes are incorporated in the solution.
197 The optimal tensor is obtained when the maximum number of twinned planes and the minimum
198 number of incompatible untwinned planes are incorporated in the solution.

199 This process therefore yields the orientation of the 3 principal stress axes, the stress ratio and a non-
200 dimensional differential stress. This non-dimensional differential stress, $\frac{(\sigma_1 - \sigma_3)}{\tau_a}$, is such that,

$$201 \quad \frac{(\sigma_1 - \sigma_3)}{\tau_a} = \frac{(\sigma_1 - \sigma_3)_{normalized}}{\tau_s^{min}} = \frac{1}{\tau_s^{min}}$$

202 Under the assumption of a known and constant CRSS, τ_a , the actual differential stress is

203 given by equation 5:

204
$$(\sigma_1 - \sigma_3) = \frac{\tau_a}{\tau_s^{min}} \quad (5)$$

205 **3.2 New inversion scheme (CSIT-2): motivation and principle**

206 If the basic principle of CSIT-2 remains more or less the same as the CSIT for the calculation
 207 of the penalization function, the major difference lies in the automatic detection of one or several
 208 tensors. The choice has been made to systematically cover the space with a regular interval of 10° for
 209 the 3 Euler's angles (defining the orientation of the stress tensor axes) and a fixed stress ratio value
 210 of 0.5. The total amount of tested tensors is of 5832 tensors in CSIT-2.

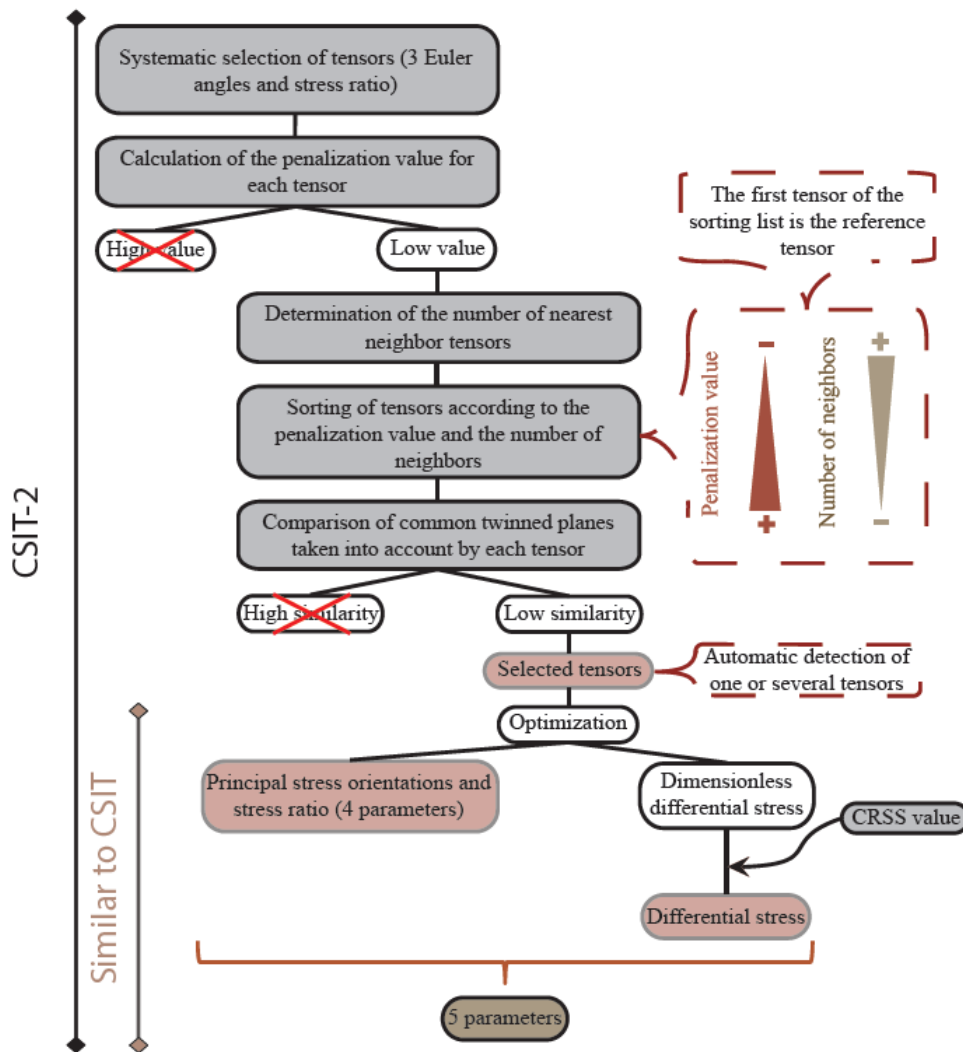


Figure 2: Workflow of CSIT-2 for inversion of calcite twin datasets.

211 The tensor that is retained by the CSIT method for further optimization is the tensor presenting

212 the minimum value of the penalization function. This means that if several tensors with the same
213 minimum penalization function exist, only one will be arbitrarily chosen for the inversion. However,
214 in case of several tensors with the same low penalization function (ideally 0, corresponding to a
215 solution with incorporation of no incompatible untwinned planes), it is interesting to keep these
216 different tensors, which might correspond to superimposed stress tensors. Contrary to CSIT, the
217 CSIT-2 allows to automatically detect the presence of one or several tensors. For that purpose, the
218 following steps are performed (Fig. 2):

- 219 (1) The user defines a starting percentage of twinned planes to be explained (20%
220 recommended).
- 221 (2) The program will test systematically different tensors with the 3 Euler's angles being
222 sampled every 10° and a stress ratio of 0.5.
- 223 (3) The penalization function is calculated for each stress tensor (equation 4).
- 224 (4) The stress tensors with a penalization function larger than a limit fixed by the user are
225 discarded.
- 226 (5) Each tensor is weighted by the number of its nearest neighbors, based on the calculation
227 of the angular distance (Yamaji and Sato, 2006). This step is important to automatically
228 detect the different clusters of tensors with low penalization function values.
- 229 (6) The tensors are sorted in descending order based on the number of nearest neighbors and
230 then in ascending order based on penalization function.
- 231 (7) The "best" tensors are selected: the first tensor of the list is the reference one. The
232 reference tensor has the largest number of neighbors and the lowest penalization function
233 value. The other tensors are kept if the percentage of shared twinned planes does not
234 exceed a percentage threshold chosen by the user.
- 235 (8) The selected tensors are then optimized for different percentages of twinned planes to be

236 explained using the Rosenbrock (1960) optimization method.

237 Thus, the choice of the retained tensors is based on different criteria: percentage of twinned
238 planes to be explained (step 1), penalization function (steps 4 and 6), angular distance (step 5) and
239 similarity criterion (step 7). The starting percentage of twinned planes to be explained is generally
240 20%. This value has been chosen because for a lower percentage, optical measurement uncertainties
241 and grain-scale heterogeneities as expected in naturally deformed samples could generate too much
242 noise and thus too many stress tensors could satisfactorily match the solution. If a percentage higher
243 than 20% is chosen there is a risk to miss potentially superimposed tensors by only detecting the best
244 expressed tensor. This percentage of twinned planes to explain has been chosen after several
245 numerical tests to configure the different parameters depending on the user (the starting percentage
246 of twinned planes to explain, the angular distance and the percentage of shared twinned planes
247 between two tensors to determine if they are similar or not). Finally, in case of superimposed stress
248 tensors with a high degree of similarity, it is possible that the inversion process may select an average
249 tensor (i.e., resulting from averaging the two applied tensors) in addition to the two applied tensors.
250 However, this average tensor is easy to identify and to discard because the technique also yields the
251 two applied tensors.

252 In order to automatically determine the different “best” tensors, it is necessary to highlight the
253 clusters of tensors with low penalization function values. For that purpose, several steps are needed.
254 The angular distance is calculated between all the selected tensors using the angular stress distance
255 defined by Yamaji and Sato (2006). Each tensor is weighed by its penalization function as well as by
256 the number of tensors within an angular distance of less than 30° (Yamaji and Sato, 2006). This 30°
257 value has been retained because it involves a low variation of orientation of the principal stress axes
258 and a possible variation of the stress ratio of less than 0.5. This step is of first importance and makes
259 it possible to determine clusters with the highest density of tensors and a low penalization function
260 value.

261 The first tensor on the sorted list is used as the reference tensor. It explains at least the chosen
262 20% of twinned planes with possible incorporation of incompatible untwinned planes. The set of
263 twinned planes explained by other tensors are compared to the set explained by this reference tensor.
264 The parameter of similarity is defined as the number of common twinned planes between the first and
265 the second tensor divided by the total number of twinned planes explained by the second tensor. A
266 new tensor is retained if it involves less than 70% of similarities (for detailed explanations, see
267 subsection 3.6). This makes it possible to detect very close tensors that consequently share a high
268 percentage of twinned planes. The twinned planes explained by this second tensor are recorded and
269 each other tensor is compared in the same way to determine a possible third tensor, and so on.

270 Following this similarity criterion, few tensors are selected. Then they are further tested
271 against the twin dataset by increasing the percentage of twinned planes to be explained. For each
272 percentage, an optimization is carried out (Rosenbrock, 1960). The ultimate goal is to explain the
273 largest number of twinned planes and untwinned planes with an as low as possible penalization
274 function value. The solution tensors are retained on the basis of the trend of evolution of their
275 parameters: orientations of principal stress axes, penalization function, τ_s^{min} value, stress ratio and
276 number of incompatible untwinned planes against the increasing number of twinned planes to be
277 explained. The first criterion considered is the stability of the principal stress axis orientations. If they
278 are stable despite the increasing number of twinned planes to be explained, the second criterion is the
279 stability of the penalization function together with the evolution of the percentage of incorporated
280 incompatible untwinned planes. This last parameter is defined as being the number of incompatible
281 untwinned planes divided by the number of twin planes taken into account by the tensor (compatible
282 twinned planes + incompatible untwinned planes). The solution then corresponds to the percentage
283 of twinned planes to be explained that is marked by the break in slope of the penalization function
284 value. If this percentage corresponds to the break in slope of the incorporation of incompatible
285 untwinned planes, then the stability of the stress ratio and of the resolved shear stress value should be
286 taken into account to ultimately refine the solution.

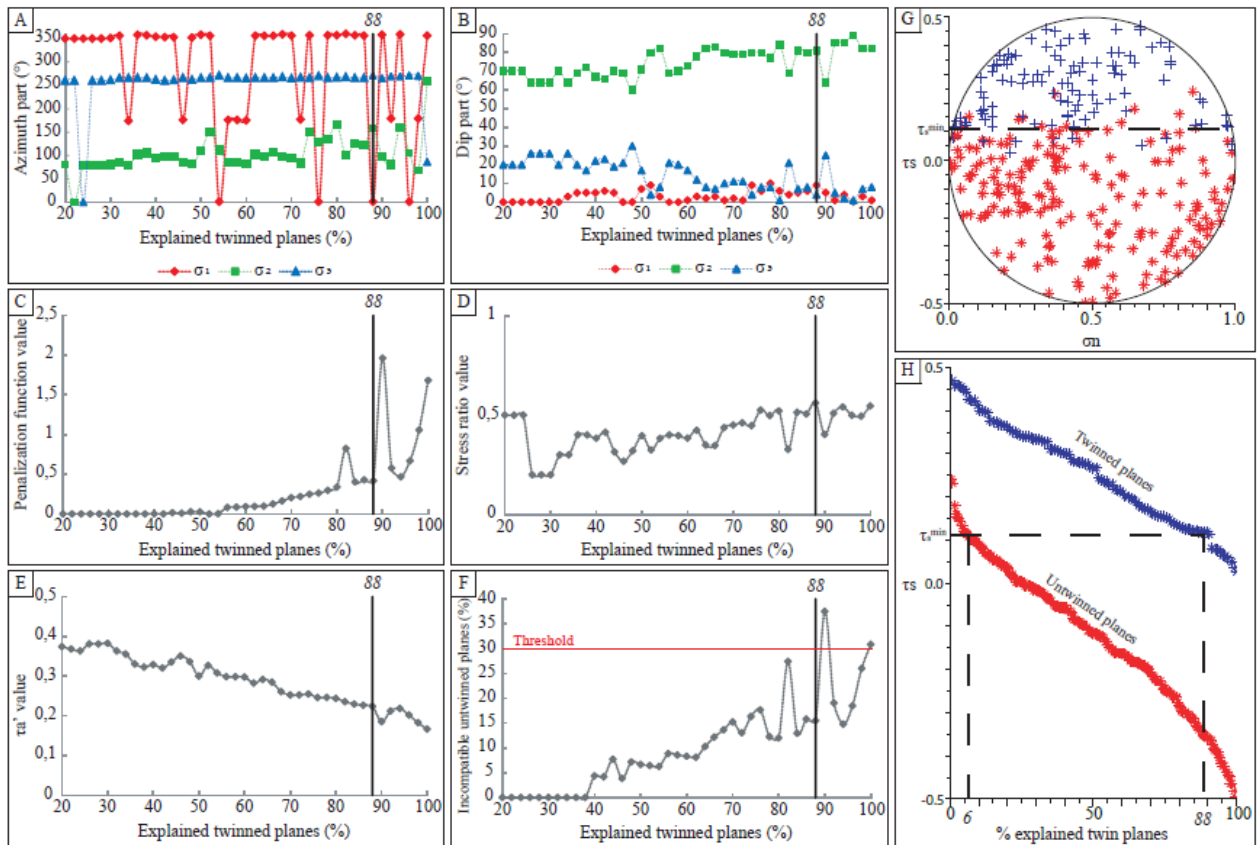


Figure 3: Graphics showing the variation of the penalization function value with the stress ratio for a same orientation stress axis (σ_1 : N180-0 and σ_3 : N270-0) and an applied stress ratio of 0.3 that has been registered after the added loop (see details in the first paragraph part 3.2) for A) 20%, B) 70% and C) 80% of explained twinned planes.

287 An example in Figure 3 illustrates how the best solution (maximum number of twinned planes
288 and minimum number of incompatible untwinned planes) is defined. Increasing the percentage of
289 twinned planes to be explained does not affect here the principal stress orientations which remain
290 very stable (Fig. 3A & B), but it affects the τ_s^{min} value (Fig. 3E) and thus the differential stress value
291 (equation 5). Figure 3C represents the evolution of the penalization function with the increasing
292 percentage of twinned planes to be explained. This curve is very similar to the curve describing
293 incorporation of incompatible untwinned planes (Fig. 3F). In this example the best choice is the
294 solution at 88% of explained twinned planes because the slope of the penalization function curve
295 greatly increases above this percentage. It means that the incorporation of incompatible untwinned
296 planes becomes too high beyond this percentage. Figures 3D and 3E display the evolution of the
297 stress ratio value and of the τ_s^{min} value used to calculate the differential stress (equation 5). For the

298 stress ratio curve the solutions between 20% and 36% of explained twinned planes are not stable.
 299 Above 36% of explained twinned planes, the stress ratio is stabilized at about 0.5. Figure 3G
 300 represents the pseudo-Mohr circle showing τ_s against σ_n and figure 3H displays the evolution of τ_s for
 301 untwinned and twinned planes as a function of the percentage of twinned planes to be explained
 302 (calculated based on the total amount of untwinned planes). Both figures provide visualization of
 303 τ_s^{min} . As shown, the value of τ_s^{min} corresponds to a slight incorporation of untwinned planes in the
 304 solution (< 10%, Fig. 3H). In addition, these incompatible untwinned planes are plotted in figure 3G
 305 close to line representing the retained τ_s^{min} ; this means that these incompatible untwinned planes
 306 sustain a low resolved shear stress compared to most of twinned planes consistent with the tensor.
 307 The solution is thus defined with confidence.

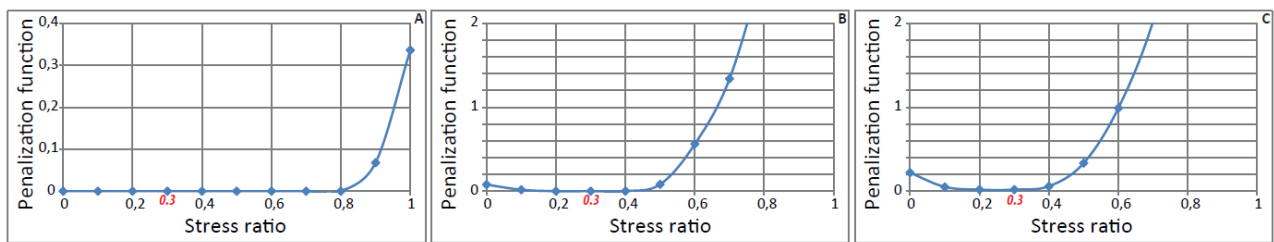


Figure 4: Determination of the best solution tensors of CSIT-based inversion on the basis of the evolution of parameters used during inversion process. The evolution of the parameters is shown as a function of the % of twinned planes to be explained by the tensor solution. The applied tensor is a N-S strike-slip regime ($\sigma_1 = N180-0$; $\sigma_3 = N270-0$) with a stress ratio of 0.5 and a differential stress of 35 MPa (test M9 in Table 1).

308 During the initial detection step, the choice to fix the stress ratio at 0.5 (following in that
 309 Yamaji, 2015b) was made (1) to reduce the computation time, and (2) because the inversion tends in
 310 polyphase cases to be stuck at tensors with extreme stress ratio (0 or 1) that account for a larger
 311 number of twin data. However, to make sure this choice does not bias the determination of stress ratio,
 312 a loop has been added before the optimization (step 8) which increases the stress ratio value by step
 313 of 0.1 from 0 to 1. The first test is a monophasic case with $\sigma_1 = N180-0$; $\sigma_3 = N270-0$, a stress ratio of
 314 0.3, a differential stress of 50 MPa (Fig. 4). It can be observed that the inversion is not very sensitive
 315 to the stress ratio at low percentage of twinned planes to explain. This suggests that at 20% of
 316 explained twinned planes (step 1), considering a fixed stress ratio (0.5) will not lead to artificially

317 focus tensor solutions toward tensors with stress ratio of 0.5 hence to discard (step 4) those with stress
 318 ratios different from this value .

319 With this initial detection step, the determination of stress tensors using CSIT-2 requires only
 320 a short computation time, about 15-20 minutes.

321 3.3 Creation of synthetic calcite twin dataset

	M1	M2	M3	M4	M5	M6	M7	M8	M9	M10	M11	M12	M13	M14	M15	M16
Equivalent grain size (MPa)	10						(2/3 grains) 5 and (1/3 grains) 15	Gaussian distribution centered on 10			Gaussian distribution centered on 8 and 12			Gaussian distribution centered on 10		
Applied stress orientation (°)	$\sigma_1 : N180-0 ; \sigma_2 : N90-90 ; \sigma_3 : N270-0$															
Φ	0	0	0,5	0,5	1	1	0,5									
Δ_{1-3} (MPa)	25	75	25	75	25	75	50	75	35	50	75	35	50	75	50	
Bias (%)	0														10	25

Table 2: Configuration of data tested for monophase cases.

322 The present method is first tested with numerically generated calcite twin datasets (Table 2
 323 and 3). The use of synthetic data with various (but controlled) sources of complexity allows to better
 324 evaluate the performance, applicability domain and limitation of the new technique. Indeed, natural
 325 data have expectedly issues (spatial distribution of grains with different sizes, heterogeneity of stress
 326 within the aggregates due for instance to stress concentration at grain boundaries, inheritance - growth
 327 twins or earlier deformation twins - due to regional tectonic history), so that it is only after the
 328 synthetic experiments have been completed that the applicability of the CSIT-2 technique to natural
 329 data will be evaluated.

330 For the simplest case (monophase synthetic sample with perfectly homogeneous grain size,
 331 table 2), one tensor is applied on randomly generated twin planes within grains with random
 332 orientations of optical C axes (Fig. 5A). Each grain is assigned a CRSS value roughly simulating its
 333 virtual size since twinning is grain size dependent (i.e, twinning is easier in large grains than in small

334 grains). A 5-parameter (deviatoric) stress tensor is applied on the generated twin data, resulting in
 335 some e-twin planes being activated (twinned) depending on their orientation with respect to the
 336 applied stress (Fig. 5B).

	B1	B2	B3	B4	B5	B6	B7	B8	B9	B10	B11	B12	B13	B14	B15	B16	B17	B18	B19	B20	B21	B22	B23	B24	B25	B26	B27	B28	B29											
Equivalent grain size (MPa)	Gaussian distribution centered on 10																																							
Applied stress orientation (*)	σ_1 : N180-0 σ_2 : N90-90 σ_3 : N270-0	σ_1 : N30-0 σ_2 : N120-90 σ_3 : N300-0	σ_1 : N180-0 σ_2 : N90-90 σ_3 : N270-0	σ_1 : N30-0 σ_2 : N120-90 σ_3 : N300-0	σ_1 : N90-0 σ_2 : N180-90 σ_3 : N360-0	σ_1 : N180-0 σ_2 : N90-0 σ_3 : N270-90	σ_1 : N180-0 σ_2 : N90-90 σ_3 : N300-0	σ_1 : N30-0 σ_2 : N120-90 σ_3 : N270-0	σ_1 : N180-0 σ_2 : N90-90 σ_3 : N300-0	σ_1 : N30-0 σ_2 : N120-90 σ_3 : N270-0	σ_1 : N180-0 σ_2 : N90-90 σ_3 : N270-90																													
ϕ	0,5					0					0,3					0,7					0,5																			
Δ_{1-3} (MPa)	50				35				75				35				75				35				75				35				75				35			
Bias (%)	10		25		10		25		35		75		35		75		35		75		35		75		35		75		35		75		35		75					

Table 3: Configuration of data tested for polyphase cases.

337 For the case of a polyphase synthetic sample (table 3) with homogeneous grain size, and in order to
 338 account for strain hardening, a second tensor is applied with each previously twinned grain being now
 339 assigned a CRSS increased by a value of 2 MPa as proposed by Gągała (2009).

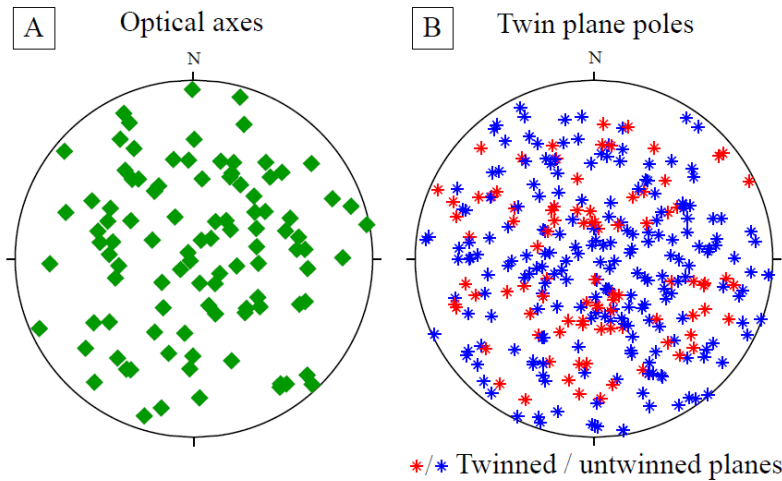


Figure 5: Wulff lower hemisphere stereographic projection of the random distribution A) C axes and B) poles of twin planes in numerically-generated datasets. The applied stress tensor corresponds to: N-S σ_1 axis, E-W σ_3 axis, a stress ratio equal to 1 and differential stress equal to 75 MPa.

340 In order to simulate a heterogeneous grain size in both synthetic monophasic and polyphase
 341 calcite aggregates, the choice was made to consider two virtual classes of grains with different sizes,
 342 simulated as two classes of grains with different assigned CRSS for twinning.

343 Finally, in order to simulate optical bias that depends on several factors (e.g., angle between
 344 the thin section and the twin lamella, width and spacing of twin lamellae, extension of lamellae across
 345 grains), some twinned planes were randomly misclassified into untwinned planes. For a horizontal
 346 thin section with 100 randomly oriented grains (i.e 300 e-twin planes), and considering that a twin

347 plane lying at an angle of 30° or less to the thin section cannot be measured using a classical U-Stage
 348 hence can be misclassified as untwinned, we estimated that the percentage of potentially optically
 349 biased twin planes is always lower than 11% with an average of 6% (Fig. 6).

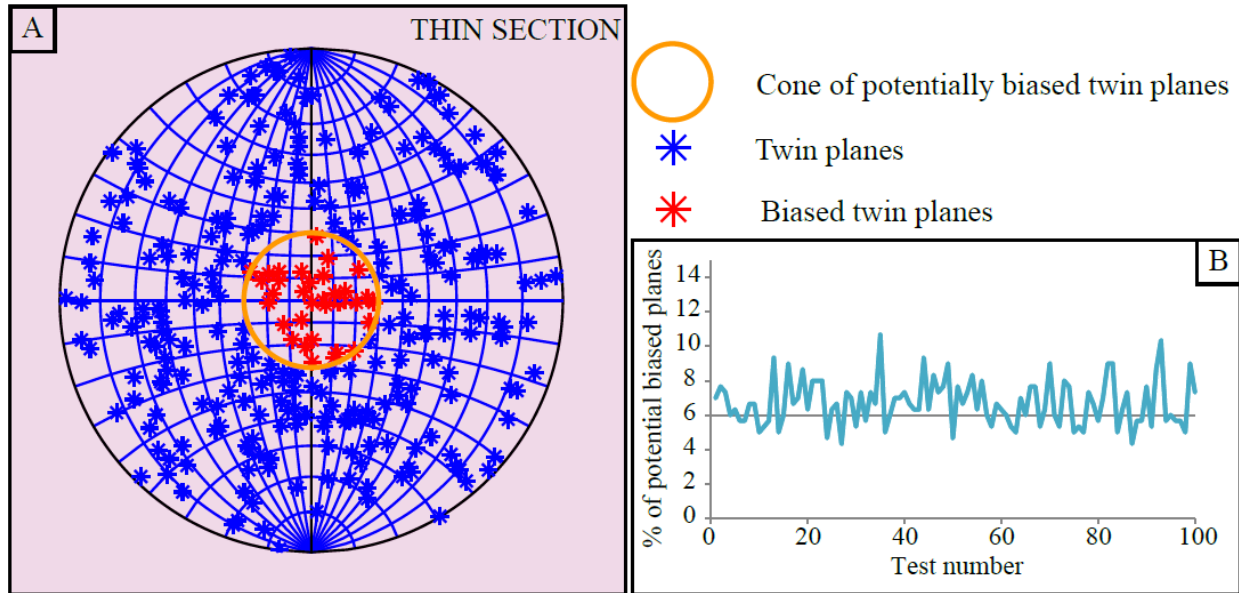


Figure 6: Evaluation of optical measurement bias related to inaccurate observations of twin planes. A) For a synthetic sample of 100 grains and 300 e-twin planes, and a horizontal thin section, the orange circle represents the cone of potentially biased poles to e-twin planes lying at less than 30° of the thin section plane. B) Variation of the percentage of potentially biased e-twin planes (lying at less than 30° of a virtual thin section plane cutting across a random distribution of twin planes) within various tests (100 synthetic datasets have been drawn and tested).

350 Following Yamaji (2015a, b), we further considered a maximum percentage of misclassified un-
 351 twinned planes of 20-25% in order to also account for the other potential sources of heterogeneity at
 352 the scale of the virtual aggregate. Note however that the weight of this bias on the quality of the result
 353 of stress inversion may be highly variable. For instance, if a randomly misclassified untwinned plane
 354 is close to the optimal position for a potential twin plane to twin regarding the stress criterion, it will
 355 receive a high resolved shear stress. Then it will appear as an incompatible untwinned plane incorpo-
 356 rated in the solution even for very low percentages of twinned planes to explain. This will greatly
 357 influence the penalization function and hence the quality of the solution. This abnormal plane is seen
 358 as an error by the software and the penalization function is strongly impacted, which could lead to
 359 discard the stress tensor from the acceptable solutions.

360

3.4 Criterion adopted to evaluate the degree of error between applied and solution ten-

361 sors

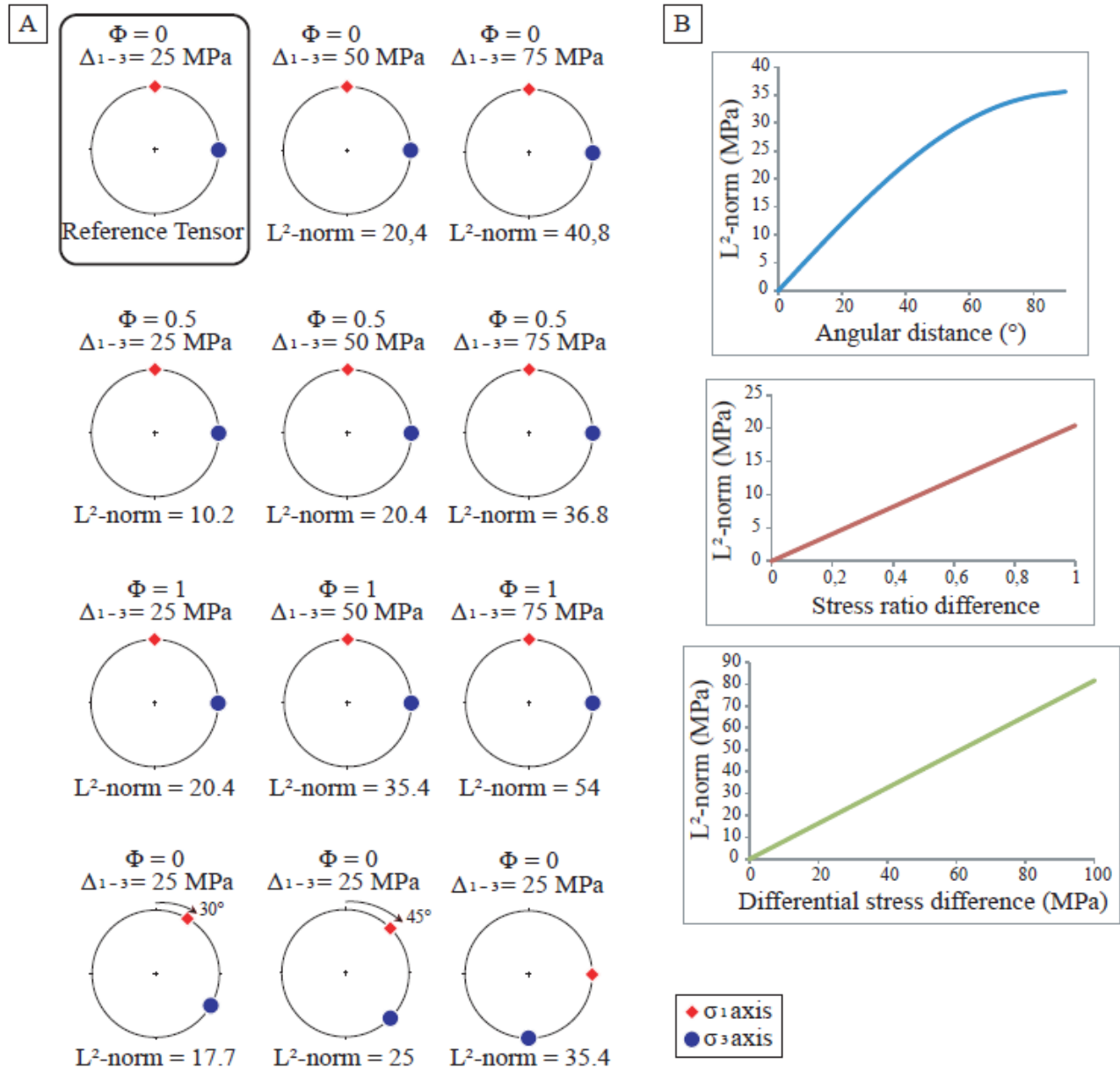


Figure 7: Evolution of the L^2 -norm value against variations of stress tensor parameters. A) Illustration of different tensor configurations and resulting L^2 -norm value. B) Sensitivity of L^2 -norm value to stress tensor parameters (principal stress orientation, stress ratio and differential stress).

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It is necessary to efficiently compare the 5 parameter stress tensors resulting from the

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inversion (called “solution tensor”) to the initially applied tensor (called “applied tensor”), in order

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to determine the accuracy of the inversion method. Peeters et al. (2009) propose different kinds of

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distance calculations between 5 parameter tensors. The L^2 -norm was chosen for our purpose, because

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it is the most robust for all tensor configurations:

$$L^2 - norm (A, B) = \sqrt{\sum_{i=1}^3 \sum_{j=1}^3 (A_{ij} - B_{ij})^2} \quad (6)$$

with A and B the tensors with 5 parameters and L^2 -norm the value of the distance in mega Pascal (MPa). Note that this equation strongly resembles the one used by Yamaji (2015b, §3.5) and differs only by a factor of $\sqrt{2/3}$. The equation can be written as a measure between tensors, σ^A and σ^B :

$$L^2 - norm(A, B) = \sqrt{(\sigma^A - \sigma^B) : (\sigma^A - \sigma^B)} = \sqrt{\frac{2}{3}} d \quad (7)$$

where the colon denotes the double-dot product of tensors (Yamaji and Sato, 2006 ; Yamaji, 2007), and d is Yamaji's (2015b) dissimilarity measure.

Figure 7 helps visualize how the L^2 -norm value evolves with different configurations of tensors, hence its sensitivity to changes in σ_1 orientation, stress ratio and differential stress. The L^2 -norm value is clearly more sensitive to variations of differential stress than to variations of the stress ratio or principal stress orientations.

3.5 Tests for calibration of the new inversion scheme

For the first tests, one tensor is applied (so-called monophasic dataset), with one grain size. The grain size is simulated using the corresponding CRSS value. But in nature it is very rare to have a sample with just one grain size. To fit with reality, other tests have been carried out with two distinct grain sizes, but also with a dispersion around the two mean grain sizes (pseudo-Gaussian distribution of grain sizes associated to different CRSS values also following a pseudo-Gaussian distribution). Taking into account the 10 MPa CRSS value commonly adopted for grains of size of about 300 μm and deformed at 3% (see Lacombe, 2010), it has been decided to test a distribution of grain sizes as corresponding to a distribution of CRSS values centered on 10 MPa, with 60% of grains with a CRSS value of 10 MPa, 15% between 10 - 13 MPa and 7 - 10 MPa, and 5% between 5 - 7 MPa and 13 - 15 MPa (denoted homogeneous grain size hereinafter). This enables to test the sensitivity and robustness

390 of the technique to slight variations in CRSS value or grain size within a defined grain size class.

391 Biases are also incorporated in order to simulate the natural heterogeneities of a rock sample
392 as well as optical measurement mistakes due to the use of a U-stage. To incorporate heterogeneities,
393 the program will randomly change a percentage of twinned planes (fixed by the user) into untwinned
394 planes.

395 In a second part, CSIT-2 is tested on datasets with two applied tensors and the same scheme
396 is carried out in order to determine the uncertainties in the results.

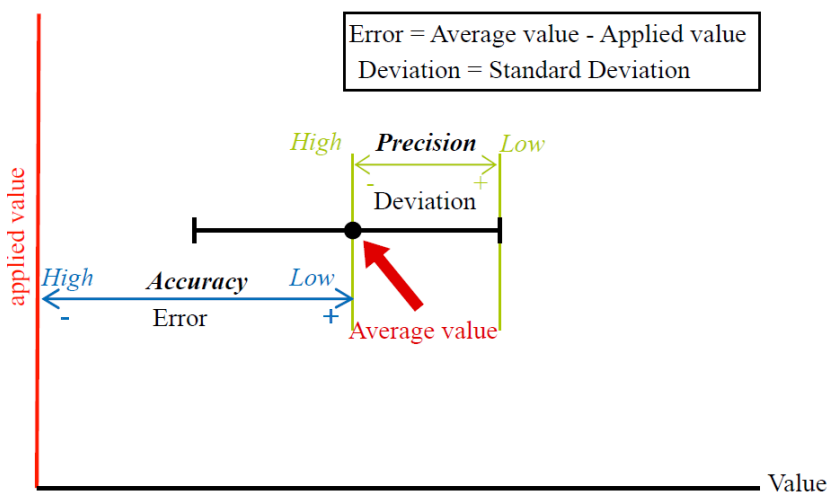


Figure 8: Definition of the terms “deviation”, “error”, “accuracy” and “precision”.

397 In order to quantify and discuss the results obtained using this new technique, several tests on
398 each configuration have been carried out in order to calculate the average value for each parameter
399 of the deviatoric tensor (orientations, stress ratio and differential stress, Table 2 and 3). About 20-30
400 tests were necessary to get the stability of the solution for monophasic datasets and 30-40 tests for
401 polyphase datasets. We define the precision of the technique as the degree to which successive tests
402 carried out under unchanged conditions yield the same results. The precision is quantified through
403 evaluation of the variability of the determined stress parameter values around the mean values over
404 the number of tests required to reach solution stability; it is called deviation hereinafter and is related
405 to reproducibility of the results (Fig.8). The lower the deviation, the higher the precision. We further
406 define the accuracy of the technique by the degree of closeness of the mean reconstructed stress
407 parameter to the true applied stress parameter. The accuracy is quantified by the error between the

408 mean stress parameter value and to the true applied value (Fig.8). The lower the error, the higher the
409 accuracy. Both error and deviation will be given either in absolute value or in percentage of the
410 applied value. As a result, we infer that the maximum methodological uncertainty associated with the
411 determination of each stress parameter (i.e., when the inversion technique is applied blindly by a
412 potential user to a naturally deformed sample) expectedly corresponds to \pm (error + deviation) as
413 derived from the results on numerically generated twin datasets. The error on the stress ratio will be
414 calculated on the maximum value of the stress ratio, i.e., 1; so that we get the same error percentage
415 for a given error whatever the applied stress ratio. For example, if the error value on the stress ratio
416 is 0.1 for an applied stress ratio of 0.5 or 1, the error percentage will be of 10% in both cases.

417 **3.6 Evaluation of the similarity of applied tensors**

418 The inversion process is expected to hardly detect and separate close tensors, because the
419 percentage of common twinned planes can be very high in this case. For instance, the examination of
420 the activated twinned planes, which are shared by both tensors with similar stress ratio but with σ_1
421 axes at 30° to each other, shows that, for a homogeneous grain size dataset, the degree (percentage)
422 of similarity increases with the differential stress applied and can almost reach 70% (Table. 4). In
423 order to test the ability of the technique to detect and separate close superimposed stress tensors, two
424 stress tensors with a deviation of 30° of the σ_1 axis were applied. In fact in tectonic studies, two tensors
425 with less than 30° difference in principal stress orientations may be considered as similar because of
426 cumulated inaccuracies on sample orientations and thin section making, measurement bias as well as
427 possible local natural reorientation of stress tensors in rocks. We also tested superimposed stress
428 tensors with perpendicular horizontal σ_1 axes (N-S and E-W) as well as stress tensors differing by
429 permutations of σ_2 and σ_3 stresses (which is a frequent situation encountered in regional paleostress
430 reconstructions).

Configuration	Tensor	σ_1	σ_2	σ_3	Φ	Δ_{1-3} (MPa)	Shared twinned planes (%)
1	T1	180/0	90/90	270/0	0,5	35	53,8
	T2	30/0	120/90	300/0	0,5	35	
2	T3	180/0	90/90	270/0	0,5	50	55,9
	T4	30/0	120/90	300/0	0,5	50	
3	T5	180/0	90/90	270/0	0,5	75	60,5
	T6	30/0	120/90	300/0	0,5	75	
4	T7	180/0	90/90	270/0	0	35	47,1
	T2	30/0	120/90	300/0	0,5	35	
5	T8	180/0	90/90	270/0	0	50	62,5
	T4	30/0	120/90	300/0	0,5	50	
6	T9	180/0	90/90	270/0	0	75	67,7
	T6	30/0	120/90	300/0	0,5	75	
7	T3	180/0	90/90	270/0	0,5	50	69,6
	T2	30/0	120/90	300/0	0,5	35	
8	T3	180/0	90/90	270/0	0,5	50	53,7
	T6	30/0	120/90	300/0	0,5	75	
9	T1	180/0	90/90	270/0	0,5	35	30,4
	T10	180/0	90/0	270/90	0,5	35	
10	T3	180/0	90/90	270/0	0,5	50	52,6
	T11	180/0	90/0	270/90	0,5	50	
11	T5	180/0	90/90	270/0	0,5	75	66,2
	T12	180/0	90/0	270/90	0,5	75	

Table 4: Evaluation of the degree of similarity between applied tensors. The table reports the maximum number of twin planes which are twinned by the two applied stress tensors for various stress configurations. These numbers are derived from 100 tests for each configurations. Φ is the stress ratio and Δ_{1-3} is the differential stress. Stress axis orientations are given in azimuth/dip ($^\circ$).

431 The similarity percentage is calculated by dividing the number of twinned planes shared by
432 both tensors by the number of planes twinned by the second tensor. This parameter is not symmetrical:
433 comparing A with B or B with A. It has been decided to compare the second tensor applied with the
434 first one because the first tensor can activate all the possible twin planes (depending on the equations
435 1 and 2) which is not the case for the second applied tensor (for which a strain hardening is applied).
436 The second tensor can therefore activate twinning on a lower number of twin planes than the first
437 applied tensor. It is this reason why the similarity criterion is calculated based on the second applied
438 tensor. The configuration with a permutation of σ_2 and σ_3 stress axes and the configuration with two
439 tensors the orientation of the maximum principal stresses of which differ by 30° are supposed to be
440 the most complex configurations in terms of tensor detection and separation. As mentioned before,

441 the percentage of similarities can reach 69.6% at high differential stress (configuration 7 in table1).
442 This is the reason why the critical percentage of similarities accepted by the process of tensor selection
443 in the new CSIT-2 inversion scheme is 70% by default. We consider that this value makes it possible
444 to differentiate most of the tensors belonging to different tectonic phases even in case of large
445 differential stresses, hence large percentages of similarities.

446 **4. Results**

447 **4.1 Monophase twin dataset**

448 In the following part, the tests start with the simplest case, a monophase dataset with
449 homogeneous grain size and no bias. Then, in order to simulate an increasing demand for the
450 technique, this dataset is then made heterogeneous in terms of grain size, and will further incorporate
451 virtual measurement bias. The basic stress configuration involves a N-S trending σ_1 axis and a E-W
452 trending σ_3 axis.

453 4.1.1 Monophase twin dataset with homogeneous grain size

454 The first tests were carried out using datasets with one applied tensor and one grain size (CRSS
455 = 10 MPa for all grains). A single orientation of principal stress axes was tested, but for this
456 configuration, different stress ratios (0, 0.5 and 1) and differential stresses (25 to 75 MPa) were
457 applied (configurations M1, M2, M3, M4, M5 and M6 in table 2).

458 Results from the inversion process show that the orientation of principal stress axes, stress
459 ratio and differential stress are well reconstructed (Figure 9). A slight discrepancy is observed for
460 differential stress magnitudes; the error however remains lower than 2.2 MPa (3%, Figure 9).

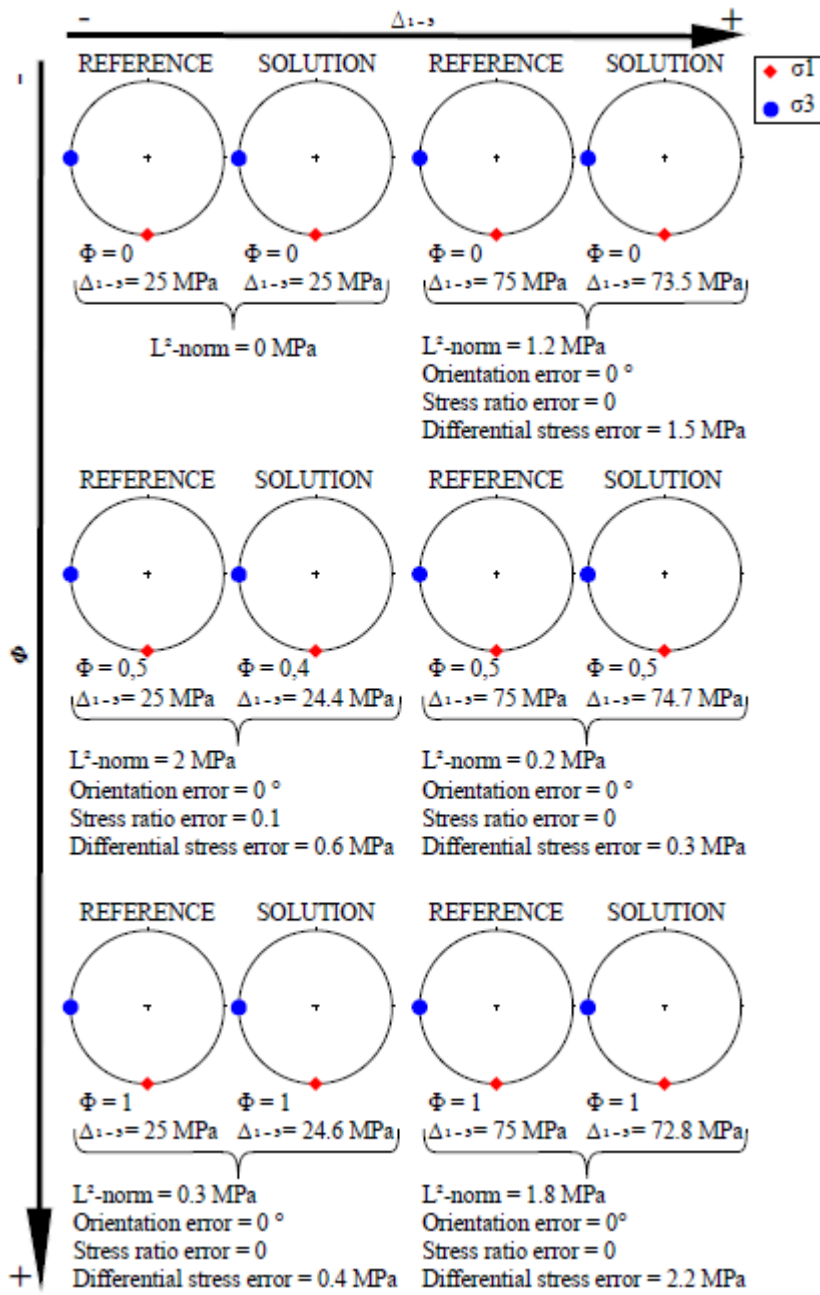


Figure 9: Results of inversion of numerically-generated monophasic datasets with homogeneous grain size (configurations M1 to M6 in table 2). Φ is the stress ratio and Δ_{1-3} is the differential stress in MPa. Total error is L^2 -norm. The error on the orientation is calculated using the scalar product between σ_1 axes of applied and solution tensors.

461 Additional tests were carried out following the same scheme but with a slight dispersion
 462 around the prevailing grain size (Gaussian distribution around a CRSS of 10 MPa, configurations M9,
 463 M10 and M12 in table 2). Results show that for the error (L^2 -norm) between the applied tensors and
 464 the solution tensors increases with the applied differential stress but remains very low and does not
 465 exceed 6 MPa (Fig. 10). The error on the orientation of principal stress axes is on average lower than
 466 4° with a deviation of $\pm 2^\circ$ (Fig. 10). For the stress ratio and the differential stress values the error is
 467 close to zero with a very low deviation (Fig.10).

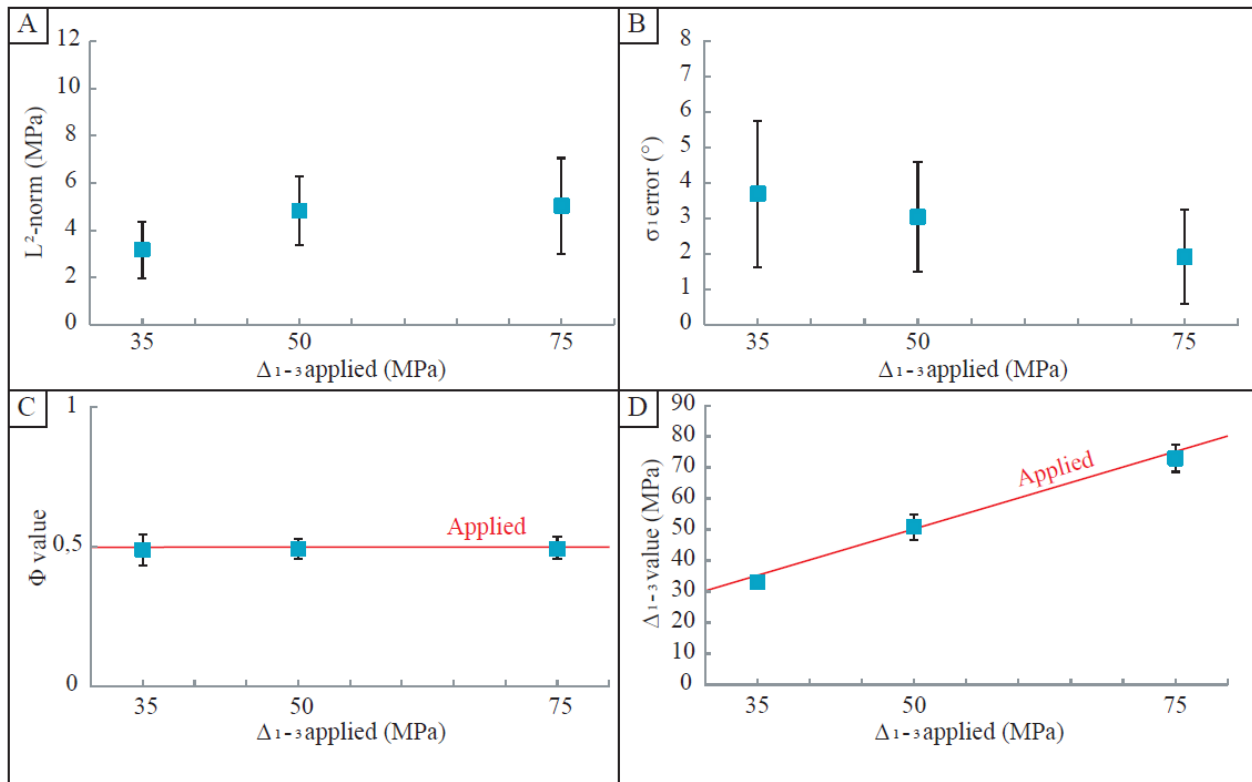


Figure 10: Inversion results of numerically-generated monophasic datasets M9, M10 and M12. The graphs show A) the results of the L^2 -norm error and deviation between the applied tensor and the solution tensor, B) the error and deviation on the σ_1 orientations, C) the deviation of stress ratio values with the mean value and D) the deviation differential stress values with the mean value. The red line represents the reference (applied) stress ratio and differential stress values.

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4.1.2 *Monophasic twin dataset with heterogeneous grain size*

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Datasets with virtually heterogeneous grain sizes are simulated using two separate CRSS values. These values are 5 MPa (2/3 of grains) and 15 MPa (1/3 of grains) (configurations M7 and M8 in table 2). However, the 10 MPa value of the CRSS was still blindly considered for the inversion process, in order to test the robustness of the technique with respect to significantly varying grain sizes in an aggregate. Figures 11A and B show the application of inversion process for applied tensors with variable differential stress of 50 MPa and 75 MPa and two perfectly distinct grain sizes. The solution tensor is nearly similar to the applied tensor for 50 MPa, whereas it differs more importantly from the applied tensor with 75 MPa, especially in terms of differential stress. According to Yamaji (2015), there is a loss of information on the differential stress value given by the inversion if this value is greater than 50-100 MPa. For these applied tensors, we further tested a constant virtual CRSS

479 not equal to 10 MPa but which instead corresponds to the CRSS applied for each grain size weighted
 480 by the number of grains with each size class. The results are worse in terms of differential stresses
 481 (43.2 MPa instead of 50 MPa or 41.7 MPa instead of 75 MPa). This confirms that a good estimate of
 482 the CRSS value does not depend solely on the average of CRSS values on measured grains but also
 483 of the spatial distribution of twinned planes consistent with the applied tensor.

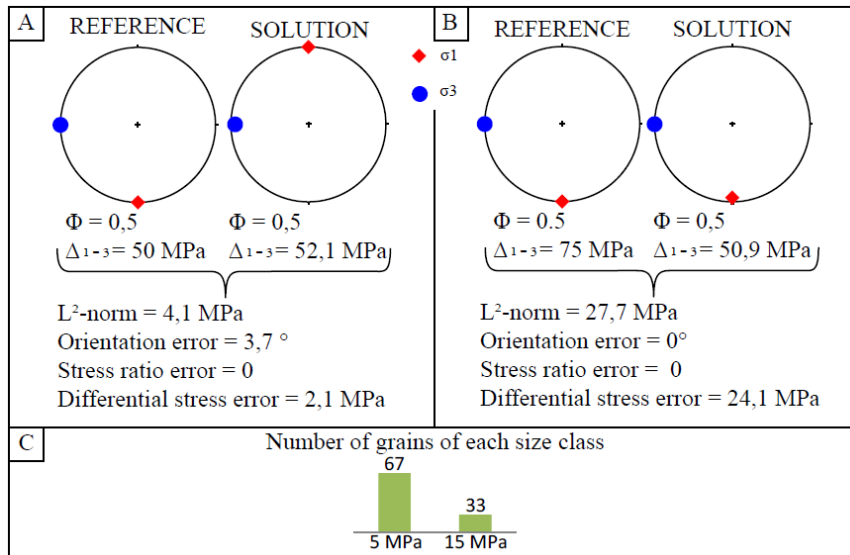


Figure 11: Inversion results of numerically-generated-monophase datasets A) M7 and B) M8 (Table 2). C) Histogram showing the number of grains of each size class used during simulation.

484 Datasets with a slight (pseudo-Gaussian type) dispersion within the two considered grain size
 485 classes are further considered (configurations M12, M13 and M14 in table 2). The error (L^2 -norm) is
 486 lower than 5 MPa but increases with the differential stress, reaching the value of 8 MPa. There is
 487 therefore a loss of information about the whole 5 parameters of the tensor around 75 MPa of
 488 differential stress (Fig. 12A). In details, regarding the principal stress orientations and stress ratio,
 489 they are well found, and the related errors do not increase with increasing applied differential stress
 490 (Fig. 12B and C). The error on the differential stress is of 0-1 MPa (1-3% of the applied value) below
 491 50 MPa and of 3 MPa (4%) at 75 MPa (Fig. 11). The deviation is of ± 1 -2 MPa (4-5%) for differential
 492 stress below 50 MPa but increases for differential stress at 75 MPa (± 7 MPa / 9%). Compared with
 493 the previous results dealing with a single grain size class, both deviations and errors are higher,
 494 especially on the differential stress value. This is mainly due to the grain size dependence of the CRSS
 495 that has not been considered here since a 10 MPa value for the CRSS has been blindly used to

496 calculate differential stress irrespective of the heterogeneous grain size.

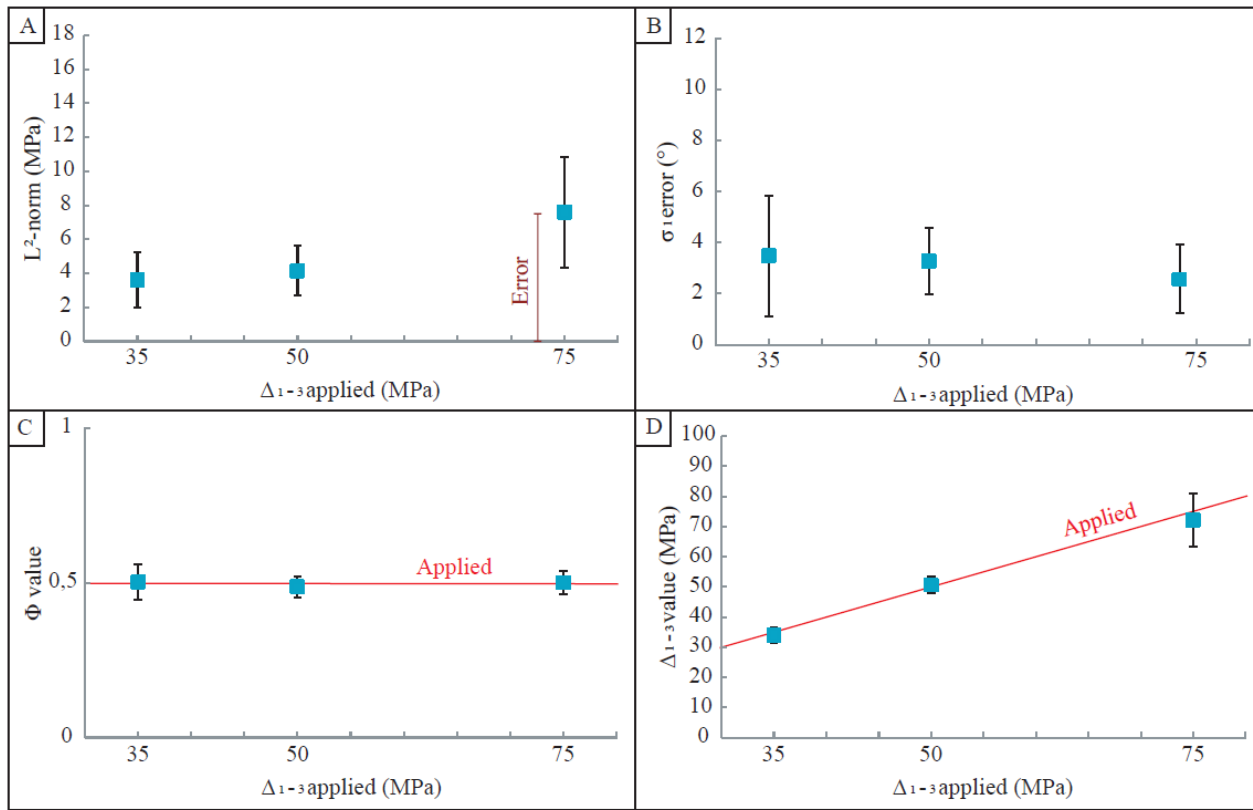


Figure 12: Inversion results of numerically-generated monophasic datasets M12, M13 and M14 (Table 2). A, B, C and D same key as in figure 10.

497 Separating the datasets into virtual homogeneous grain size classes strongly improves the
 498 results as shown by the tests on datasets with homogeneous grain size. Thus, as discussed later, it is
 499 of first importance to carry out inversion only after the dataset has been divided into nearly
 500 homogeneous grain size classes, each corresponding to a given value of the CRSS. This is the reason
 501 why all the tests shown hereinafter are only performed on datasets corresponding to a homogeneous
 502 grain size (pseudo-Gaussian dispersion around a single CRSS value of 10 MPa).

503 4.1.3 *Monophasic twin dataset with homogeneous grain size and optical bias*

504 In order to test the effect of an increasing bias, 10% or 25% of twinned planes have been
 505 randomly changed into untwinned planes. Results are presented in figure 13. Each point corresponds
 506 to the result of 20-30 tests. A stress ratio of 0.5 and a differential stress of 50 MPa are imposed
 507 (configurations M15 and M16 in table 2). The error (L²-norm) for 10% or 25% of incorporated bias

508 are very similar (Fig. 13A) but with a larger deviation for the results with 25% of bias. If the
 509 parameters of the deviatoric stress tensor are considered one by one, the principal stress orientations,
 510 stress ratio and differential stress are very similar to those of the applied tensor. Thereby, the error on
 511 σ_1 orientation is of 3° with an deviation of $\pm 2^\circ$ (Fig. 13B), there is a negligible error (<0.01) for the
 512 stress ratio but an deviation of less than ± 0.1 (10%) (Fig 13C), and a very slight error (< 2 MPa) on
 513 differential stress values with an deviation of about 10% or less (Fig. 13D).

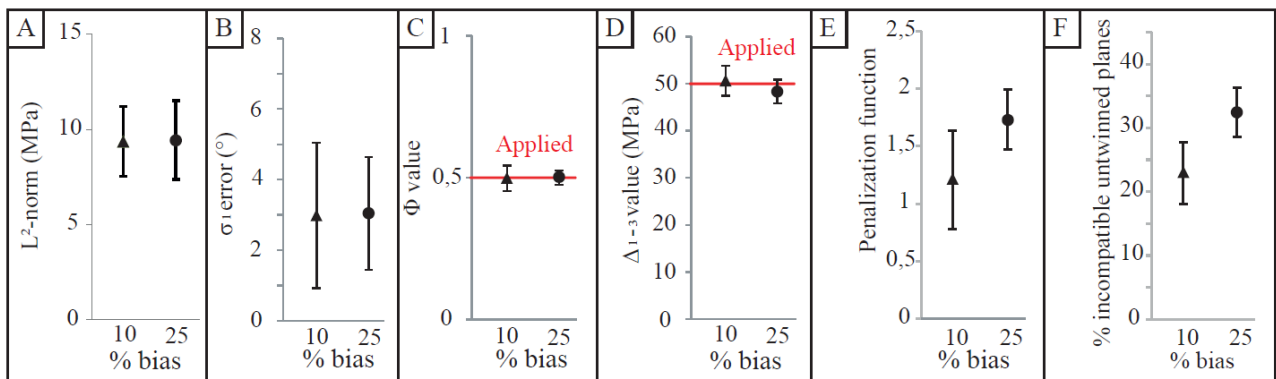


Figure 13: Inversion results of numerically-generated monophasic datasets M15 and M16 (Table 2). A, B, C and D same key as in figure 10.

514 Figure 13E and F show that with 10% and 25% bias, a solution tensor with a low error (L^2 -
 515 norm) is found to the cost of an increase of the penalization function and also of the incorporation of
 516 incompatible untwinned planes with the increase of the incorporation of bias. For the tests with 25%
 517 of bias, the solution have been determined on the basis of the breaks in slope of curves as previously
 518 discussed, but the values for the penalization function and the percentage of incompatible untwinned
 519 planes in the solution are greater than the one for 10% or even 0% of incorporated bias. This means
 520 that compared to the 0% bias configuration M10 a larger tolerance threshold toward increasing
 521 penalization function value for 10% or 25% of bias explains the similar values for the L^2 -norm.

522 4.2 Polyphase calcite twin dataset

523 4.2.1 Polyphase twin dataset with homogeneous grain size, no bias and different stress ratio

524 Results are shown for polyphase cases with two applied tensors (configurations B18 then B21,
 525 B19 then B22 and B20 then B23 in table 3) and with a Gaussian distribution of grain sizes (centered

526 on 10 MPa). The first applied tensor is a N-S compression with an E-W extensional part (σ_1 : N180-
527 0; σ_3 : N270-0) with a stress ratio of 0.3. The second applied tensor is turned of 30° between σ_1 axes
528 (σ_1 : N30-0; σ_3 : N300-0) with a stress ratio of 0.7. These tensors have been applied on twin data for
529 an increasing differential stress (35, 50 and 75 MPa) (Fig. 14A). The results of the CSIT-2 inversion
530 on these 3 configurations show that there is a loss of information with increasing differential stress
531 (Fig. 14B). Figure 14C shows that the orientation of the two applied tensors are well recovered with
532 an error of $4-7^\circ$ (and a deviation of $2-3^\circ$) for both tensors. The error on the stress ratio for the first
533 tensor is negligible (< 0.1) with a deviation of $\pm 0.03-0.05$ ($\pm 3-5\%$) (Fig. 14D). For the second tensor,
534 the error on the stress ratio is of $0.06-0.13$ (6-13%) with a deviation of $\pm 0.04-0.06$ ($\pm 4-6\%$). The
535 differential stress is well retrieved with an error of $0.05-2$ MPa (0.15-6.5%) with a deviation of $\pm 1-2$
536 MPa ($\pm 2.9-5.7\%$) for low applied differential stress (< 50 MPa) and of $\pm 5-6$ MPa ($\pm 6-8\%$) for an
537 applied differential stress of 75 MPa (Fig. 14E). These results show that CSIT-2 is able to identify
538 and separate superimposed stress tensors with very different stress ratios. Figure 14D shows that with
539 increasing differential stress there is no loss of accuracy but a loss in the precision of the results.

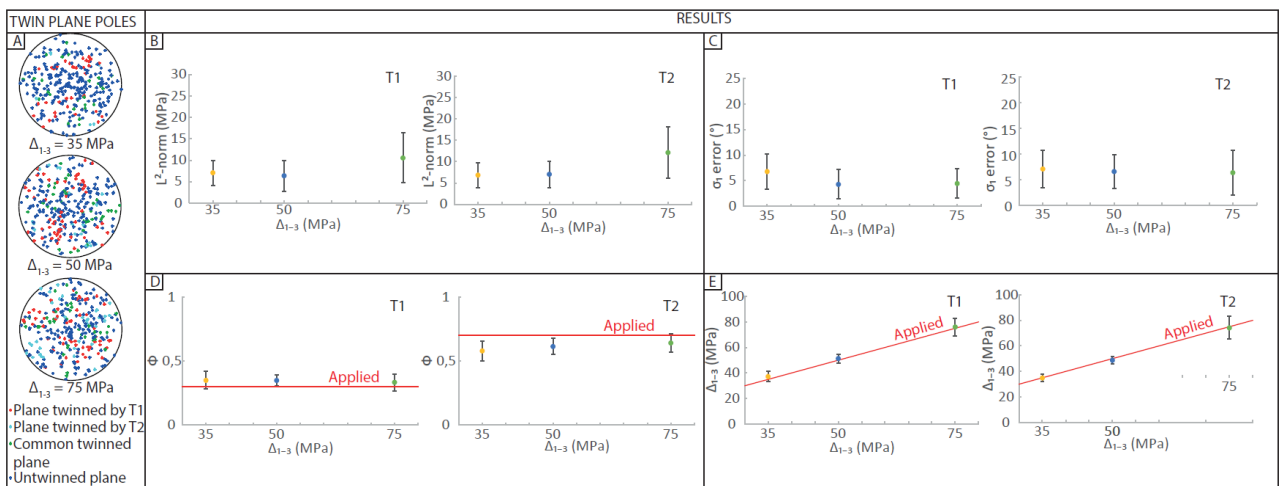


Figure 14: Inversion results of numerically-generated polyphase datasets B18 then B21, B19 then B22 and B20 then B23 configurations (Table 3). A) Wulff stereo-diagrams (lower hemisphere) of twin plane poles generated for the three configurations described previously. The graphs show the results of the inversion with B) the results of the L^2 -norm error and deviation between the applied tensor and the solution tensor, C) the error and deviation on the σ_1 orientations, D) the deviation of stress ratio values with the mean value and E) the deviation differential stress values with the mean value. The red line represents the reference (applied) stress ratio and differential stress values.

540 4.2.2 Polyphase twin dataset with homogeneous grain size and optical bias

541 Results for polyphase cases with a difference of 30° between σ_1 axes of both tensors are
 542 summarized in figure 15 (configurations B1 then B3 and B2 then B4 in table 3). The distribution of
 543 grain size (i.e. CRSS value) is a pseudo-Gaussian, centered on a CRSS value of 10 MPa. The stress
 544 ratio and the differential stress are the same for both tensors, that is, $\Phi = 0.5$ and $\Delta_{1-3} = 50$ MPa.
 545 Figure 15B shows that, for the first tensor applied the error is of 9-11 MPa for the L^2 -norm with 10
 546 or 25% of optical bias. Adding optical bias (10-25%) has almost no impact on the differential stress
 547 parameter. For the second tensor, the error (L^2 -norm) is about 10 MPa. The first tensor has an error
 548 of 6° on the orientation of principal stress axes with a deviation of $\pm 2-3^\circ$ (Fig. 15C). The second
 549 tensors has an error of $7-8^\circ$ on the principal stress orientations with a deviation of $\pm 2-3^\circ$ (Fig. 15C).
 550 The accuracy for the second tensor is slightly lower than for the first one. The error on the stress ratio
 551 parameter is of 0-0.03 (3%) with a deviation of $\pm 0.03-0.09$ (3-9%) for both tensors (Fig. 15D). The
 552 error on the differential stress parameter is of 1-7 MPa (2-14%) with a deviation of ± 5 MPa (10%)
 553 for both tensors (Fig. 15E). The different parameters of the stress tensors are fairly well estimated.

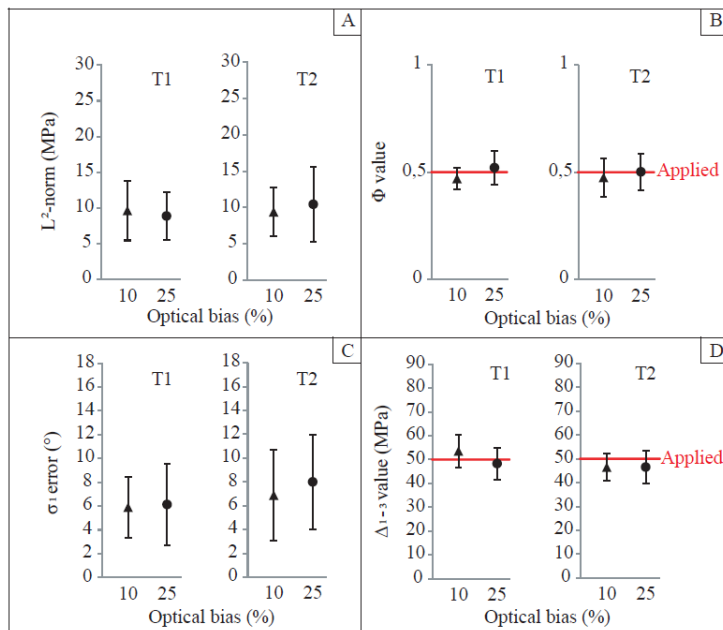


Figure 15: Inversion results of numerically-generated polyphase datasets applying B1 and B3 configurations then B2 and B4 configurations (Table 3). A) the results of the L^2 -norm error and deviation between the applied tensor and the solution tensor, B) the error and deviation on the σ_1 orientations, C) the deviation of stress ratio values with the mean value and D) the deviation differential stress values with the mean value. The red line represents the reference (applied) stress ratio and differential stress values.

554 As for the monophase tests with the increasing percentage of bias incorporation, CSIT-2 shows
 555 similar results in terms of L^2 -norm error for 10% or 25% of incorporated bias. A more important
 556 incorporation of incompatible untwinned planes and an increase of the penalization function value

557 are accepted. Thus a value of 10% of bias will only be tested hereinafter.

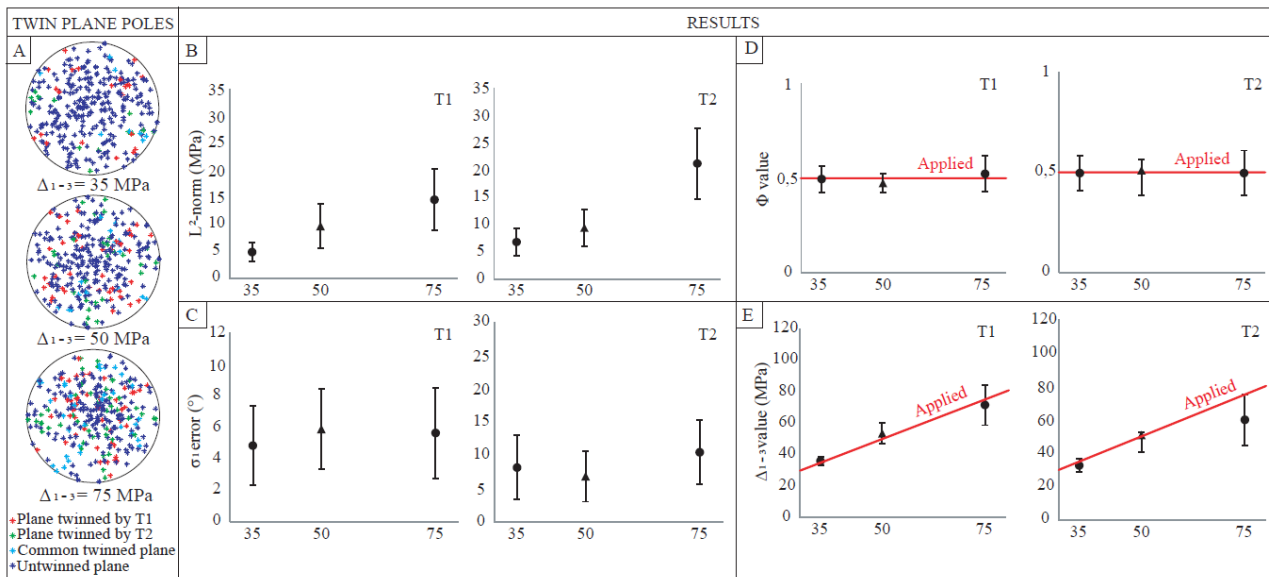


Figure 16 : Inversion results of numerically-generated polyphase datasets applying B5 then B7, B1 then B3 and B6 then B8 configurations (Table 3). A, B, C, D and E same key as in figure 14.

558 Having in mind the expected loss of information related to high applied differential stress, the
 559 influence of the differential stress on the result of the inversion process was then tested. The applied
 560 parameters are two stress tensors with 30° of difference in orientation of the σ_1 axes, a stress ratio of
 561 0.5 and 10% of optical bias (configurations B5 then B7, B1 then B3 and B6 then B8 in table 3). Three
 562 differential stresses are tested: 35, 50 and 75 MPa. Results show that the error increases with the
 563 applied differential stress (Fig. 16B). The error on the orientation of σ_1 (Fig. 16C) is of less than 6°
 564 (with a deviation of $\pm 2^\circ$) for the first tensor and of 10° (with a deviation of $\pm 5^\circ$) for the second tensor.
 565 The error on the stress ratio value is close to zero ($< 10^{-1}$) for both tensors and the deviation is of \pm
 566 0.1 (10%) (Fig. 16D). The error on the differential stress value is of 1-3 MPa (3-8%) for the first
 567 tensor and the deviation is of 2-10 MPa (6-13%) (Fig. 16E). For the second tensor with an applied
 568 differential stress lower or equal to 50 MPa the error is of 2-3 MPa (7%) with a deviation of ± 3 -5
 569 MPa (9%) (Fig. 16E). At 75 MPa, the error increases for the second tensor. This error is of -15 MPa
 570 (-20%) for a deviation of ± 13 MPa (21%) (Fig. 16E). Looking at the different stress parameters, the
 571 differential stress is the less constrained parameter. For the second tensor applied, there is a strong

572 error for the last tests with a clear underestimate of the differential stress. This last observation concurs
 573 with the results of Yamaji's (2015b) study.

574 The influence of the differential stress on the results of the inversion process is also tested on
 575 the following cases with two tensors with σ_1 and σ_3 axes rotated by 90° (configurations B5 then B12,
 576 B1 then B13 and B6 then B14 in table 3). Figure 15 shows the L^2 -norm variation with various applied
 577 differential stress: 35, 50 and 75 MPa and a stress ratio of 0.5 for both tensors. For both tensors, a
 578 similar trend is observed with an increase of the average L^2 -norm value (the error) up to 75 MPa of
 579 applied differential stress and of the deviation (Fig. 17B). For principal stress orientations (Fig. 17C),
 580 the error remains the same for both tensors and even with increasing differential stresses (of about 2-
 581 4°) with a slight deviation of $\pm 1^\circ$. The error on the stress ratio is the lowest (Fig. 17D), as well as for
 582 the associated deviation. Figure 17E also indicates that inversion provides a very good estimate of
 583 the differential stress until 50 MPa. There is an increase of the error between 50 and 75 MPa for both
 584 tensors which can be estimated approximately at -6 MPa (-10 MPa for the second tensor) with a very
 585 slight deviation of ± 5 MPa (7%).

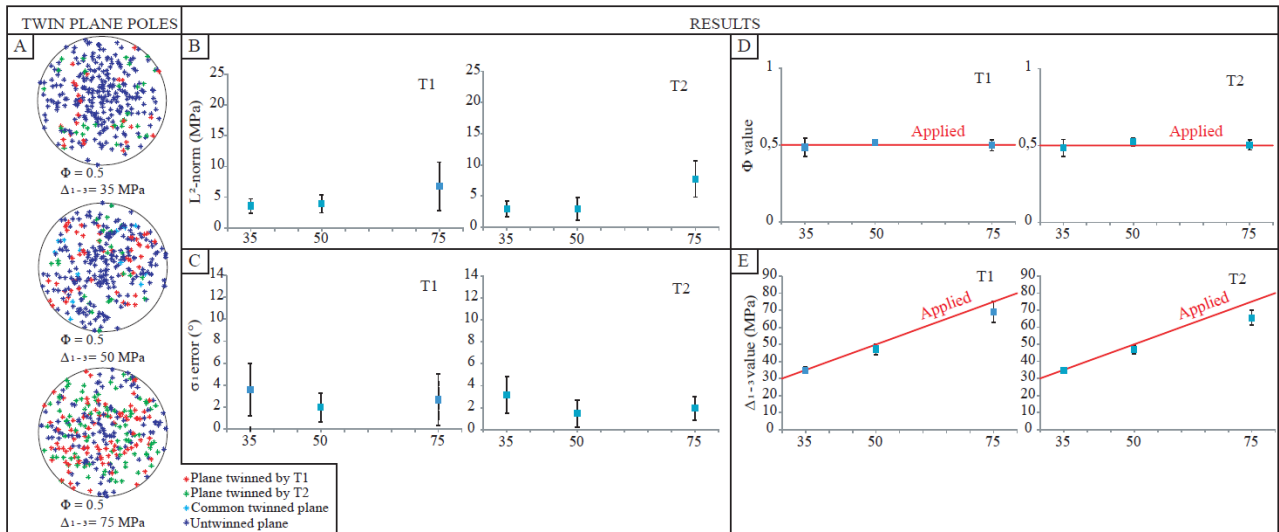


Figure 17: Inversion results of numerically-generated polyphase datasets applying B5 then B9, B1 then B10 and B6 then B11 configurations (Table 3). A, B, C, D and E same key as in figure 14.

586 Other tests have been carried out for polyphase datasets with superimposed stress tensors (Fig.
 587 18A) with similar σ_1 axes, stress ratio (0.5) and differential stress (35, 50 or 75 MPa) but with a

588 permutation of σ_2 and σ_3 axes (configurations B5 then B12, B1 then B13 and B6 then B14 in table 3).
 589 The error (L^2 -norm) is the same for both tensors (less than 10 MPa) and is stable with increasing
 590 differential stress (Fig. 18B). The error on principal stress orientation is low (Fig. 18C), less than 5°
 591 for both tensor and the deviation is about ± 2 - 3° . The error on the stress ratio (Fig. 18D) is decreasing
 592 with increasing differential stress and the same for the deviation. The differential stress is perfectly
 593 found with an error of 0 MPa and a deviation of less than ± 5 MPa (7%) (Fig. 18E).

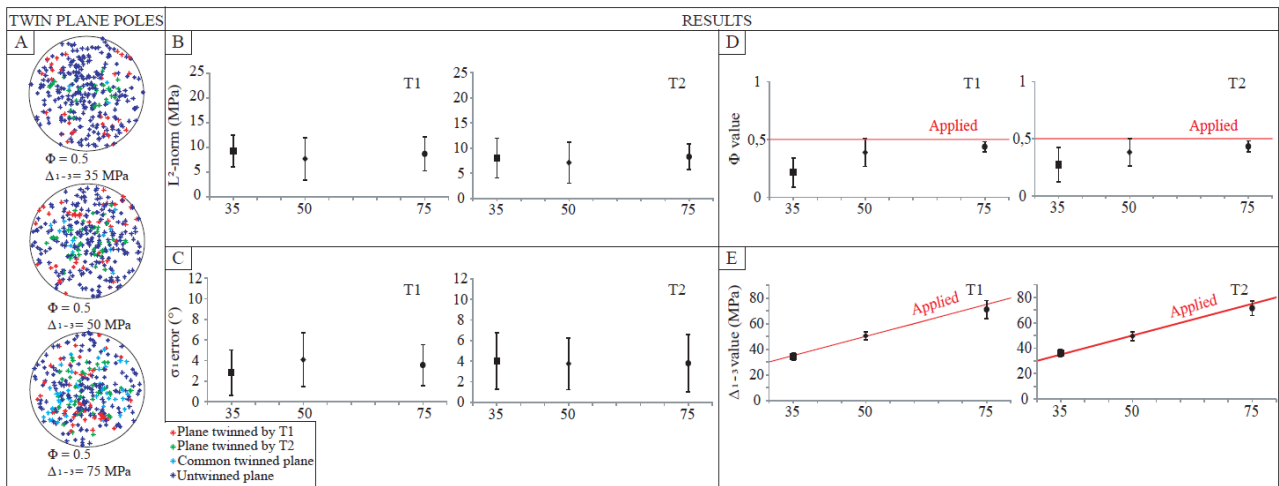


Figure 18: Inversion results of numerically-generated polyphase datasets applying B5 then B12, B1 then B13 and B6 then B14 configurations (Tables 3). A, B, C, D and E same key as in figure 14.

594 Additional tests were carried out to evaluate the effect of a difference of stress ratio between
 595 both applied tensors (configurations B5 then B15, B1 then B16 and B6 then B17 in table 3) (Fig.
 596 19A). The first tensor has a N-S compression with an E-W extensional part and a stress ratio of 0.
 597 The second tensor has been rotated with respect to the first tensor by 30° and corresponds to a stress
 598 ratio of 0.5. Results show that the total error (L^2 -norm) is increasing with the applied differential
 599 stress and the same for the deviation (Fig. 19B). For principal stress orientation, the error is of 4 - 7°
 600 for a deviation of ± 3 - 4° for both tensors (Fig. 19C). The stress ratio is very well reconstructed with
 601 a negligible error ($< 10^{-2}$) and a negligible deviation for the first tensor and an error of -0.1 (-10%)
 602 and a deviation of less than ± 0.1 (10%) for the second tensor (Fig. 19D). The differential stress is
 603 well retrieved by the inversion process but there is a slight increase of the deviation width for both
 604 tensors and a slight error for the second tensor with an applied differential stress of 75 MPa (Fig.

605 19E). The error is of 1-7 MPa (2-14%) with a deviation of $\pm 2-3$ MPa (5-7%) for differential stress
 606 below or equal to 50 MPa and about 9-10 MPa (12-14%) of error with a deviation of $\pm 6-7$ MPa (8-
 607 9%) for applied differential stress values of 75 MPa.

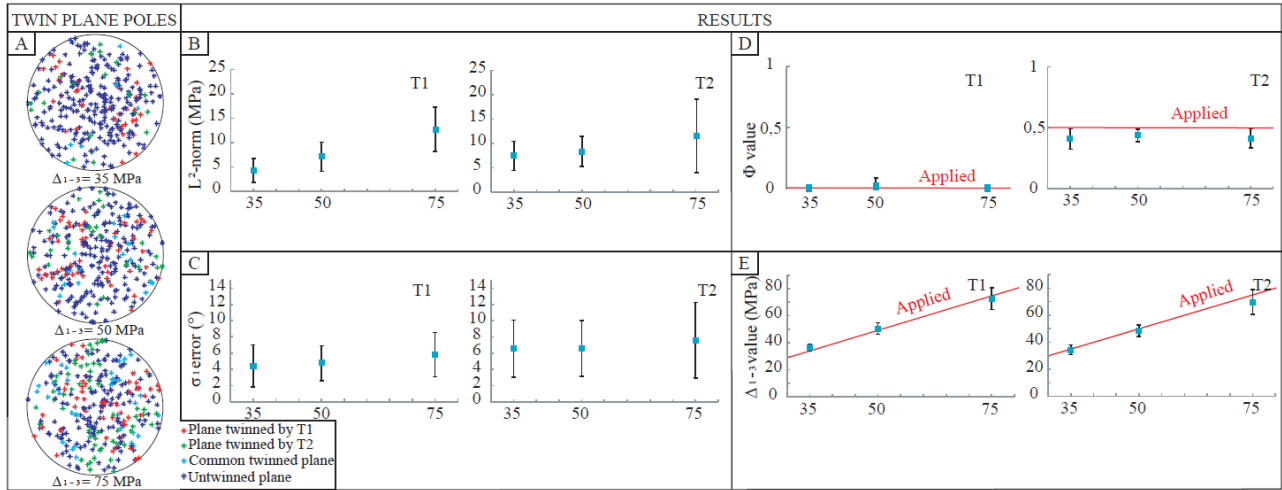


Figure 19: Inversion results of numerically-generated polyphase datasets of B5 then B15, B1 then B16 and B6 then B17 configurations (Table 3). A, B, C, D and E same key as in figure 14.

608 In the last tests the ability of the method to differentiate two tensors with a same value of stress
 609 ratio but varying differential stresses is tested (Fig. 20). Thus, the first tensor with a N-S trending σ_1
 610 has a differential stress of 50 MPa and the second tensor with N30° trending σ_1 has a differential
 611 stress of 35 or 75 MPa (configurations B1 then B7 and B1 then B8 in table 3). Tensors are very close
 612 and these configurations are the most difficult in terms of separation because of the overlap of twin
 613 data explained by the two tensors. As previously, the distribution of grain sizes (i.e. CRSS value) is a
 614 pseudo-Gaussian centered on a CRSS value of 10 MPa (Fig. 20B & B'). Figure 20B & B' show the
 615 distribution of shared twinned planes of both tensors. It can be observed that there is a higher number
 616 of shared twinned planes in figure 20B' than in figure 20B where the differential stress of the second
 617 tensor equals 75 MPa. This is explained by the fact that both tensors are very close and an increase
 618 of the differential stress value increases the number of common twinned planes (progressively
 619 overlapping spherical caps in the sense of Yamaji, 2015a). Figure 20A & A' show that the principal
 620 stress orientations and stress ratio are well estimated but, as observed previously, there is an increase
 621 of error on the differential stress value for the second tensor at high differential stress (Fig. 20A').

622 For the configuration shown in figure 20A, the error is of 4-7° with a deviation of ± 2-3° for principal
 623 stress orientations, less than 0.1 (10%) for the stress ratio, 1-3 MPa (2-8%) with a deviation of ± 2-3
 624 MPa (4-8%) for the differential stress. For the configuration shown in figure 20A', the error is of 6°
 625 with a deviation of ± 2° for principal stress orientations, 0.02 (2%) for the stress ratio and about 2-5.5
 626 MPa (4-7 %) with a deviation of ± 3-5 MPa (6-7%) for the differential stress.

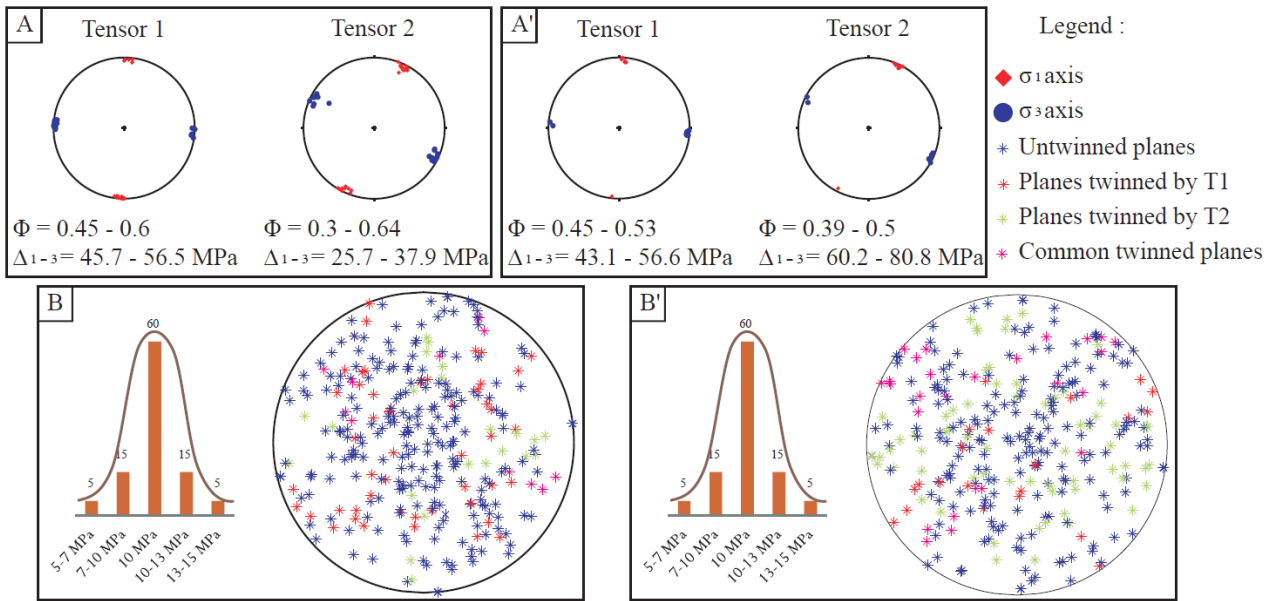


Figure 20 : Inversion results of numerically-generated polyphase datasets B1 then B7 and B1 then B8 configurations (Table 3). A and A') Results of the inversion for each configuration. B and B') Histograms of the repartition of grain sizes and an example of stereographic projection (Wulff lower hemisphere) of twinned/untwinned plane poles.

627 5. Interpretation and discussion of the results of inversion of numerically 628 generated datasets using CSIT-2

629 5.1 Overall efficiency of CSIT-2 to determine paleostress from monophase and 630 polyphase datasets

631 5.1.1 Determination of the principal stress orientations

632 For monophase datasets with a perfectly homogeneous grain size principal stress orientations
 633 are fully retrieved (Fig. 9). When a slight dispersion around the mean grain size is added, the average
 634 error is about 4° with a deviation of ± 2° (Fig. 10). The error increases with two distinct grain sizes

635 of about 4° (by considering a constant CRSS value of 10 MPa) (Fig. 11). With two distinct grain size
636 classes with a pseudo-gaussian distribution, the error on the principal stress orientations is the same
637 than previously (Fig. 12). The same observations can be made for the results of dataset inversion with
638 a bias incorporation of 10 or 25% (by randomly changing twinned planes into untwinned planes) (Fig.
639 13). A slightly larger deviation in the principal stress orientations is observed with an increase of bias
640 incorporation in datasets (25%). Thus, CSIT-2 can accurately and precisely reconstruct principal
641 stress orientations from monophasic datasets in all configurations even with a high incorporation of
642 bias.

643 As a result, for a naturally deformed monophasic sample with homogeneous grain size, the
644 methodological uncertainty associated with the determination of principal stress orientations does not
645 exceed $\pm 8^\circ$.

646 For polyphase datasets with one grain size class, the determination of the principal stress axes
647 is also accurate and precise, the maximum error reaching 10° on average with a maximum deviation
648 of $\pm 5^\circ$ (Fig. 14-20). This higher error compared to monophasic datasets is due to the fact that CSIT-
649 2 (as for CSIT) is able to estimate parameters of the stress tensor (orientations of principal stress axes
650 and stress ratio) while the fifth parameter (non-dimensional differential stress) is found later by
651 considering a constant CRSS value of 10 MPa. In the cases of datasets with different grain sizes,
652 applied tensors may consequently not cause twinning of some favorably oriented twin planes. These
653 planes therefore act as misclassified twinned planes (e.g., bias) during the inversion process. In fact,
654 small grains have a higher CRSS value and the applied resolved shear stress value may thus be too
655 low to cause twinning along them. This can slightly affect the determination of principal stress
656 orientation.

657 The incorporation of bias in monophasic and polyphase datasets makes it slightly more difficult
658 to accurately and precisely determine principal stress orientations (Fig. 13 and 15). This is due to the
659 strong influence of the penalization function in the choice of the tested tensors. If the penalization

660 function value exceeds 0.5, the tensor is not selected (see section 3.2). Depending on the orientation
661 of untwinned planes with respect to the tensor, this value can exceed 0.5, leading to an error on
662 principal stress orientations. The error on principal stress orientations is of 6° and 10° for the first and
663 the second tensors when they differ of 30° in the orientation of principal stress axes with a deviation
664 of $\pm 5^\circ$ (for 10% bias).

665 Gagala (2009) stated that the CSIT was not able to separate very close tensors. In contrast,
666 CSIT-2 makes it possible to unambiguously and reliably reconstruct superimposed tensors with only
667 30° of difference between σ_1 axes, hence with a high percentage of shared twinned planes.

668 The orientations of the principal stress axes are thus the best constrained parameters, because
669 the 3D spatial orientation of twinned planes provides strong constraints on possible orientations of
670 stress axes. This observation was the basis of the Turner's (1953) analysis of calcite twins.

671 In nature it is very rare to have a sample having recorded just one phase (one applied tensor).
672 Thus, the user will be more interested by the accuracy for polyphase cases (two or more applied
673 tensors). If the tensors are very close in principal stress orientations (i.e. 30° rotation between
674 principal stress axes between both tensors), the error is 10° with a deviation of $\pm 5^\circ$ (Fig. 14-16). Thus,
675 the maximum uncertainty in calculated principal stress orientations is $\pm 15^\circ$. For cases with very
676 different applied tensors in term of orientations (i.e. around 90° rotation between principal stress axes
677 between both tensors), the error is 4° with and deviation of $\pm 2^\circ$, hence the maximum uncertainty is
678 $\pm 6^\circ$ (Fig. 17). In the case of $\sigma_2 - \sigma_3$ stress permutation between both applied tensors the error is 4°
679 with a deviation of $\pm 4^\circ$, so the maximum uncertainty is therefore $\pm 8^\circ$ (Fig. 18).

680 As a result, the maximum methodological uncertainty associated with determination of
681 principal stress orientations from a naturally deformed sample with an homogeneous grain size using
682 CSIT-2 can be considered $\pm 15^\circ$; the usual uncertainty is expected to be about $\pm 10^\circ$.

683 5.1.2 Determination of the stress ratio

684 In general, the stress ratio is accurately and precisely retrieved in monophasic and polyphasic
685 datasets, with bias of 10 or 25% and high differential stress (Fig. 13 and 15).

686 For monophasic cases, the error is negligible with a deviation of ± 0.04 , so the maximum
687 uncertainty for monophasic cases is ± 0.04 (4%) on the stress ratio value. For polyphasic cases with
688 30° of difference between principal stress axes of the two applied tensors, the error is of 0.03 (3%)
689 with a deviation of ± 0.08 (8%), so the maximum uncertainty is of ± 0.1 (10%). For tensors with
690 90° of difference between principal stress axes the error is of 0.02 (2%) with a deviation of ± 0.05
691 (5%), so the maximum uncertainty is of ± 0.07 (7%). For all these configurations CSIT-2 is very
692 accurate and precise for the stress ratio determination. For tensors with a permutation of σ_2 and σ_3
693 axes, the error is expectedly higher, 0.3 (30%) for low differential stress and decrease until 0.07 (7%)
694 for high differential stress with a deviation of ± 0.1 (10%). This last configuration is the most difficult
695 one because at low applied differential stress the number of shared twinned planes is very high and
696 the program will tend to find one tensor with an extreme value of stress ratio. Extreme stress ratio
697 values (in practice $\Phi = 0$) make it possible to take into account more twinned planes for two tensors
698 with similar σ_1 axes. With increasing differential stress, the percentage of shared twinned planes
699 between tensors decreases and allows to more accurately and precisely find the stress ratio values.

700 As a result, the maximum methodological uncertainty associated with the determination of
701 the stress ratio from a naturally deformed sample with an homogeneous grain size using CSIT-2 can
702 be considered ± 0.4 (40%); the usual uncertainty is expected to be about ± 0.1 (10%).

703 5.1.3 Determination of differential stress magnitudes

704 In monophasic datasets with one grain size class and no bias (Fig. 9-10), differential stresses
705 are retrieved with a deviation that does not exceed 3 MPa. The loss of information on the
706 determination of differential stress, when the applied stress is greater than 50 MPa as highlighted by
707 Yamaji (2015a), is not observed (maximum error of 2 MPa for an applied differential of 75 MPa).
708 However, this effect is clearly observed with monophasic datasets with two different grain size classes

709 (see §5.3) or with polyphase datasets (Fig. 11-12).

710 It is noticeable that, among the 5 parameters of the deviatoric stress tensor, the differential
711 stress is clearly the less constrained parameter. This is mainly due to the sensitivity of the CRSS to
712 grain size and to the difficulty to take this effect into account. The error may reach 20% in polyphase
713 cases at high applied differential stresses. Results from monophasic datasets show a good estimate of
714 the differential stress compared to polyphase datasets. For differential stress lower than 50 MPa the
715 error does not exceed 2 MPa for monophasic datasets without bias. The results of the analysis of
716 monophasic datasets with two grain size classes point toward the need for dividing the dataset into
717 subsets of homogeneous grain sizes before inversion in order to better estimate the differential stresses.

718 In polyphase cases with one grain size class and incorporation of 10% of bias, the maximum
719 misfits on the differential stress value is observed at high applied differential stress (75 MPa). This
720 occurs in all cases except for the configuration with a rotation of 90° (Fig. 18) of the principal stress
721 axes. This configuration gives the most accurate and precise values for all parameters of the deviatoric
722 stress tensors (regarding polyphase cases). For cases with two applied tensors with a difference of
723 principal stress orientation of 30°, the error is of 1-6 MPa (12%) for applied differential stress equal
724 or below 50 MPa and of 3-15 MPa (20%) above 50 MPa (Fig. 16). The deviation can reach $\pm 2-9$
725 MPa (18%) in the worst cases for differential stress applied equal or below 50 MPa and $\pm 10-13$ MPa
726 (17%) above 50 MPa applied.

727 As a result, the maximum methodological uncertainty associated with determination of
728 differential stresses from a naturally deformed sample with a homogeneous grain size using CSIT-2
729 can be considered $\pm 37\%$; this rather high value is expected for high differential stresses. The usual
730 uncertainty is expected to be about $\pm 25-30\%$.

731 **5.3 Influence of heterogeneous grain size**

732 Several configurations of grain sizes have been tested in order to determine the robustness of
733 CSIT-2 to varying grain sizes. As observed when dealing with monophasic datasets, a high variability

734 of grain sizes does not affect the accuracy of the determination of principal stress orientations or stress
735 ratio. However, and especially in the case of two grain size classes (Fig. 11-12), there is a loss of
736 information for differential stresses. This loss is higher at high differential stress. This is due to the
737 application of a constant CRSS value of 10 MPa for all grains. As mentioned previously, several
738 authors concurred to say that the CRSS value is strongly grain size dependent (Newman, 1994; Rowe
739 and Rutter, 1990). Thus, the CRSS value has to be adapted for each grain size. The main problem is
740 our poor knowledge regarding the evolution of the CRSS value with grain size.

741 Principal stress orientations are generally accurately and precisely determined by CSIT-2,
742 although there are few cases at low applied differential stress showing bad results (mainly on the dip
743 value of principal stress axis). This is due to the fact that the software calculates the 4 parameters
744 using $(\sigma_1 - \sigma_3) = 1$ without taking into account the different grain sizes. Thus, at low differential stress,
745 twinning in small grains (with high CRSS values) cannot be activated due to the differential stress of
746 the tensor even if they are favorably oriented regarding the stress tensor orientation. In these cases,
747 having two different grain sizes can bias the results.

748 **5.4 Influence of optical measurement bias**

749 The influence of the incorporation of bias in the datasets appears to be complex. It depends
750 on the orientation of misclassified planes regarding to the applied tensor. If a randomly misclassified
751 plane has a low applied resolved shear stress value, then the effect of the misclassification on the
752 results is insignificant. If the randomly misclassified plane has a high applied resolved shear stress
753 value regarding the applied tensor, then there is a strong influence on the penalization function, which
754 consequently increases. Because the selection of tested tensors relies partly on the penalization
755 function value, if this value is too high (above the limit fixed by the user), the tensor will be discarded,
756 even if this tolerance toward a value of 0.5 allows to be less restrictive than the previous method
757 (CSIT). The CSIT-2 selection process may miss “good” tensors depending on the orientation of the
758 misclassified untwinned planes. It is to date impossible to predict how it affects the orientations of

759 principal stress axes and other parameters because it is depending on the resolved shear stress applied
760 on this incompatible untwinned planes and how many there are. Few tests tend to show that the
761 principal stress orientations can be strongly affected, especially the dip of the stress axes, the azimuths
762 being well retrieved. The stress ratio and the differential stress are not affected by the inaccuracy of
763 the principal stress orientations. They remain well retrieved.

764 Our results show that the CSIT-2 method is overall robust for twin datasets with up to 25% of
765 incorporated bias. Considering the breaks in slope on the curves of the different parameters as a
766 function of the increasing number of twinned planes explained (Fig. 3 and 13F) leads to accurate
767 results even at such high bias (see sections 3.2 and 4 for more details), but at the cost of an increase
768 of the penalization function (up to 1.5) and also of the incorporation of incompatible untwinned planes
769 (number of incompatible untwinned planes over number of compatible twinned planes + number of
770 incompatible untwinned planes, Fig. 13E, up to 1.5). However, for natural cases the amount of optical
771 bias is not a priori known and an untwinned plane seen as incompatible for the inversion is not
772 necessary an optical measurement bias. It is therefore recommended, when analyzing (blindly) a
773 naturally deformed sample, to consider with care any solution tensor that would incorporate (more
774 than) 30% of incompatible untwinned planes and a penalization function value that would exceed 1.5
775 (Fig. 13E). The geological setting helps determine whether the solution-tensor is significant or not.

776 **5.5 Practical way to optimize data inversion**

777 The optical bias, likely due to errors in measurements using a U-stage can have a significant
778 effect (on the orientation of principal stress axes) despite the improvement of the technique. To
779 circumvent this difficulty, an index of uncertainty in the untwinned status of a twin plane has been
780 established for measurements of natural samples. This way, the user can double-check the status and,
781 in case of doubt, even change the status of the plane of poor confidence in the dataset. Note however
782 that this will be applied only on untwinned planes which appeared at low percentage of twinned
783 planes to be explained and therefore on which the tensor exerts a high resolved shear stress value.

784 In order to minimize the optical bias and measurement errors and to get information from
785 completely untwinned grains, twin data are currently being measured using EBSD rather than using
786 a U-stage (Parlangeau *et al.*, 2015). Optical bias consequently falls down to 0%. However, natural
787 heterogeneities at the grain scale (stress shadows, heterogeneous grain-to-grain stress transmission)
788 can of course not be circumvented and their weight on the quality of results can only be estimated by
789 comparing natural (non-perfect) data and numerical data. The decrease of incorporated bias has a
790 positive effect on the accuracy of the stress results (see comparison of monophasic results without/with
791 bias in section 5.3).

792 Overall, the least constrained parameter of the reconstructed deviatoric stress tensors is the
793 differential stress magnitude, especially when applied differential stresses are greater than 75 MPa.
794 Combining inversion of calcite twin data with fracture analysis and rock experiments (e.g., Lacombe,
795 2007) may however help test the validity and the meaning of determined stress magnitudes against
796 the mechanics of rock masses. Our study finally highlights that sorting the whole dataset into sub-
797 classes of homogeneous grain size before inversion is the best way to reliably define the 5 stress
798 tensor parameters, especially differential stresses. That is the reason why it is strongly recommended
799 to estimate the grain size distribution in a natural twin datasets and to apply separately the inversion
800 technique to homogeneous grain size classes, provided the number of available twin is sufficient to
801 secure a reliable stress tensor computation. In that case, provided each class yields similar accurate
802 principal stress orientations and stress ratio, assigning a different value of the critical resolved shear
803 stress to each class as a function of the mean grain size should provide more reliable (and expectedly
804 consistent) estimates of differential stresses (see section 7). Taking into account the grain-size
805 dependence of the CRSS in the inversion process is therefore a strong requirement; further work
806 should focus on providing better constraints on the variation of the CRSS as a function of grain size
807 (work in progress).

808 **6 Comparison with CSIT**

809 Few studies have focused on estimating uncertainties on the results of the former CSIT (Lacombe
810 and Laurent, 1996, 1992; Laurent et al., 2000). In order to illustrate the improvement on stress
811 determination brought by using CSIT-2 instead of CSIT, we provide hereafter a comparison of the
812 stress results obtained from both techniques when applied to polyphase datasets since Gaęala (2009)
813 has casts some doubt on the ability of CSIT to well retrieve close superimposed stress tensors. The
814 first configuration tested is the one applying a N-S compression with a stress ratio of 0.5 and a
815 differential stress of 50 MPa, the second applied tensor is turned of 30° between σ_1 axes with a stress
816 ratio of 0.5 and a differential stress of 50 MPa (configurations B25 then B27 in table 3). The second
817 configuration is exactly the same than the first one but with a differential stress of 75 MPa for both
818 tensors (configurations B26 then B28 in table 3). The last tested configuration is applying a first
819 tensor with a N-S strike-slip regime (σ_1 : N180-0 and σ_3 : N270-0) with a stress ratio of 0.5 and a
820 differential stress of 35 MPa. The second tensor applied is also a N-S strike-slip regime but with a
821 permutation of the σ_2 and σ_3 axes (σ_1 : N180-0 and σ_3 : N270-90) with a stress ratio of 0.5 and a
822 differential stress of 35 MPa (configurations B24 then B29 in table 3).

First tensor									
		<u>Applied</u>		CSIT		<u>Applied</u>		CSIT-2	
Stress axes orientation (°)	σ_1	N180-0	σ_1	N185-8	σ_1	N180-0	σ_1	N1-1	
	σ_2	N90-90	σ_2	N46-79	σ_2	N90-90	σ_2	N84-80	
	σ_3	N270-0	σ_3	N275-7	σ_3	N270-0	σ_3	N92-10	
Stress ratio		0,5		0,53		0,5		0,48	
<u>Differential stress (MPa)</u>		50		45,3		50		50	
<u>L²-norm (MPa)</u>		9,6				6,2			

Second tensor									
		<u>Applied</u>		CSIT		<u>Applied</u>		CSIT-2	
Stress axes orientation (°)	σ_1	N30-0	σ_1	N36-5	σ_1	N30-0	σ_1	N28-4	
	σ_2	N120-90	σ_2	N117-85	σ_2	N120-90	σ_2	N160-84	
	σ_3	N300-0	σ_3	N126-5	σ_3	N300-0	σ_3	N298-4	
Stress ratio		0,5		0,06		0,5		0,45	
<u>Differential stress (MPa)</u>		50		41,7		50		48,6	
<u>L²-norm (MPa)</u>		17,5				5,0			

Table 5: Results of the inversion using CSIT and CSIT-2 of the configuration B25 then B27. The L²-norm is the distance between the applied tensor and the solution-tensor found by CSIT or CSIT-2.

823 For the first configurations B25 then B27 (Table 3), the results are shown in table 5. L²-norm

824 value for solution-tensors found by CSIT-2 are way lower than the one calculated using CSIT.
 825 Especially for the configuration B27 (Table 3) where CSIT finds a stress ratio of 0.06 instead of 0.5
 826 which significantly increases the L^2 -norm value. The stress axis orientations are retrieved by both
 827 CSIT and CSIT-2. The differential stress is also well retrieved by both techniques with less error on
 828 CSIT-2 results than using CSIT.

829 For the second configurations B26 then B28 (Table 3), the results are shown in the table 6. This
 830 configuration is different from the first one only about the differential stress value which is higher,
 831 75 MPa for both tensors. As said previously, there is a loss of the information about differential stress
 832 between 50-75 MPa of applied differential stresses. Again, the distance between the applied tensors
 833 and the solution tensors is lower for the results using CSIT-2 than for CSIT. Especially for the first
 834 tensor (B26 in table 3) for which CSIT strongly overestimates the differential stress. The tensor found
 835 is clearly intermediate between the first and the second applied tensors.

<u>First tensor</u>									
		<u>Applied</u>		CSIT		<u>Applied</u>		CSIT-2	
Stress axes orientation (°)	σ_1	N180-0	σ_1	N196-3	σ_1	N180-0	σ_1	N7-4	
	σ_2	N90-90	σ_2	N78-84	σ_2	N90-90	σ_2	N198-86	
	σ_3	N270-0	σ_3	N286-6	σ_3	N270-0	σ_3	N97-1	
Stress ratio		0,5		0,45		0,5		0,46	
<u>Differential stress (MPa)</u>		75		92,4		75		75,9	
<u>L²-norm (MPa)</u>		35,6				13,8			

<u>Second tensor</u>									
		<u>Applied</u>		CSIT		<u>Applied</u>		CSIT-2	
Stress axes orientation (°)	σ_1	N30-0	σ_1	N25-9	σ_1	N30-0	σ_1	N25-5	
	σ_2	N120-90	σ_2	N116-81	σ_2	N120-90	σ_2	N121-85	
	σ_3	N300-0	σ_3	N295-9	σ_3	N300-0	σ_3	N115-5	
Stress ratio		0,5		0,49		0,5		0,49	
<u>Differential stress (MPa)</u>		75		74,7		75		65,3	
<u>L²-norm (MPa)</u>		12,3				11,9			

Table 6: Results of the inversion using CSIT and CSIT-2 of the configuration B26 then B28. The L^2 -norm is the distance between the applied tensor and the solution-tensor found by CSIT or CSIT-2.

836 For the last configurations B24 then B29 (Table 3), the results are shown in table 7. This
 837 configuration is the most difficult to retrieve for CSIT-2 as shown in figure 18, especially for the
 838 stress ratio value. In table 7, the L^2 -norm distance calculated between applied and solution tensors

839 shows that, again, CSIT-2 is more accurate than CSIT. CSIT finds a tensor which allows the
 840 permutation between σ_3 and σ_2 axes with a stress ratio very low of 0.03.

First tensor									
		<u>Applied</u>		CSIT		<u>Applied</u>		CSIT-2	
Stress axes orientation (°)	σ_1	N180-0	σ_1	N1-15	σ_1	N180-0	σ_1	N1-0	
	σ_2	N90-90	σ_2	N204-73	σ_2	N90-90	σ_2	N266-86	
	σ_3	N270-0	σ_3	N93-6	σ_3	N270-0	σ_3	N91-4	
Stress ratio		0,5		0,59		0,5		0,49	
<u>Differential stress (MPa)</u>		35		32,5		35		33,5	
<u>L²-norm (MPa)</u>		7,1				2,2			

Second tensor									
		<u>Applied</u>		CSIT		<u>Applied</u>		CSIT-2	
Stress axes orientation (°)	σ_1	N180-0	σ_1	N179-4	σ_1	N180-0	σ_1	N184-0	
	σ_2	N90-0	σ_2	N88-19	σ_2	N90-0	σ_2	N94-0	
	σ_3	N270-90	σ_3	N281-71	σ_3	N270-90	σ_3	N1-90	
Stress ratio		0,5		0,03		0,5		0,45	
<u>Differential stress (MPa)</u>		35		37,3		35		32,3	
<u>L²-norm (MPa)</u>		15,0				2,9			

Table 7: Results of the inversion using CSIT and CSIT-2 of the configuration B24 then B29. The L²-norm is the distance between the applied tensor and the solution-tensor found by CSIT or CSIT-2.

841 As a result, although some stress configurations are similarly retrieved by CSIT and CSIT-2.
 842 CSIT-2 being always more accurate than CSIT. Some other more complex stress configurations are
 843 clearly badly retrieved by CSIT while being consistently retrieved by CSIT-2. This illustrates that
 844 using CSIT-2 will expectedly improve the reliability of stress determination in polyphase settings in
 845 forthcoming tectonic studies.

846 **7 Application to naturally deformed polyphase samples**

848 In order to test the CSIT-2 and its ability to derive geologically meaningful paleostresses, the
 849 technique is applied on samples collected from limestones of Tithonian-Aptian age (Maiolica
 850 formation) in the Monte Nero anticline located within the Umbria-Marches tectonic domain of the
 851 northern Apennines (Italy). The Monte Nero-Serra Santa is an arcuate fold with a backlimb dipping
 852 30° towards W-SW and an intensively folded forelimb, where the strata are locally overturned
 853 (Fig.21). Microstructural investigations revealed occurrence of several sets of joints and veins (mode

854 I opening) that developed mainly before the onset of folding (Beaudoin et al., 2016).

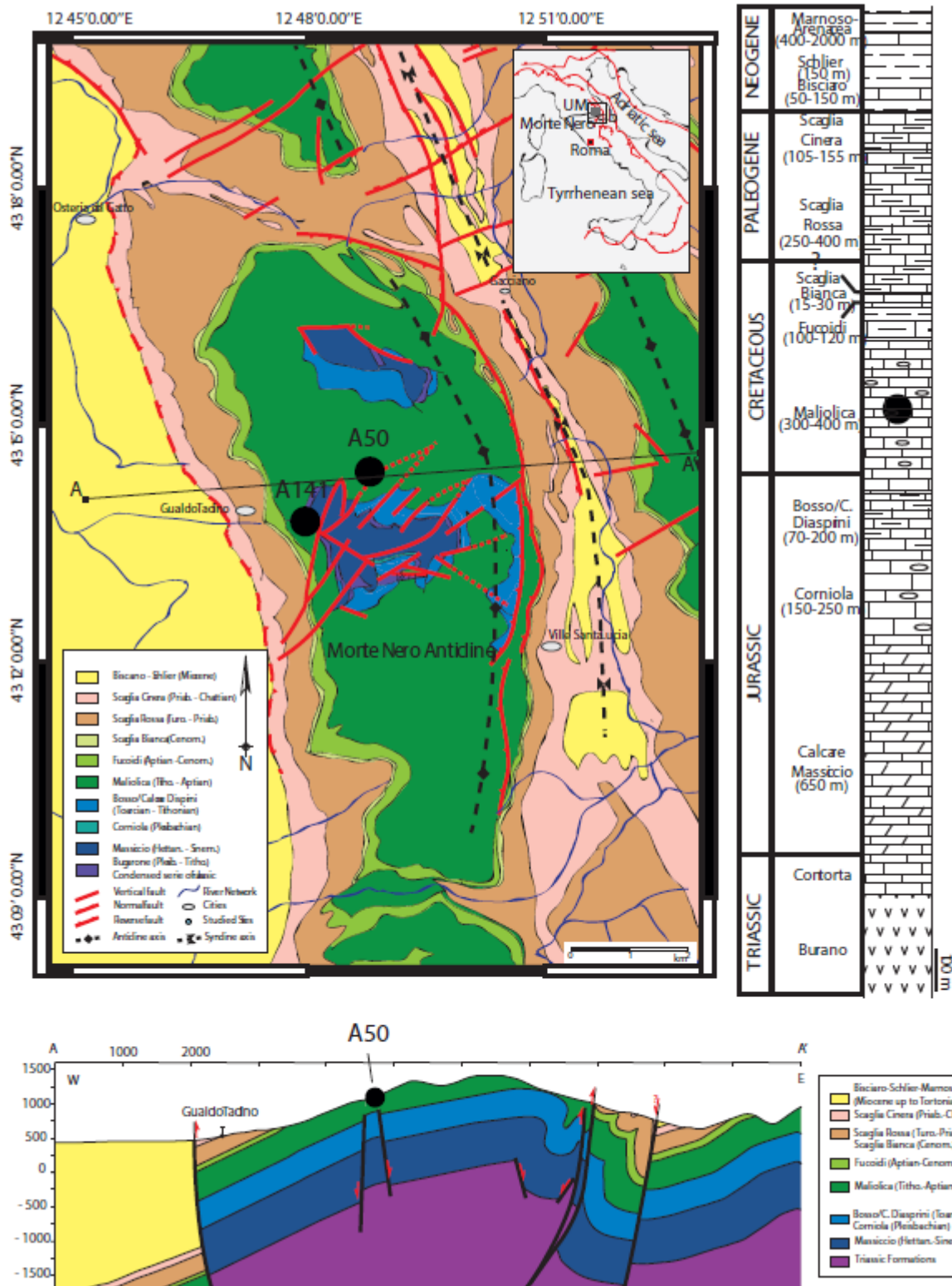


Figure 21: Simplified geological map and stratigraphic log of the Monte Nero anticline (northern Apennines) with location of the sample studied (modified after Beaudoin et al., 2016).

855 In the western limb of the fold, we selected a first sample containing two intersecting veins

856 belonging to successive sets recognized in the field. After unfolding, Vein 1 (Fig. 22A) belongs to a
 857 bed-perpendicular N050 vein set (N65-69S in present attitude), while Vein 2 belongs to a second set
 858 of bed-perpendicular veins striking N090-110° (N291-84N in present attitude). Vein 2 clearly cuts
 859 across Vein 1 and therefore unambiguously postdates it.

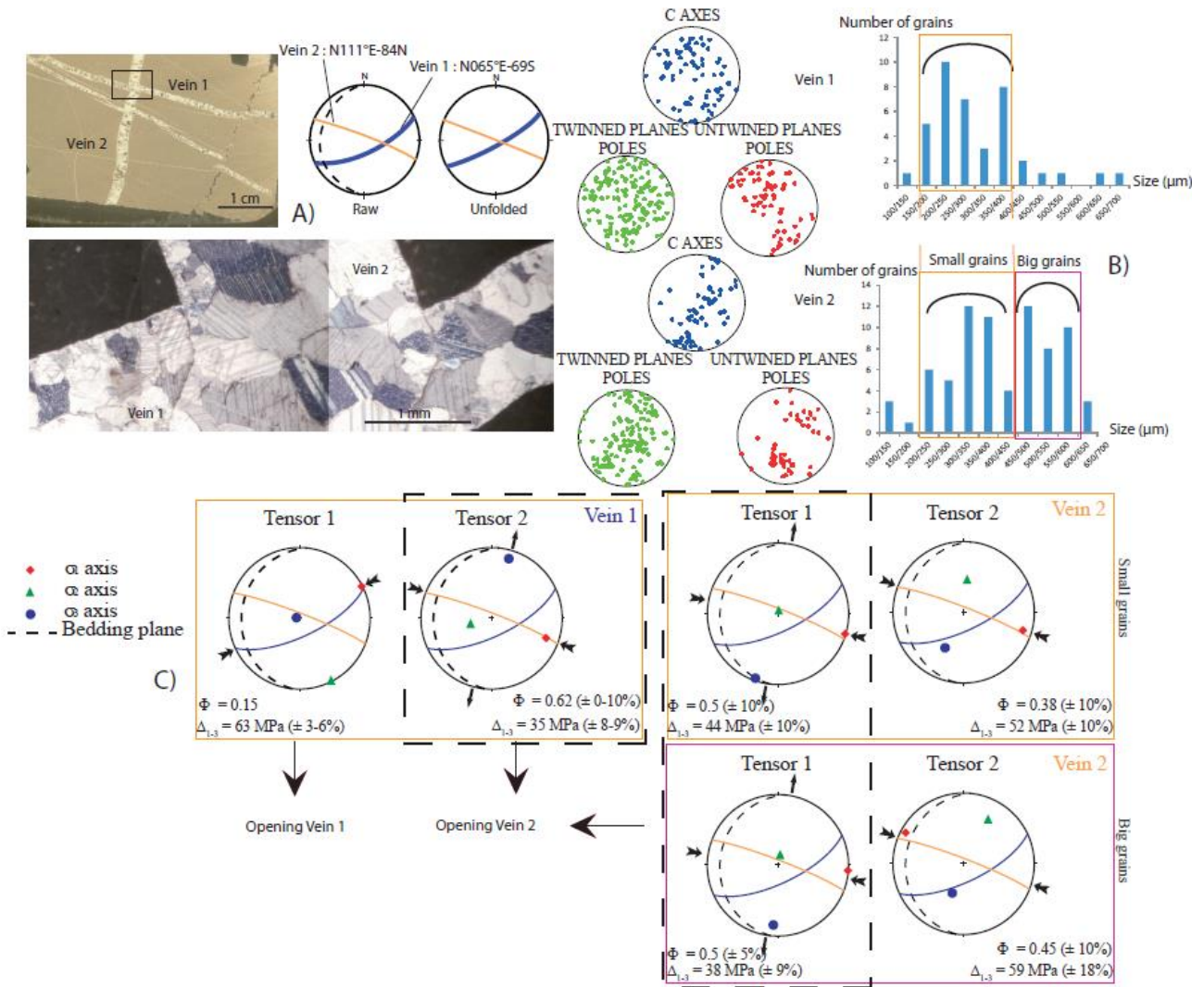


Figure 22: Inversion results of naturally deformed polyphase datasets. A) Picture of a thin section (crossed polars) showing crosscutting veins, together with stereographic projection of measured veins (Wulff's lower hemisphere equal area projection). B) Plots of C axes, and poles of twinned and untwinned planes from veins 1 and 2 together with distribution of related grain sizes. C) Results of inversion of calcite twins from vein 1 and vein 2 (for more details, see text). For the vein 1, the first tensor is oriented with σ_1 : N63-2 and σ_3 : 297-87 and the second tensor is oriented with σ_1 : N110-21 and σ_3 : 15-13. For the vein 2 small grains, the first tensor is oriented with σ_1 : N105-1 and σ_3 : 195-3 and the second tensor is oriented with σ_1 : N108-16 and σ_3 : 215-47. For the vein 2 big grains, the first tensor is oriented with σ_1 : N95-1 and σ_3 : 185-20 and the second tensor is oriented with σ_1 : N300-8 and σ_3 : 200-53.

860 This chronology between the two vein sets is documented in many places at the scale of the fold and

861 is therefore statistically valid at the regional scale. These vein sets are associated with sets of bed-
862 perpendicular stylolites of tectonic origin and are parallel to the teeth they exhibit (peaks oriented
863 N050 and N090-110). This observation supports the fact that both fracture sets developed under sub-
864 horizontal compression (σ_1 axis) before folding.

865 We carried out U-stage measurements of calcite twins within these two veins from 3 mutually
866 perpendicular thin-sections. Calcite grains display thin (0.5 μm) and rectilinear e-twins, which cross
867 the crystals over all their length (Fig. 22A). These characteristics indicate that calcite grains probably
868 underwent weak strain, 3-4% at most, under conditions of temperature lower than 150°C–200°C
869 (Ferrill et al., 2004). For each vein, we measure and report the orientations of C axes and of twinned
870 and untwinned planes and we estimate grain sizes using the 3 thin-sections (Fig. 22B) to avoid as
871 much as possible bias related to 2D observations. We could define a single grain size class for Vein
872 1 and two grain sizes for Vein 2. One should keep in mind that because these classes must contain a
873 sufficient number of grains for the inversion to be statistically valid (at least 30 grains), they must not
874 be too narrow. Inversion is carried out for each grain size class independently. For Vein 1 the CRSS
875 considered is of 9 MPa. For Vein 2, the CRSS value is of 10 MPa for the lower grain size (200-400
876 μm) and 7.5 MPa for the higher grain size (400-600 μm). Note that although the grain size class of
877 Vein 1 is similar to the smaller grain size class of Vein 2, the adopted CRSS value are slightly different
878 (9 and 10 MPa, respectively). This is because the CRSS is also dependent on internal twinning strain,
879 which is roughly estimated using twin density to be higher in Vein 2 than in Vein 1. This way to take
880 into account strain hardening is similar to Rocher et al. (2004) and Amrouch et al (2010).

881 Taking into account the crosscutting relationships between the veins (Fig. 22A), twinned
882 calcite from Vein 1 expectedly recorded (at least) the state of stress responsible for its opening, but
883 also the later state of stress responsible for the formation of Vein 2. In contrast, calcite from Vein 2
884 should not have recorded the state of stress responsible for the earlier opening of Vein 1 but should
885 have expectedly recorded the state of stress responsible for its own formation.

886 Inversion results shown in figure 22C illustrate that two tensors are found by the inversion
887 process within each vein. Vein 1 records a $N050 \pm 6^\circ$ compression with a stress ratio of 0.15, a
888 differential stress of $63 \text{ MPa} \pm 3\text{-}6\%$ and a $N110 \pm 6^\circ$ compression associated with perpendicular
889 extension, a stress ratio of 0.62 ± 0.1 , a differential stress of $35 \text{ MPa} \pm 8\%$. Vein 2 yields a stress
890 tensor similar to the second tensor from vein 1. The uncertainties associated with the previous results
891 are estimated from the interpretation of the analyses on synthetic datasets. Results from the inversion
892 process are consistent across grain size ranges.

893 A relative chronology between successive twinning stresses can be established through
894 consideration of orientation of computed stress axes (as well as of stress ratio) with respect to vein
895 orientation. The simple underlying idea is that a stress tensor determined from the calcite grains filling
896 a vein with a σ_3 axis perpendicular to the vein strike is likely related to the vein opening while other
897 tensors with stress axes inconsistent with the vein geometry likely reflect later, post-opening stress
898 regimes (Lacombe, 2010).

899 The compressional configuration of tensor 1 from Vein 1 with subhorizontal σ_1 axis lying
900 parallel to the vein and subvertical σ_3 axis, is not at first glance consistent with opening of Vein 1.
901 But the low value of the stress ratio supports that σ_2 and σ_3 are very close in magnitudes hence prone
902 to switch, so the computed σ_3 axis is consistent with vein opening in a strike-slip / compressional
903 stress regime. This tensor should be considered as predating tensor 2, which is therefore likely post-
904 opening. The strike-slip configuration of tensor 2 from Vein 1 with subhorizontal σ_1 and σ_3 axes lying
905 within and perpendicular to Vein 2, respectively, is in perfect agreement with opening of this vein.
906 This means that Vein 1 recorded the stress regime responsible for opening of Vein 2 which postdates
907 Vein 1. Similarly, the strike-slip configuration of tensor 1 from Vein 2 with subhorizontal σ_1 and σ_3
908 axes lying within and perpendicular to the vein, respectively, is in perfect agreement with opening of
909 Vein 2, and should be considered as predating tensor 2 from Vein 2. Tensor 2 from Vein 2 is therefore
910 a likely post-opening stress tensor, which reflects a later change from strike-slip to compressional

911 stress configuration, the σ_1 axis remaining unchanged.

912 Interestingly, tensor 2 from Vein 1 and tensor 1 from Vein 2 are also very close in terms of
913 stress magnitudes with only 0.1 of difference in stress ratio and 9 MPa maximum difference in
914 differential stress magnitude ($\sigma_1 - \sigma_3$).

915 On a methodological point of view, these results show that despite the natural heterogeneity
916 of the calcite filling the veins, CSIT-2 captures the stress regimes consistent with opening of
917 successive regional vein sets which developed during successive substages of the tectonic evolution
918 of the Monte Nero anticline (Beaudoin et al., 2016). The pre-folding N050 compression is related to
919 the regional Apenninic compression which formed the Umbria-Marches domain and started during
920 Tortonian times (Barchi et al., 2012; Billi et al., 2007; Marshak et al., 1982; Storti and Salvini, 2001;
921 Tavani et al., 2008). The subsequent pre-folding N090 to N110 compression is interpreted as a
922 perturbation of the Apenninic compression caused by a N-S striking fault at depth beneath the fold,
923 likely inherited from Tethyan rifting, and which reactivation as a high-angle thrust controlled the
924 structure of the Monte Nero anticline (Beaudoin et al., 2016.).

925 Finally, differential stresses obtained from vein 1 (63 MPa \pm 3-6% for the first tensor and 35
926 MPa \pm 8-9%) and 2 (38-44 MPa \pm 9-10%) are in good agreement with independent differential stress
927 estimates based on tectonic stylolite roughness paleopiezometry at the same locations (Beaudoin et
928 al., 2016). Taking into account an average burial of the Maiolica formation of 2700 m at the time of
929 deformation as derived from the stratigraphic succession, these values are also in good agreement
930 with predicted ranges of differential stress values for compressional strike-slip stress regime (opening
931 of Vein 1) and strike-slip stress regime (opening of Vein 2) at this depth based on differential
932 stress/depth relationship in the crust as reported by Lacombe (2007).

933 As shown in figure 23A, C axes and poles to twinned and untwinned planes for both veins
934 show a non homogeneous spatial distribution. Even though the high level of consistency of the results
935 argues in favor of the robustness of the technique to such potential bias, we also analyzed another
936 sample containing a vein from the same set (N050 trending bed-perpendicular set) than V1 from the

937 former sample that shows a more homogeneous distribution of C axes and poles to twinned and
 938 untwinned planes. This sample is located (Fig. 23A) in the western part of the Monte Nero anticline,
 939 also in the Massicio formation.

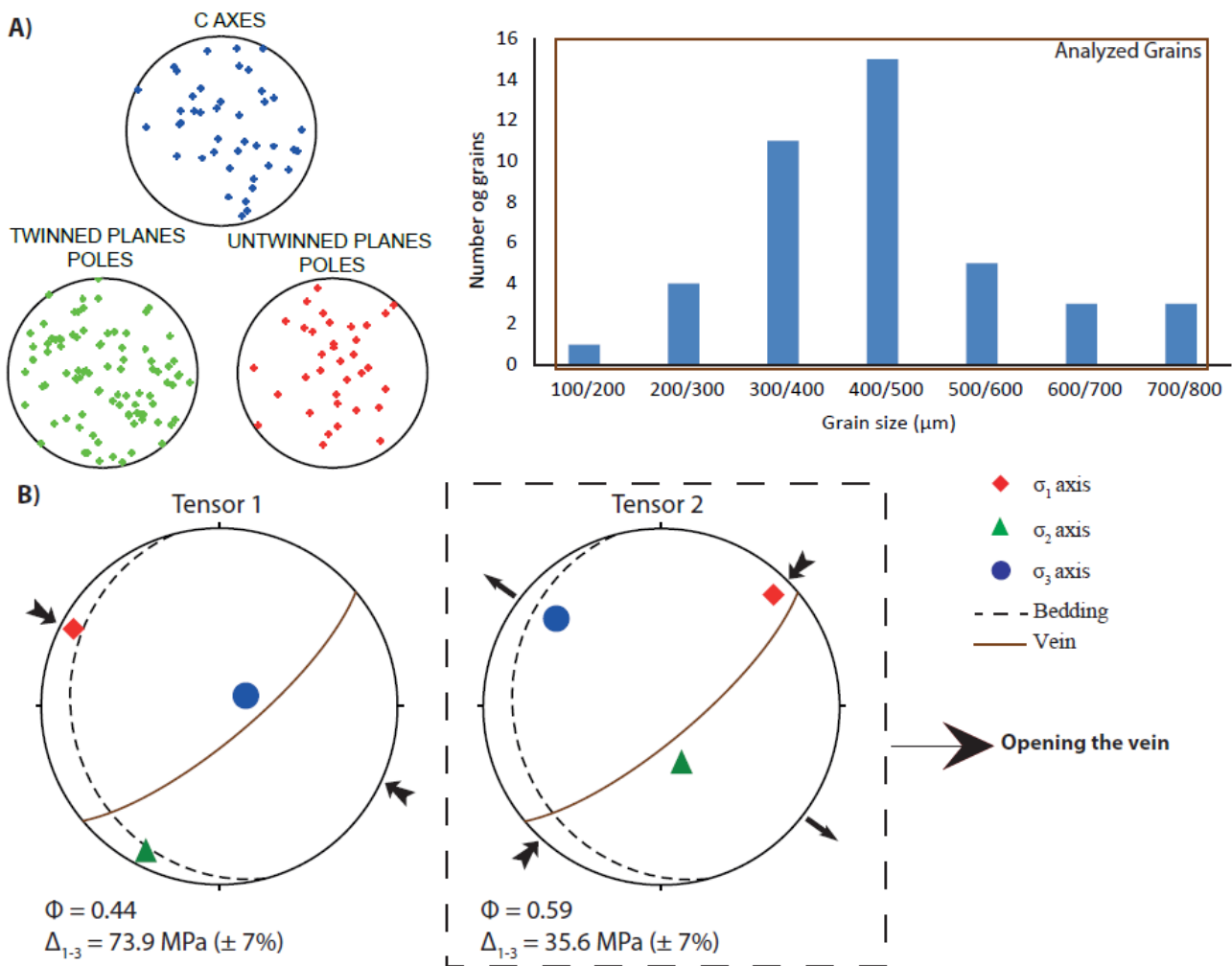


Figure 23: Inversion results of naturally deformed polyphase datasets. A) Plots of C axes, and poles of twinned and untwinned planes with distribution of related grain sizes. B) Results of inversion of calcite twins (for more details, see text). The first tensor is oriented with σ_1 : N298-8 and σ_3 : 68-77. The second tensor is oriented with σ_1 : N45-12 and σ_3 : 310-24.

940 The results of the inversion show a strike-slip configuration with a N45 trending σ_1 axis and a
 941 perpendicular horizontal σ_3 axis (Fig. 23B) consistent with the opening of the vein (N50-75S in
 942 present attitude). The maximum differential stress is 35.6 MPa ($\pm 7\%$) with a stress ratio of 0.59.
 943 Another tensor has been revealed by the inversion that corresponds to a N118 compression with a
 944 differential stress value of 73.9 MPa ($\pm 7\%$) and a stress ratio of 0.44. The 118° compression likely
 945 postdates the strike-slip regime with a N45 σ_1 axis which is consistent with vein opening.

946 In terms of orientations, both stress tensors are consistent with those determined
947 independently from the nearby former sample, which supports the ability of the technique to provide
948 consistent, regionally significant stress tensors. The consistency of the results from both samples
949 further indicates that a slight preferred orientations of the C axes and poles to twinned and untwinned
950 planes exerts a negligible bias on stress tensor determination using CSIT-2.

951 The 35.6 MPa and 73.9 MPa differential stress values associated with the N45 strike-slip and
952 the N118 compressional stress regimes are different from the values obtained from the former sample
953 for the corresponding tensors (63 MPa and 52/59 MPa, respectively). However, these values are
954 associated with a much greater uncertainty than those derived from the tests on synthetic datasets
955 because the low number of grains precluded any separation of the natural dataset into classes of
956 homogeneous grain size, so that the 9 MPa value of the CRSS adopted for calculation is badly
957 constrained. In spite of this additional effect, the values for the second sample remain of the same
958 order than those derived from the first sample and fall within the range of differential stresses reported
959 by Beaudoin et al. (2016) in the Monte Nero anticline.

960 **7 Conclusions**

961 Inversion of calcite twin data is to date an efficient approach to determine both paleostress
962 orientations and magnitudes in the upper crust. This paper proposes a new technique inspired from
963 the CSIT (Etchecopar, 1984) but which circumvents its main limitations. The ability of the new
964 technique to detect, to separate and to determine stress tensors from monophasic and polyphasic twin
965 datasets including measurements errors or various grain sizes is demonstrated by numerous tests on
966 synthetic (numerically generated) twin datasets. In contrast to Gaġala (2009), Rez and Melichar (2010)
967 and Yamaji (2015), who do not report any application of their techniques to natural data, this paper
968 shows that apart from synthetic samples for which the physical problems related to stress transmission,
969 grain rheological properties (e.g., elasticity) and grain-scale stress heterogeneities are neglected, the
970 technique also yields reliable paleostresses from naturally deformed polyphasic samples. It is however
971 strongly advised to handle the results provided by any stress inversion techniques with care, and to

972 have a critical look at the results, making the best use of available geological information (e.g.,
973 relative chronology) to guide the inversion procedure and separation of superimposed stress tensors.

974 The main technical limitations of paleostress reconstructions from calcite twins to date,
975 whatever the inversion technique is used, are related to (1) potential errors in optical measurements;
976 (2) the influence of grain size and grain size distribution in the deformed aggregates, and (3) our
977 insufficient knowledge of the variations of the CRSS value for twinning with grain size. While the
978 first is likely to be overcome by twin data acquisition using EBSD (Parlangeau et al., 2015) and the
979 second is possibly circumvented by defining several grain size classes and treating them separately,
980 understanding the influence of the grain size distribution and characterizing the way the CRSS varies
981 with changing grain size are challenges for forthcoming studies.

982

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