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**Sound velocities and density measurements of solid hcp-Fe and hcp-Fe-Si(9wt.%) alloy  
at high pressure: Constraints on the Si abundance in the Earth's inner core**

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## Abstract

We carried out sound velocity and density measurements on solid hcp-Fe and an hcp-Fe-Si alloy with 9 wt.% Si at 300 K up to  $\sim 170$  and  $\sim 140$  GPa, respectively. The results allow us to assess the density ( $\rho$ ) dependence of the compressional sound velocity ( $V_P$ ) and of the shear sound velocity ( $V_S$ ) for pure Fe and the Fe-Si alloy. The established  $V_P$ - $\rho$  and  $V_S$ - $\rho$  relations are used to address the effect of Si on the velocities in the Fe-FeSi system in the range of Si concentrations 0 to 9wt.% applicable to the Earth's core. Assuming an ideal linear mixing model, velocities vary with respect to those of pure Fe by  $\sim +80$  m/s for  $V_P$  and  $\sim -80$  m/s for  $V_S$  for each wt.% of Si at the inner core density of  $13000 \text{ kg/m}^3$ . The possible presence of Si in the inner core and the quantification of its amount strongly depend on anharmonic effects at high temperature and on actual core temperature.

**Keywords:** seismic wave velocities; iron; iron-silicon alloys; high pressure; high temperature; Earth's inner core

## 1. Introduction

The physical properties of iron and iron alloys at high pressure are crucial to refine the chemical composition and dynamics of the Earth's core. In this respect, density ( $\rho$ ), compressional-wave ( $V_P$ ) and shear-wave ( $V_S$ ) sound velocities are of particular importance, as those parameters can be directly compared to seismological observations. Over the last twenty years, a great effort has been devoted to the development of experiments capable of probing sound velocity of metallic samples at high pressure, with a specific focus on iron (see *Antonangeli and Ohtani [2015]* for a recent review). Ab initio calculations have been extensively applied as well to assess material's properties at core pressures and temperatures [e.g. *Vočadlo et al., 2009; Sha and Cohen, 2010; Martorell et al., 2013*]. Yet, a consensus has not been reached, not only concerning the absolute values of velocities of solid iron at inner core conditions, but also the dependence of velocities upon pressure and temperature.

Since the seminal work of *Birch [1952]* it has been well established that light elements are alloyed to iron in the Earth's core to account for the density difference between pure Fe and seismological observations (e.g. model PREM by *Dziewonski and Anderson [1981]*). For the solid inner core, many recent experimental studies suggest silicon as one of the major candidates, based on its physical properties (density and sound velocity) and/or affinity for the metallic phase during Earth's differentiation [e.g. *Lin et al., 2003; Badro et al., 2007; Antonangeli et al., 2010; Mao et al. 2012; Siebert et al., 2013; Fischer et al., 2015; Tateno et al., 2015*]. However, different works propose different amount of Si alloyed to Fe in the inner core, ranging from ~2wt.% [*Badro et al., 2007; Antonangeli et al., 2010*] up to ~8% [*Mao et al. 2012; Fischer et al., 2015*]. One of the causes for such a discrepancy is the large pressure and temperature extrapolation necessary to compare experimental results with inner core seismological models. For instance, results based on linear extrapolations of  $V_P$ - $\rho$  relation argued for about 2 wt% Si alloyed to Fe in the inner core [*Badro et al., 2007; Antonangeli et*

*al.*, 2010], while a model using a power law for the  $V_P$ - $\rho$  extrapolation proposed 8 wt% Si [Mao *et al.* 2012]. In contrast with the bulk of the experimental results, a very recent computational work on silicon alloys at inner core conditions [Martorell *et al.*, 2016] suggested that both the P-wave and the S-wave velocities of any hcp-Fe-Si alloy would be too high to match the seismically observed values at inner-core density.

To shed light on this ongoing debate, we carried out sound velocity and density measurements on pure Fe and a Fe-Si alloy with 9 wt.% Si in the hexagonal close-packed structure (hcp) from  $\sim 40$  GPa up to  $\sim 170$  GPa, using inelastic x-ray scattering (IXS) and x-ray diffraction (XRD). IXS allows a clear identification of longitudinal aggregate excitations in polycrystalline samples [Fiquet *et al.*, 2001, 2009; Antonangeli *et al.*, 2004, 2010, 2012, 2015; Badro *et al.*, 2007; Mao *et al.*, 2012; Ohtani *et al.*, 2013] and the derivation of  $V_P$  from a sine fit of the phonon dispersion. Combining the measured  $V_P$  with the bulk modulus derived from the equation of state,  $V_S$  can be determined as well, while the density is directly obtained from the collected diffraction patterns. In this study, we aim to establish precise relations between velocities (both  $V_P$  and  $V_S$ ) and density for Fe and a representative Fe-Si alloy with 9 wt.% Si over a wide pressure range at room temperature. The results will provide a benchmark for calculations and will serve as reference for further studies of increased compositional complexity or addressing the temperature effects on the velocities.

## 2. Materials and Methods

Starting materials consisted in commercially available polycrystalline samples of Fe (99.998%, Alpha Aesar) and a Fe-Si alloy with 9 wt.% Si (Goodfellow, hereafter Fe-Si9). The same Fe-Si alloy was used in previous study of equation of state, with an average Si content measured by electron microprobe analysis of 8.87 wt% [Zhang and Guyot, 1999].

IXS and XRD measurements have been carried out at the European Synchrotron Radiation facility (ESRF) at ID28 and ID27 beamlines, respectively. IXS measurements have been performed on polycrystalline specimens compressed in a diamond anvil cell (DAC) using the Si(9,9,9) instrument configuration, which yields an overall energy resolution of 3 meV full width half maximum (FWHM). Absolute energies have been calibrated prior to the experiment comparing IXS diamond phonon dispersion with that obtained by inelastic neutron and Raman scattering. Specific to this experiment, we double-checked the energy calibration by comparing the sound velocity measured by IXS on iron powders at ambient conditions with the Voigt–Reuss–Hill average of ultrasonic determination on single crystal [Guinan and Beshers, 1968]. We also calibrated the scattering angle at the small working values of our IXS measurements by collection of diffraction from a silver behenate standard. Optics in Kirkpatrick-Baez configuration allowed focusing the x-ray beam at sample position at  $30 \times 70 \text{ } \mu\text{m}^2$  (horizontal x vertical, FWHM) or down to  $12 \times 7 \text{ } \mu\text{m}^2$  (horizontal x vertical, FWHM) depending upon DAC configuration. Momentum resolution was set by slits in front of the analyzers to  $0.28 \text{ nm}^{-1}$  and to  $0.84 \text{ nm}^{-1}$ , in the scattering plane and perpendicular to it. A vacuum chamber was used to minimize the quasi-elastic scattering contribution from air. Good-statistic data have been obtained with typical integration time of  $\sim 300 \text{ s}$  per point for Fe, and  $\sim 500\text{-}600 \text{ s}$  per point for Fe-Si9.

Pressures were generated by symmetric type, MAO DAC, using composite Re/c-BN gaskets, with either  $150/300 \text{ } \mu\text{m}$  beveled anvils, or  $40/100/250 \text{ } \mu\text{m}$  beveled anvils prepared by focus ion beam (FIB) milling technique [Fei et al., 2016]. Diamonds were pre-aligned and oriented to select the fastest transverse acoustic phonon of the diamond in the scattering plane and to minimize its intensity. The focused beam of  $12 \times 7 \text{ } \mu\text{m}^2$  FWHM at sample position granted collection of clean spectra on specimens down to  $\sim 35 \text{ } \mu\text{m}$  in diameter. Such a small beam also permitted to probe phonons across moderate pressure gradients (as determined

from the fine diffraction mesh, see below), while the composite gasket ensured relatively thick samples (8 to 12  $\mu\text{m}$  at the highest pressure), and hence proper IXS signal, averaged over a reasonably large number of grains. Pressure was increased off line by monitoring the Raman spectra at the tip of the diamonds, and more precisely measured by the x-ray diffraction according to known samples equation of state. Specifically we used a third-order Birch-Murnaghan formalism, with  $V_0 = 22.47 \text{ \AA}^3/\text{unit cell}$  [Dewaele *et al.* 2006],  $K_0 = 155 \text{ GPa}$  and  $K' = 5.37$  [Sakai *et al.*, 2014] for hcp-Fe and  $V_0 = 23.50 \text{ \AA}^3/\text{unit cell}$ ,  $K_0 = 129 \text{ GPa}$  and  $K' = 5.24$  for hcp-Fe-Si9 [Fei, 2017].

At each investigated pressure point, we mapped the aggregate longitudinal acoustic phonon dispersion throughout the entire first Brillouin zone collecting 6 to 9 spectra in the 3-12.5  $\text{nm}^{-1}$  range. The energy positions of the phonons were extracted by fitting a set of Lorentzian functions convolved with the experimental resolution function to the IXS spectra. Figure 1 shows an example of the collected IXS spectra and the fitted result. We derived  $V_P$  from a sine fit to the phonon dispersion [Antonangeli *et al.*, 2004] (Figure 1), with error bars between  $\pm 1$  and  $\pm 3\%$  for Fe and between  $\pm 2$  and  $\pm 4\%$  for Fe-Si9. The errors account for statistical errors, finite energy and momentum resolution, as well as deviation from ideal random orientation of the polycrystalline samples. Combining the measured  $V_P$  with bulk modulus from the equation of state (the difference between isothermal and adiabatic bulk modulus at 300 K is negligible), we also derived  $V_S$  [Antonangeli *et al.*, 2004], with uncertainties, obtained by propagating uncertainties on  $V_P$  and on  $K$  (the contribution from uncertainties on density was observed to be negligible), between  $\pm 5$  and  $\pm 6\%$  for pure-Fe, and between  $\pm 8$  and  $\pm 10\%$  for Fe-Si9 (assuming different equation of state leads to small effects on  $V_S$  well within reported error bars).

For both samples, we collected angle dispersive 2D diffraction patterns at each investigated pressure point, with a monochromatic wavelength of 0.3738  $\text{\AA}$  (iodine K edge).

This allowed for clear structure determination and direct measurements of samples' density. Taking advantage of the  $3 \times 3 \text{ }\mu\text{m}^2$  beam, we mapped the entire sample area, monitoring pressure gradients across the sample chamber. Diffraction data are also used to detect any developed texture. Examples of collected diffraction patterns are shown in Figure 2 and Figure 3. The diffraction patterns of the compressed hcp-Fe (Figure 2) show rather smooth rings, indicating the small sizes of the diffracting crystallites (average size  $\sim 25 \text{ nm}$  at 167 GPa) and the good orientation averaging (only 100 reflection shows some variation in intensity with the azimuthal angle). Two-dimensional detector images caked into rectilinear projection show negligible dependence of the d spacing on the azimuthal angle around  $2\theta=0$  direction (Figure 2), and hence a negligible deviatoric stress [Wenk *et al.*, 2006]. Furthermore, the (002) reflection, although weak, is still visible up to the highest attained pressure, further highlighting the marginal preferential orientation. Such observations support the overall validity of the random orientation approximation, critical to the analysis and interpretation of the IXS results [Antonangeli *et al.*, 2004; Bosak *et al.*, 2007;2016]. The diffraction patterns collected for the Fe-Si9 alloy (Figure 3) are somewhat less favorable than those on pure Fe, in particular in term of sizes of crystallites (average size  $\sim 40 \text{ nm}$  at 117 GPa) and randomness of the distribution (intensity variation are quite visible for both 100 and 101 reflections), but they are still acceptable. The (002) reflection, still visible at all probed pressure, is very weak, as a direct consequence of a small preferential orientation fully developed already at 59 GPa and not significantly evolving with pressure, with the c-axis preferentially aligned along the main compression axis of the cell. Similar texture has been already reported in previous experiments on iron [Wenk *et al.*, 2000] and other metals with hcp structure [Merkel *et al.*, 2006]. Such a moderately increased deviation from the ideal random distribution is reflected into the fairly increased error bars on the velocities derived from the IXS data (deviation from ideal average can affect velocities up to 2%).



At the highest compression the maximum observed difference in pressure across the sample chamber ( $\sim 35 \mu\text{m}$ ) is  $<7 \text{ GPa}$  for Fe and  $<10 \text{ GPa}$  for Fe-Si9. Over the volume seen by IXS we obtain an average pressure of  $167 \text{ GPa}$  (Fe), with a standard deviation of  $2 \text{ GPa}$  and a standard error of  $1 \text{ GPa}$ , and an average pressure of  $144 \text{ GPa}$  (Fe-Si9), with a standard deviation of  $2 \text{ GPa}$  and a standard error of  $1 \text{ GPa}$ .

### 3. Results

The experimentally determined densities and velocities for hcp-Fe and hcp-Fe-Si9 are summarized in Table 1. The details are presented below.

The measured compressional and shear sound velocities as a function of density for hcp-Fe are plotted in Figure 4. These new measurements of  $V_P$  are in very good agreement with the  $V_P$ - $\rho$  linear relationship recently proposed by fitting combined datasets derived from multiple techniques [Antonangeli and Ohtani, 2015], extending the data coverage at extreme pressures. We notice that the extrapolation of the established trend to higher density is in remarkable agreement with ab initio calculations at  $0 \text{ K}$  [Vočadlo et al., 2009; Sha and Cohen, 2010], clearly supporting a linear dependence of  $V_P$  on density. The derived  $V_S$ - $\rho$  linear relationship is also in general agreement with results of ab initio calculations at  $0 \text{ K}$ . We also noticed the good agreement between the slope of our  $V_S$ - $\rho$  trend with that obtained by the most recent nuclear resonant inelastic x-ray scattering (NRIXS) experiments [Murphy et al., 2013; Gleason et al., 2013; Liu et al., 2016], even if actual  $V_S$  values derived by NRIXS are somewhat lower, between 3 to 8% depending upon datasets. Such a difference is at least partially due to the enrichment in heavier Fe isotopes of samples used for NRIXS studies with respect to sample of natural isotopic abundance used here.

The measured compressional and shear sound velocities as a function of density for hcp-Fe-Si9 are shown in Figure 5. Our  $V_P$  measurements on samples with 9 wt.% Si are very close to previous IXS measurements on samples with 8 wt.% Si [Mao *et al.*, 2012], but they are systematically higher than early determination by NRIXS on samples with 8 wt.% Si [Lin *et al.*, 2003]. Similar to the case of pure Fe, our measurements support a linear dependence of  $V_P$  on  $\rho$  for Fe-Si9. The derived  $V_S$ - $\rho$  relationship can be well described by a second order polynomial (Figure 5).

Comparison of results obtained for Fe and Fe-Si9 (Figure 6) show that Si alloying systematically increases  $V_P$  at constant density over the investigated pressure range. Linear fits indicate that, even if  $V_P$  of the Fe-Si9 alloy increases with density slower than pure Fe, Fe-Si9 is still expected to have significantly higher  $V_P$  than Fe at inner core density ( $\sim 12390$  m/s vs.  $\sim 11680$  m/s at  $13000 \text{ kg/m}^3$ ). On the other hand, the derived density evolution for  $V_S$  of Fe-Si9 is such that the Si-bearing alloys is expected to have higher  $V_S$  than pure Fe only up to  $\rho \approx 11200 \text{ kg/m}^3$ , with  $V_S$  of Fe larger than  $V_S$  of Fe-Si9 at inner core density ( $\sim 5130$  m/s vs.  $\sim 5890$  m/s at  $13000 \text{ kg/m}^3$ ). This trend (i.e  $V_P$  increasing with Si content and  $V_S$  decreasing) has been reported as well by recent ab initio calculations of Fe-Si alloys at core pressures [Martorell *et al.*, 2016]. However, on the contrary to the case of pure Fe, the extrapolation of our experimental results for Fe-Si9 does not agree with the calculations.

#### 4. Discussion

Concerning hcp-Fe, we note a remarkable agreement between our new measurements, previous measurements by various techniques and ab initio calculations for  $V_P$ , and a reasonable agreement for  $V_S$ . The established consensus provides very strong constraints on the linear dependence of velocities on density and on actual values of velocities of hcp-Fe at

inner core densities and 300 K (Figure 4), which can by now be considered known within few percent (with  $V_P$  better constrained than  $V_S$ ).

Somewhat less evident is the case for Si bearing hcp Fe-alloys. Literature data obtained in the  $\sim 40$  to  $\sim 100$  GPa range on samples of the same nominal composition [Lin *et al.*, 2003; Mao *et al.*, 2012] are in clear disagreement (Figure 5). Reasons for the discrepancy between NRIXS [Lin *et al.*, 2003] and IXS [Mao *et al.*, 2012] data possibly include systematic differences due to the techniques, or due to the sample's texture. The  $V_P$  measured in this study are in a good agreement with previous IXS determination at lower pressures [Mao *et al.*, 2012] and significantly extend the probed pressure range. In view of our new data, a sub-linear relationship between  $V_P$  and density, as proposed by Mao *et al.*, [2012] on the basis of data over a more restricted pressure range, seems not justified. Linear extrapolation of experimental results to inner core density and comparison with calculations [Tsuchiya and Fujibuki, 2009; Martorell *et al.*, 2016] show however a disagreement, more important for  $V_P$  than for  $V_S$ . The difference would be even more striking when considering a power-law sub-linear extrapolation. In particular, the calculations seem to overestimate the effect of Si on  $V_P$  of the Fe-Si alloys. We noticed that ab initio calculations on Fe-Si alloys, even when performed at 0 K, give quite conflicting results [Tsuchiya and Fujibuki, 2009; Martorell *et al.*, 2016], highlighting the difficulty in performing calculations taking into account the configurational order/disorder inherent to alloys. Further investigation by both experiments and theoretical calculations is necessary to resolve the discrepancy.

The direct comparison between results obtained on Fe and on Fe-Si9 allows us to address the effect of Si content on the velocities of a hcp  $\text{Fe}_{1-x}\text{Si}_x$  alloy in the limit of low to moderate Si concentration (0 to 9wt.%). The simplest approach is to use an ideal linear mixing model [e.g. Badro *et al.*, 2007; Antonangeli *et al.*, 2010]. Using the reference relations established here for pure Fe and the extrapolation of our measurements on Fe-Si9, at the inner

core density of  $13000 \text{ kg/m}^3$  we get a variation  $\sim +80 \text{ m/s}$  on  $V_P$  and  $\sim -80 \text{ m/s}$  on  $V_S$  for each wt.% of Si (Figure 6). Measurements of  $V_P$  on an Fe-Ni-Si alloy with 4.3wt.% Ni and 3.7wt.% Si [Antonangeli et al., 2010] extrapolated to  $13000 \text{ kg/m}^3$  yield  $V_P \sim 12100 \text{ m/s}$ , in good agreement with our estimate of  $V_P \sim 11980 \text{ m/s}$  for a Fe-Si alloy with 3.7wt.% Si (difference  $\sim -1\%$ ). This agreement argues in favor of the suitability of the here-proposed estimate. Moreover it suggests that the effect on the compressional sound velocity due to Ni inclusion at level of 4 to 5 wt.% is minor. Further independent support also comes from the good agreement observed between our predicted value of  $V_P \sim 12160 \text{ m/s}$  and the extrapolation of very new measurements on a Fe-Si alloy with 6wt.% Si [Sakairi et al., Am. Min. in press.] yielding  $V_P \sim 11940 \text{ m/s}$  (difference  $\sim +1.8\%$ ).

In order to use our data to assess the Si abundance in the inner core by comparison with seismological models, the effects of high temperature have to be accounted for. A velocity vs. density representation, as the one proposed here, implicitly accounts for quasi-harmonic effects, but anharmonic effects might be important as well, in particular on  $V_S$  and for temperatures approaching melting. Sound velocity measurements at simultaneous high pressure and high temperature conditions are at the cutting edge of current technical capabilities and only few datasets are available, mostly for pure Fe [e.g. Antonangeli et al., 2012; Mao et al., 2012; Ohtani et al., 2013; Sakamaki et al., 2015]. If we model high-temperature effects for Fe following Sakamaki et al. [2015],  $V_P$  is expected to be lowered by  $\sim -0.09 \text{ m/s K}^{-1}$  at the constant density of  $13000 \text{ kg/m}^3$ . The orange arrow in Figure 4 highlights the magnitude of the expected reduction of  $V_P$  for T up to  $\sim 7000 \text{ K}$ . Alternatively we can model temperature-induced softening (in this case for both  $V_P$  and  $V_S$ ) following calculations by Martorell et al., [2013]. As these calculations have been performed at constant pressure, while here we are interested in the effects at constant density, we corrected the computed values according to the measured density dependence of sound velocities to

compensate for the effects due to density variation with increasing temperature. Once limiting to  $T$  up to 7000 K, the estimated lowering of  $V_P$  and  $V_S$  are, respectively,  $\sim -0.12 \text{ m/s K}^{-1}$  and  $\sim -0.32 \text{ m/s K}^{-1}$  at the constant density of  $13000 \text{ kg/m}^3$ . The violet arrows in Figure 4 highlights the magnitude of the expected reduction of  $V_P$  and  $V_S$  for  $T$  up to  $\sim 7000 \text{ K}$ . In qualitative agreement with recent calculations, for Fe, temperature effects alone permit to match inner core velocities (but not densities, which remain too high for pressures in the range 330 to 360 GPa). In the case of Fe-Si alloys we can only rely on calculations [Martorell *et al.*, 2016], which, once corrected as in the case of Fe, yield for a sample with 3.2 wt% Si a reduction of  $V_P$  and  $V_S$  of, respectively,  $\sim -0.12 \text{ m/s K}^{-1}$  and  $\sim -0.34 \text{ m/s K}^{-1}$ , and for a sample with 6.7 wt% Si a reduction of  $\sim -0.20 \text{ m/s K}^{-1}$  and  $\sim -0.23 \text{ m/s K}^{-1}$ , at the constant density of  $13000 \text{ kg/m}^3$ . We note that theoretical estimates for pure Fe and a Fe-Si alloy with 3.2wt.% Si are very close, while those for a Fe-Si with 6.7wt.% Si differ, with an effect on  $V_P$  almost double and an effect on  $V_S$  about 30% smaller. The arrows in Figure 5 highlights the magnitude of the expected reduction of  $V_P$  and  $V_S$  for  $T$  up to  $\sim 7000 \text{ K}$  if we apply to our measurements on Fe-Si9 the correction estimated for samples with 3.2wt.% Si (dark blue arrows) or that for samples with 6.7 wt.% Si (green arrows). Similarly to the case of Fe, if temperature effects are as large as expected according to calculations, temperature alone might be enough to explain inner core velocities (but again, not the densities, too low for pressures in the 330 to 360 GPa range for samples with 9 wt.% Si [Tateno *et al.*, 2015]).

If we assume temperature effects at the constant density of  $13000 \text{ kg/m}^3$  of  $\sim -0.20 \text{ m/s K}^{-1}$  for  $V_P$  and  $\sim -0.23 \text{ m/s K}^{-1}$  for  $V_S$  (as from estimates from calculations on a sample with 6.7 wt% Si) we match PREM values of  $V_P$  and  $V_S$  for a Si concentration of  $10 \pm 1 \text{ wt.}\%$  and  $T$  between 6500 and 6700 K. This solution however is not acceptable, as such Fe-Si alloy is expected to have the right density only for pressures well above 360 GPa [Tateno *et al.*, 2015]. If we assume temperature effects at the constant density of  $13000 \text{ kg/m}^3$  of  $\sim -0.12 \text{ m/s K}^{-1}$  for

$V_P$  and  $\sim -0.33 \text{ m/s K}^{-1}$  for  $V_S$  (as from estimates from calculations on pure Fe and on a sample with 3.2 wt% Si) we obtain PREM values of  $V_P$  and  $V_S$  for a Si concentration of  $3 \pm 2$  wt.% and T between 6200 and 6500 K. P-V-T relation for a Fe-Si alloy with  $\sim 3$  wt.% Si has not been experimentally determined yet, but calculations suggest such an alloy to have a density of  $\sim 13160 \text{ kg/m}^3$  at 360 GPa and 6400 K [Martorell et al., 2016], thus making this solution acceptable. Furthermore, an inner core temperature of 6200-6500 K is compatible with estimates based on measurements of the Fe and Fe-Si alloys melting curve [Anzellini et al., 2013; Morard et al., 2011]. However, as already mentioned, the most recent experimental determination of temperature dependence of  $V_P$  for Fe by Sakamaki et al. [2016] argues for a less important temperature-induced lowering with respect to that proposed by calculations. If we assume temperature effects at the constant density of  $13000 \text{ kg/m}^3$  of  $\sim -0.09 \text{ m/s K}^{-1}$  for  $V_P$  as from Sakamaki et al. [2016], we match PREM value of  $V_P$  for  $\sim 1$  wt.% Si at 6300 K and  $\sim 2$  wt.% Si at 7300 K. The last solution is not acceptable as a Fe-Si alloy is not solid at such a high temperatures [Morard et al., 2011; Anzellini et al., 2013]. Furthermore, irrespectively whether we assume a temperature effect on  $V_S$  of  $\sim -0.33 \text{ m/s K}^{-1}$  (as from estimates from calculations on pure Fe and a Fe-Si alloy with 3.2 wt.% Si), or  $\sim -0.23 \text{ m/s K}^{-1}$  (as from estimates from calculations on Fe-Si alloy with 6,7 wt.% Si), or  $\sim -0.24 \text{ m/s K}^{-1}$  for  $V_S$  (scaling the estimates from calculations on pure Fe in line with the reduced effect on  $V_P$ ), there is no solution matching PREM values of  $V_P$  and  $V_S$  for a fixed Si content. Further constraints on the effects of high-temperature on sound velocities thus remain crucial to reliably estimate the Si content in the inner core.

## 5. Conclusions

We carried out sound velocity and density measurements on solid hcp-Fe and an hcp-Fe-Si alloy with 9 wt.% Si up to  $\sim 170$  and  $\sim 140$  GPa, respectively. The experimentally

established  $V_P$ - $\rho$  and  $V_S$ - $\rho$  relations for pure Fe are in good agreement with results from ab initio calculations and clearly show that both compressional and shear velocities scale linearly with density at 300 K (Figure 4). At 300 K and the inner core density of  $13000 \text{ kg/m}^3$ , the reference values for  $V_P$  and  $V_S$  are respectively  $11680 \pm 250 \text{ m/s}$  and  $5890 \pm 360 \text{ m/s}$ . Measurements on the Fe-Si alloy with 9 wt.% Si allowed us to discriminate between previous inconsistent datasets (Figure 5) and to propose  $V_P$ - $\rho$  and  $V_S$ - $\rho$  relations for Fe-Si9. These results are used to address the presence and abundance of Si in the Earth's inner core.

From a methodological standpoint, constraints coming only from density [e.g. *Tateno et al., 2015*] or even by combined density and compressional sound velocity [e.g. *Badro et al., 2007; Mao et al., 2012; Ohtani et al., 2013*] can be used to exclude possibilities, but it is necessary to simultaneously consider  $V_P$ ,  $V_S$  and  $\rho$  to propose a consistent composition for the Earth's inner core. Qualitatively, at inner core conditions, high temperature reduces sound velocities, even at constant density, while Si alloying at level of 9 wt.%, lowers  $\rho$ , increases  $V_P$  and decreases  $V_S$  with respect to pure Fe. These same effects have been very recently suggested by calculations on Fe-Si alloys [*Martorell et al., 2016*], as well as for carbon alloys [*Caracas, 2017*]. Assuming an ideal linear mixing model to be valid for low to moderate Si concentration ( $<10\text{wt.}\%$ ), we quantitatively evaluate the effect in  $\sim +80 \text{ m/s}$  on  $V_P$  and  $\sim -80 \text{ m/s}$  on  $V_S$  for each wt.% of Si at the inner core density of  $13000 \text{ kg/m}^3$ . Further studies on samples of intermediate compositions will allow refinement of this estimation.

We explored the possible solutions for an hcp-Fe-Si alloy whose density, compressional and shear sound velocities would match PREM values for pressures in the range 330 to 360 GPa and temperatures in the range 4000 to 7500 K. The existence of a solution and the amount of Si necessary to match the seismological observations strongly depends on the way we model anharmonic effects on sound velocities at high temperature and on core temperature. In particular, we obtain possible solutions only for large temperature corrections, relatively

high core temperatures (with  $T$  comprised between 6200 and 6500 K), and for Si content not exceeding  $3\pm 2$  wt.% Si. Accordingly, the current results do not support the presence of Si in the inner core at a level of 6 to 8 wt.% as recently proposed [Mao *et al.*, 2012; Fischer *et al.*, 2015; Tateno *et al.*, 2015]. On the sole basis of density and sound velocities systematics, we cannot discriminate between results proposing little (up to 4 wt.%) [e.g. Badro *et al.*, 2007; Antonangeli *et al.*, 2010] to no presence [Martorell *et al.*, 2016] of Si in the inner core. More experimental and theoretical work on Fe-Si alloys remains to be performed, so as to extend the directly probed pressure and temperature range and to check the limit of the ideal mixing approximation. We also encourage performing calculations not only at actual core conditions, but as well at conditions where experimental data exist, so as to validate theoretical treatments of alloys.

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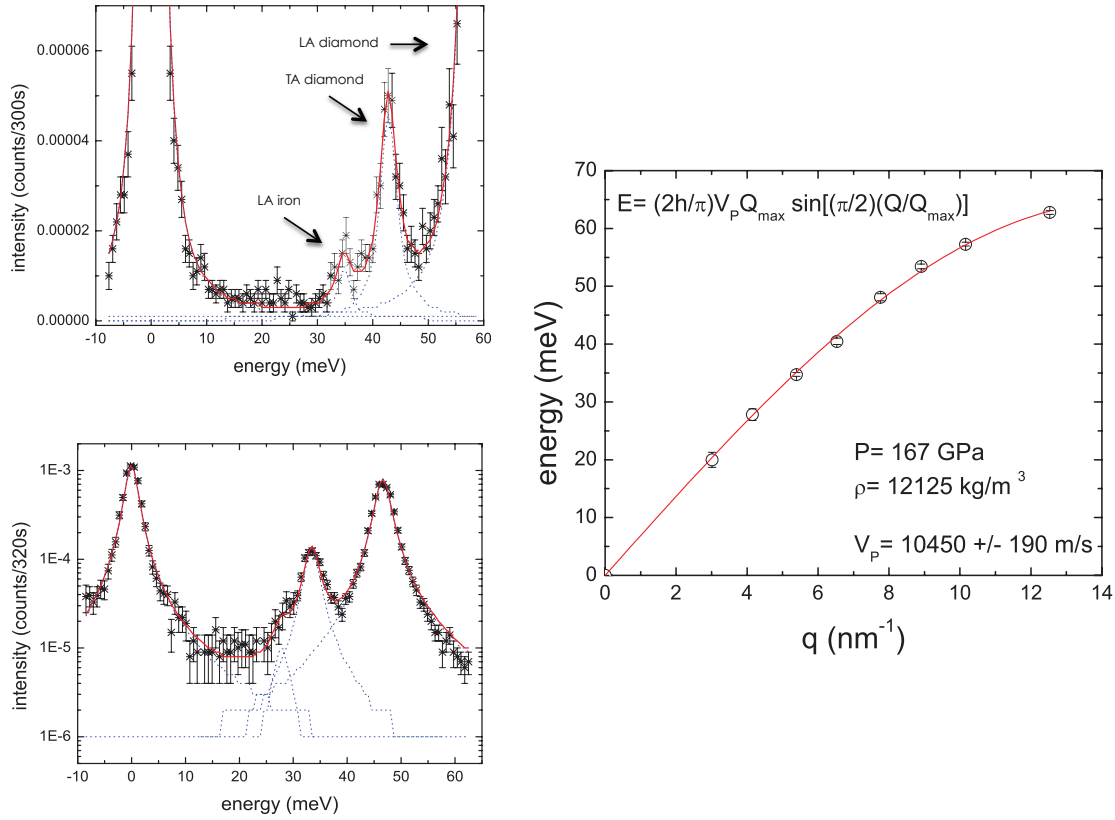
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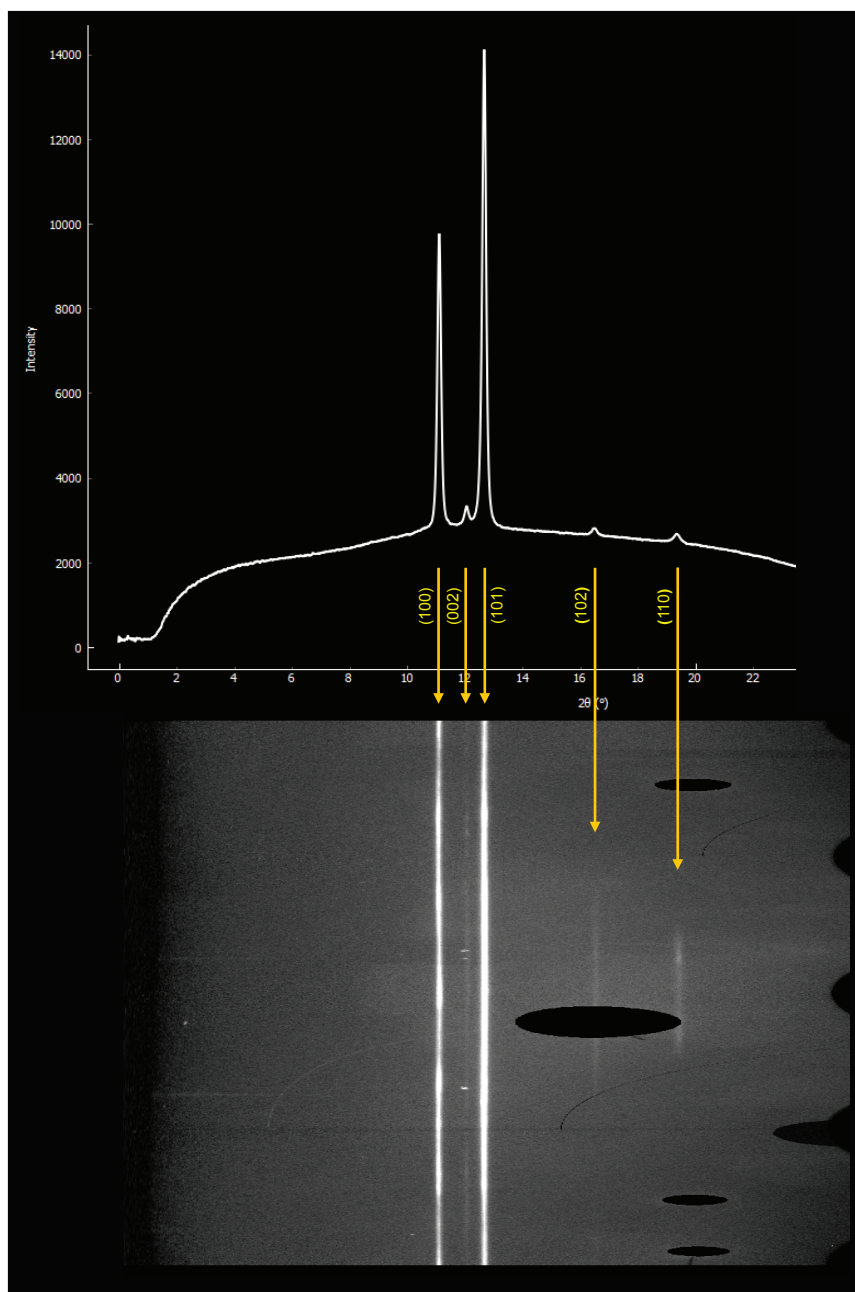
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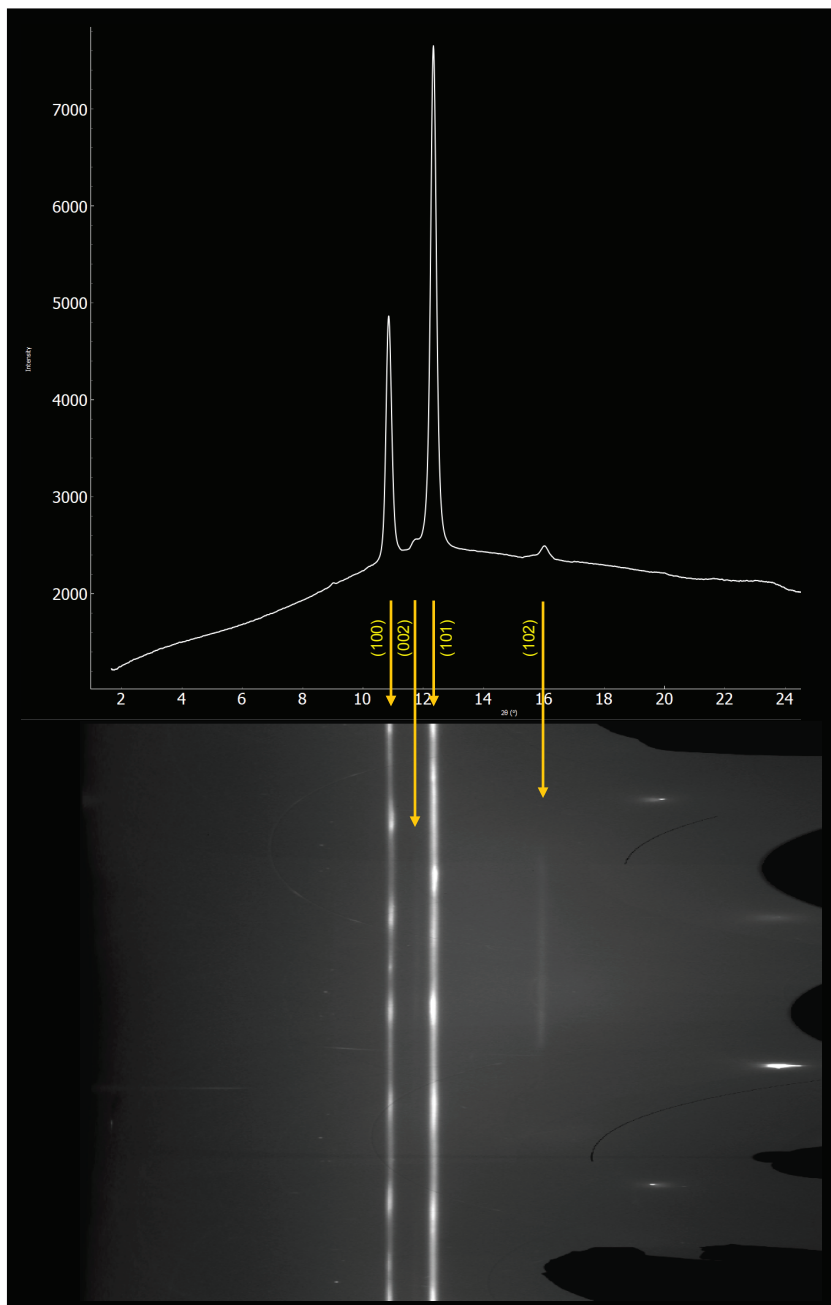
**Figure 1. Examples of IXS spectra (left) and aggregate phonon dispersion (right) obtained for pure-Fe at the highest investigated pressure ( $\rho=12125 \text{ kg/m}^3$ , corresponding to  $\sim 167 \text{ GPa}$ ). Up left: IXS spectrum for  $q=5.39 \text{ nm}^{-1}$ ; bottom left IXS spectrum for  $q=4.15 \text{ nm}^{-1}$ . IXS spectra are characterized by an elastic line, centered around zero, and inelastic features, assigned for increasing energy to the longitudinal acoustic (LA) aggregate phonon of iron and the transverse acoustic (TA) and longitudinal acoustic (LA) phonons of diamond. The experimental points and error bars are shown together with the best-fit (red line) and individual excitations (dashed blue lines). Sample phonons for  $q$  of  $5.39 \text{ nm}^{-1}$  and higher are well resolved and visible in linear scale, while for smaller  $q$  values, sample phonons and TA phonon of diamonds get very close, and sample phonons become a shoulder on the low-energy side of the TA phonon of diamond, better visible in logarithmic scale.**



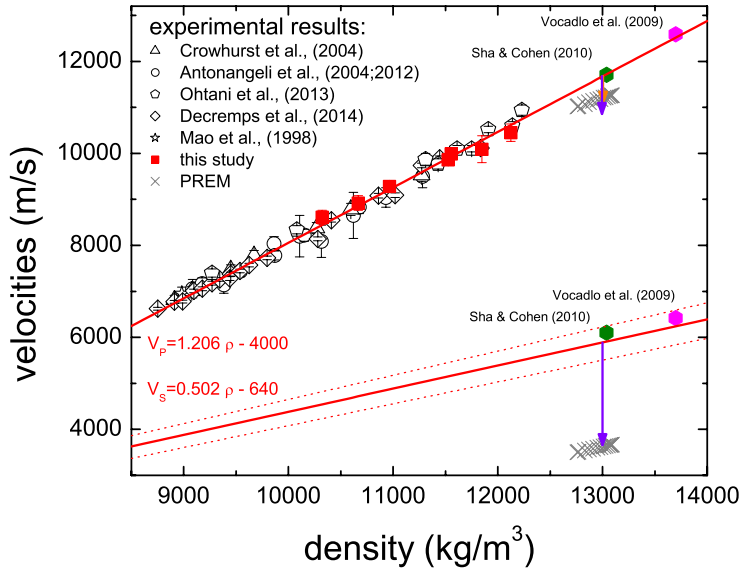


**Figure 2. Example of integrated diffraction pattern collected on pure hcp-Fe at P~167 GPa (top) and caked into a rectilinear projection (bottom). 2D diffraction images have been integrated using Dioptas [Prescher and Prakapenka, 2015].**

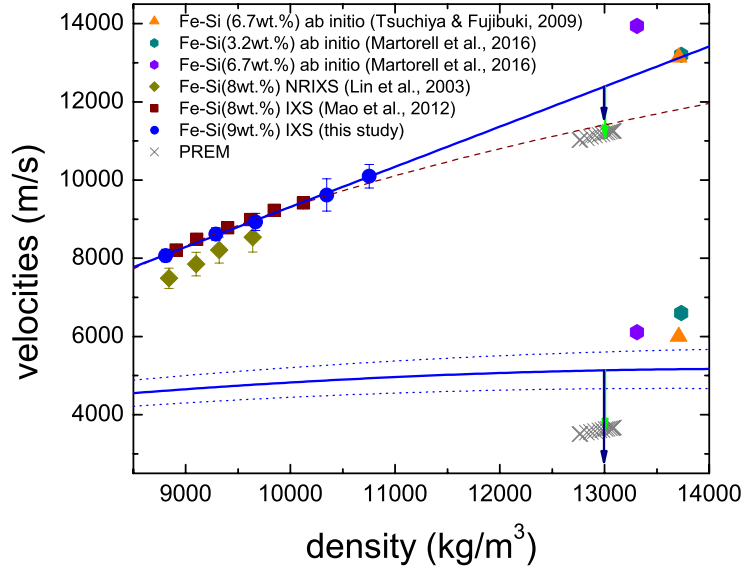




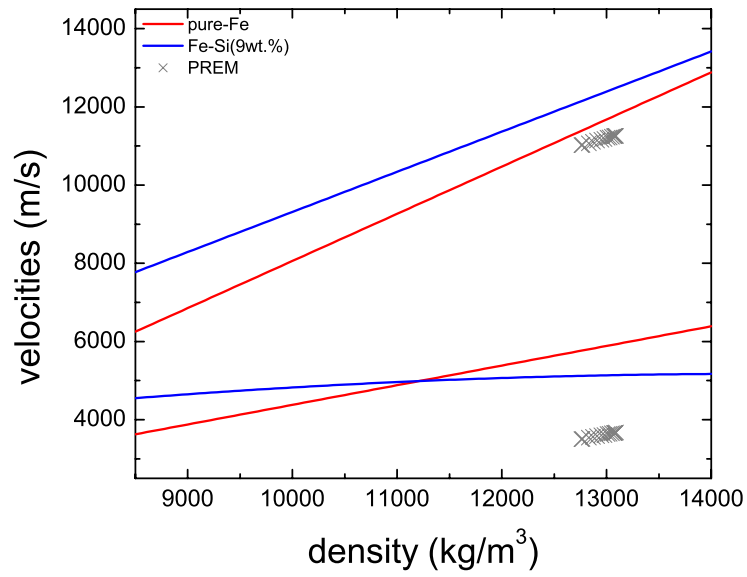
**Figure 3. Example of integrated diffraction pattern collected on hcp-FeSi9 at P~117 GPa (top) and caked into a rectilinear projection (bottom). 2D diffraction images have been integrated using Dioptas [Prescher and Prakapenka, 2015].**



**Figure 4. Aggregate compressional ( $V_P$ ) and shear ( $V_S$ ) sound velocities of hcp-Fe at 300 K as a function of density.** Results of this study are compared with a selection of published measurements at 300 K [Mao et al., 1998; Crowhurst et al., 2004; Antonangeli et al., 2004, 2012; Ohtani et al., 2013; Decremps et al., 2014] (for further details see Antonangeli and Ohtani [2015]), ab initio calculations at 0 K and 295 GPa [Vočadlo et al., 2009] and at 0 K and 13040 kg/m<sup>3</sup> [Sha and Cohen, 2010]. PREM [Dziewonski and Anderson, 1981] is reported as crosses. Solid lines show the established linear  $V_P$ - $\rho$  and  $V_S$ - $\rho$  relationships. Dotted lines show confidence level on the derived  $V_S$ . Arrows indicate possible magnitude of anharmonic effects up to 7000 K (see text).



**Figure 5. Aggregate compressional ( $V_P$ ) and shear ( $V_S$ ) sound velocities of hcp-Fe-Si9 at 300 K as a function of density.** Results of this study are compared with measurements at 300 K on a hcp-Fe-Si alloy with 8 wt.% Si by NRIXS [Lin et al., 2003] and by IXS [Mao et al., 2012] as well as with results of ab initio calculations at 0 K and 360 GPa on an hcp-Fe-Si alloy with 6.7 wt.% Si [Tsuchiya and Fujibuki, 2009] and at 0 K and 360 GPa on hcp-Fe-Si alloys with 3.2 and 6.7 wt.% Si [Martorell et al., 2016]. PREM [Dziewonski and Anderson, 1981] is reported as crosses. Solid lines show the proposed  $V_P$ - $\rho$  ( $V_P=1.026 \times \rho-946$ ) and  $V_S$ - $\rho$  ( $V_S=1530+0.503 \times \rho-1.736 \times 10^{-5} \times \rho^2$ ) relationships. Dotted lines show confidence level on the derived  $V_S$ . The dashed line is the empirical power-law function used by Mao et al., [2012] to describe their  $V_P$ - $\rho$  data. Arrows indicate possible magnitude of anharmonic effects up to 7000 K (see text).



**Figure 6. Comparison of the proposed density dependence of the aggregate compressional ( $V_P$ ) and shear ( $V_S$ ) sound velocities of hcp-Fe (red) and hcp-FeSi9 (blue) extrapolated to core density, along with PREM [Dziewonski and Anderson, 1981] shown as crosses.**

**Table 1. Measured densities and compressional sound velocities ( $V_P$ ).** Pressure estimated from measured diffraction patterns are reported as well. See text for discussion of pressure uncertainties and pressure gradients. Assuming different equation of state for hcp-Fe leads to a maximum difference in the reported pressure of less than 10 GPa at the highest density when using equation of state from Mao et al., [1990].

Sample	Density (kg/m <sup>3</sup> )	Pressure (GPa)	$V_P$ (m/s)
hcp-Fe	10325	63	8610±150
hcp-Fe	10665	79	8920±160
hcp-Fe	10965	96	9280±90
hcp-Fe	11525	124	9860±110
hcp-Fe	11555	126	9990±120
hcp-Fe	11850	146	10090±290
hcp-Fe	12125	167	10450±190
hcp-Fe-Si9 <sup>a</sup>	8805	42	8070±170
hcp-Fe-Si9	9285	59	8620±160
hcp-Fe-Si9	9665	79	8930±220
hcp-Fe-Si9	10350	117	9620±410
hcp-Fe-Si9	10755	144	10100±300

<sup>a</sup> This point have been collected on decompression.