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Full wave indoor measurements cross-validation with the model DEMOS for Foliage Penetrating applications

L. Hettak¹, H. Saleh^{2,3}, C. Dahon¹, M. Casaletti¹, O. Meyer⁴, J-M Geffrin², and H. Roussel¹

Abstract— For Foliage Penetrating (FoPen) radar development we developed previously a hybrid volume/surface model, named DEMOS, to evaluate the electromagnetic scattering from large scenes composed by targets (metallic objects) placed in a natural environment (dielectric object). In this paper, we compare the scattered field obtained by DEMOS with quasi-monostatic measurements done in an anechoic chamber on scaled models composed of dielectric and metallic structures. For all measurements, we consider both polarizations, HH and VV. Our final objective is to determine the optimal configurations for the detection of a target placed in a forest environment in the VHF-UHF frequency bands.

Index Terms—Monostatic measurements, radar detection, Foliage Penetrating.

I. INTRODUCTION

FoPen (Foliage Penetrating) radar development is very expensive because it requires several measurement campaigns to estimate the best radar configuration for target detection (incident angle, polarization, etc...). This justifies the interest in "full wave" electromagnetic models dedicated to the modeling of scattering of large forest areas in the presence of metallic targets or a human [1]-[2]. Such models could replace in the near future the first step of radar design thus limiting the number of measurement campaigns. Nevertheless, the implementation of such an electromagnetic model presents two main challenges. First, this requires taking into account a scene composed of highly heterogeneous media (lossy dielectric materials for the trees and metals for the target). Second, a large-sized scene (the focal spot of the UHF radar antenna could be up to $50 \times 50 \text{ m}^2$). Several full-wave techniques can be used to evaluate the field scattered by a mixed environment (dielectric and metallic media). In our case, we take advantage of an integral formulation that combine the volume integral equation (VIE) for the trees [3] with the surface ones (SIE) for the targets [4] and use the same Dyadic Green's function for both formulations to incorporate the interface air/ground [5]. We named our model DEMOS for Domain dEcomposition MOdel for the analysis of target Scattering in forested areas. This model has been numerically validated in the first step for a simple configuration with the commercial software FEKO [5].

Here we compare in amplitude and phase our model DEMOS with quasi-monostatic measurements performed in an anechoic chamber on scaled models combining metallic and dielectric elements. In order to be able to consider realistic scenes, a scale

factor of a twenty-fifth has been used on both geometry and frequency band of interest. This choice transforms the FoPen frequency band (320-480 MHz) into (8-12 GHz) fitting the operative bandwidth of our measurement platform, and allowing the measurement of scenes containing an electrically large target and trees.

This approach, already validated for forested areas [6]-[7] is now extended to the case of targets placed in a forest environment. The aim of this paper is to present cross-validations of our model DEMOS with measurements in an anechoic chamber.

II. FORMULATION

In order to consider realistic forest scenes and to overcome the limitations due to the huge number of unknowns, an Extended-CBFM (CBFM-E) compression scheme has been implemented in our model (DEMOS) [5]. The algorithm begins with the decomposition of the computational domain associated with the forest (trunks and branches) into blocks and proceeds to generate the characteristic basis functions (CBFs) for these blocks. In a second step, the number of CBFs retained for each block is much lower than the original number of low-level basis functions for the same block to obtain a significant compression ratio (ratio between the number of the original basis functions and the number of post-CBFM unknowns). This turns out in a significant reduction in terms of computational time and memory consumption compared to a conventional MoM (Method of Moments) approach [8].

III. MEASUREMENTS ON SCALED MODELS

Since environmental conditions and experimental uncertainties may dramatically influence the scattering, as well as the forest electromagnetic properties change during the year, the underlying idea is to carry out scaled-model measurements in an anechoic chamber. The measurements are made using the quasi-monostatic configuration in the anechoic chamber of the CCRM [9, 10]. Radar scattering models for a metal target existing in a forest environment are usually designed to operate in the VHF band between 320 and 480 MHz. The microwave analog situation is reduced with a scaling factor of 1/25 and the experiments are made in the frequency band from 8 to 12 GHz. The ground is represented by a flat metal plate with 1 m diameter, that is considered to be infinite in the model. The

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metal plate is glued on expanded polystyrene support, which is placed on the top of the central mast. The metal plate is present during the measurement of the total and incident fields. The targets to be measured are therefore aligned at the center of the metal plate. The measurements are made using X-band horn antennas and the residual bistatisme angle between them is 12° . The distance between the antennas and the origin O at the center of the metal plate is 1.648 m, which is around 41 m at the initial scale. The displacement of the wagon carrying the antennas on the vertical arch is denoted by the angle φ_s . The measurements are made in the two co-polarization cases $\theta\theta$ (VV) and $\varphi\varphi$ (HH) defined in Figure 1 and Figure 2. A metal squat cylinder was chosen as a reference target to calibrate the measured scattered field. The cylinder has a diameter of 95 mm and a height of 44.45 mm. During the measurement, the center of the cylinder is aligned at the center of the metal plate on one of its two parallel faces. It was chosen for two reasons: first, it has a relatively high electromagnetic signature which can overcome the experimental noise. Second, it is asymmetric in the measurement configuration so that its scattered field is variable with respect to the monostatic angle φ_s .

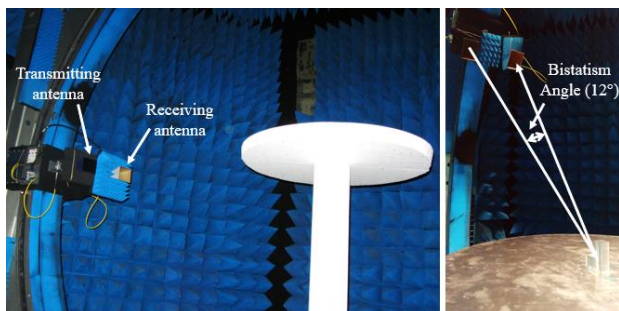


Figure 1: In the case of this picture the emitter and the receiver are moved on a semi-vertical arch during the scattering measurement in a quasi-monostatic configuration. The targets are placed on the metal disk supported by a polystyrene mast.

Our first comparison concerns a simple configuration composed of an L-shaped target placed on a metal plate (see Figure 2). In figure 3, we compare for the VV and HH polarizations the variations of the measured and computed fields with respect to the incident angle θ at 8 GHz and 11 GHz. We obtain a good agreement between the two results both in amplitude and phase.

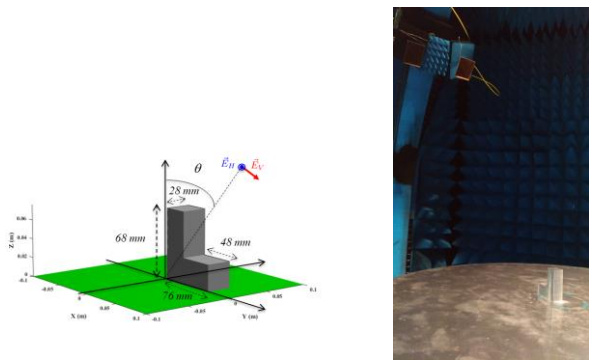


Figure 2: Geometry of the L-shaped target and image of the measurement

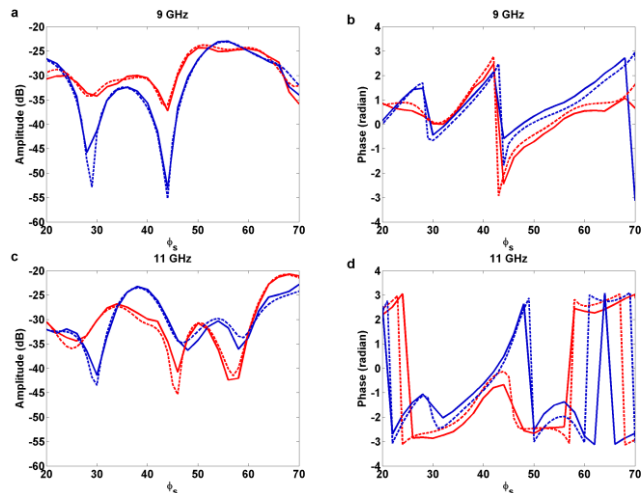


Figure 3: Comparison of the scattered field: Amplitudes (a, c) and Phases (b, d) of the measured (dashed) and calculated (solid) scattered fields by the L-shaped target placed on a metal plate for VV (blue) polarization and HH (red) polarization at 9 (a, b) and 11 GHz (c, d).

If we look at the holographic view of the field in figure 4, we observe a globally good agreement between measurements and simulations for both polarizations.

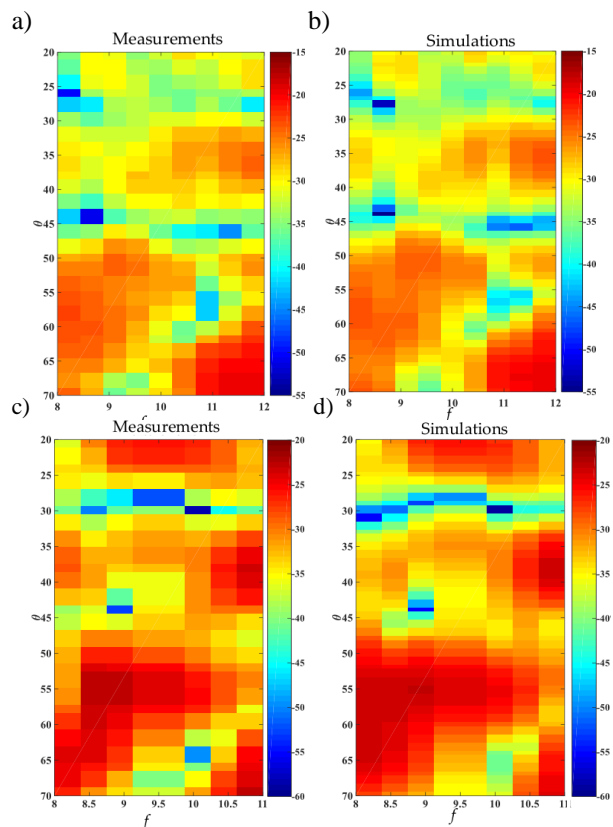


Figure 4: Holographic views for the frequency band 8-11 GHz and θ varying from 20 to 70° (measurements left and simulations right) VV polarization (a, b) and HH polarization (c, d)

For the second case, we consider the same metallic target associated with a high permittivity dielectric cylinder. Given that it is not simple to obtain a cylinder of high permittivity corresponding to wood permittivity [11], we have chosen to make the dielectric cylinders ourselves, first we printed with a

3D printer a hollow cylinder in ABS and in a second phase we filled it with a liquid composed of a 76% glycerol part and of 24% water. The variation of the permittivity of this liquid has been measured at 25°C in the frequency band 8-12 GHz. The dielectric characterization system consists of a junction between a coaxial waveguide connected to an Agilent E8364C vector network analyzer on a side and a cylindrical cell at the other side. This cell is made up of a circular 7 mm diameter waveguide filled up by a liquid under test, terminated by a short circuit [12]. A dielectric coaxial tight window is inserted between the waveguide and the cell. The device is connected to the vector network analyzer [13-14]. The real part of the relative permittivity varies from eight to ten and the imaginary part from six to nine. The height of the cylinder is 16 cm which corresponds to 4 m for the transposed size. This height is so comparable to that of a tree of medium height. Since we want to study the masking effect of the target by the trees, we measured the scattered field for three positions of the cylinder: ahead, beside and behind the target (Figure 5).

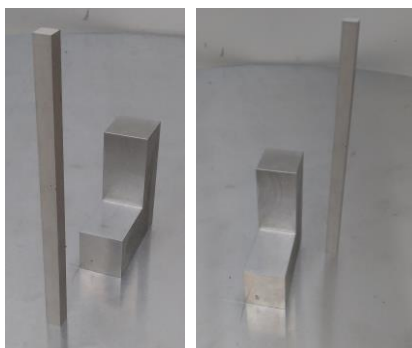


Figure 5: View of two measured configurations (ahead and beside)

In figure 6 we compare for the HH and VV polarizations the variations of the measured and scattered fields with respect to the incident angle θ at 8 GHz and 11 GHz when the cylinder is beside and behind the target respectively. We notice a good agreement between measurements and simulations since the permittivity of the dielectric bar is not perfectly mastered.

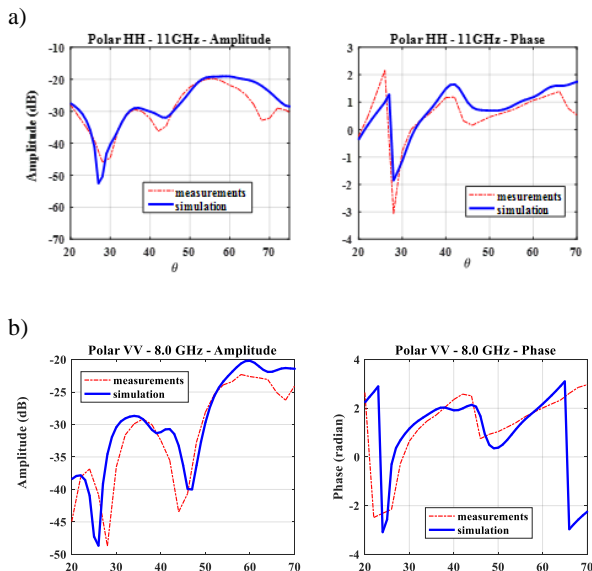


Figure 6: Comparison of the scattered field: Amplitudes and Phases measured (red) and calculated (blue) scattered fields by the L-shaped target and a dielectric cylinder placed on a metal plate for VV polarization at 8 GHz (b) and HH polarization at 11 GHz (a) when the cylinder is beside (a) or behind (b) the target.

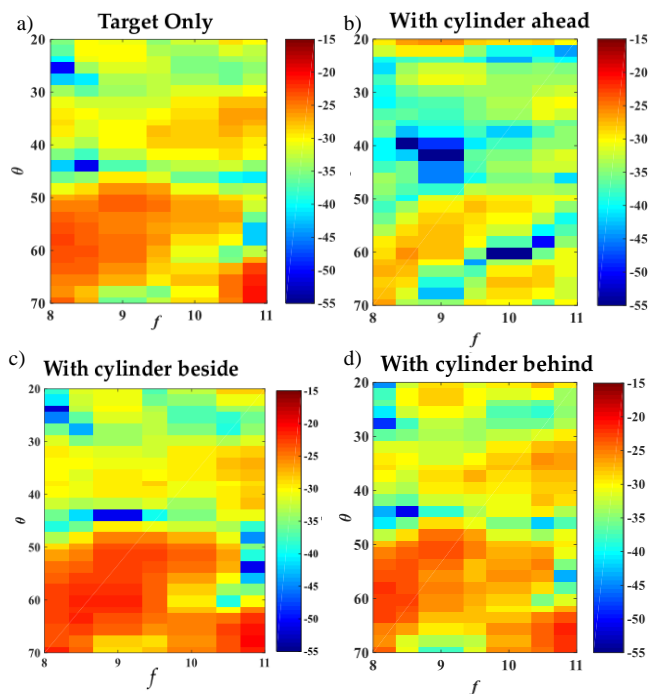


Figure 7: Holographic views of measurements in VV polarization for the frequency band 8-11 GHz and θ varying from 20° to 70° for the 4 configurations: a) Target only, b) Position 1 (target with cylinder ahead), c) Position 2 (target with cylinder beside) and d) Position 3 (target with cylinder behind)

In figure 7 and 8 we give the variations of the measured scattered field for both co-polarization VV and HH, with respect to the incident angle θ and frequency when we consider four different configurations: the target only, the target with the cylinder ahead, beside and behind. We compare only measurements in order to evaluate the masking effect of the cylinder. We observe that when the cylinder is ahead of the target, the level of the field diffracted by the target is strongly attenuated for the VV polarization. On the other hand, for the HH polarization, this masking effect is less pronounced. Furthermore, the level of the diffracted field by the target is stronger for angles beyond 50°. This observation was reproduced on a measurement made on a much more complex configuration composed of a model of tank placed in the middle of a set of five trees with branches (see figure 9). These measurements (figure 10) suggest that the HH polarization will facilitate the detection of hidden targets undercover and that the observation angles above 50° should be preferred.

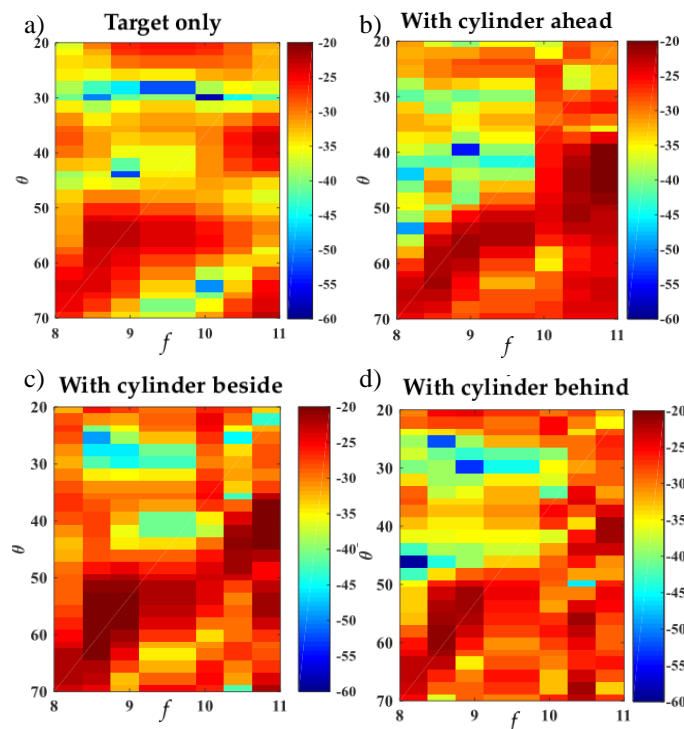


Figure 8: Holographic views of measurements in HH polarization for the frequency band 8-11 GHz and θ varying from 20° to 70° for the 4 configurations: a) Target only, b) Position 1 (target with cylinder ahead), c) Position 2 (target with cylinder beside) and d) Position 3 (target with cylinder behind)



Figure 9: View of scaled tank placed in the middle of the five scaled trees

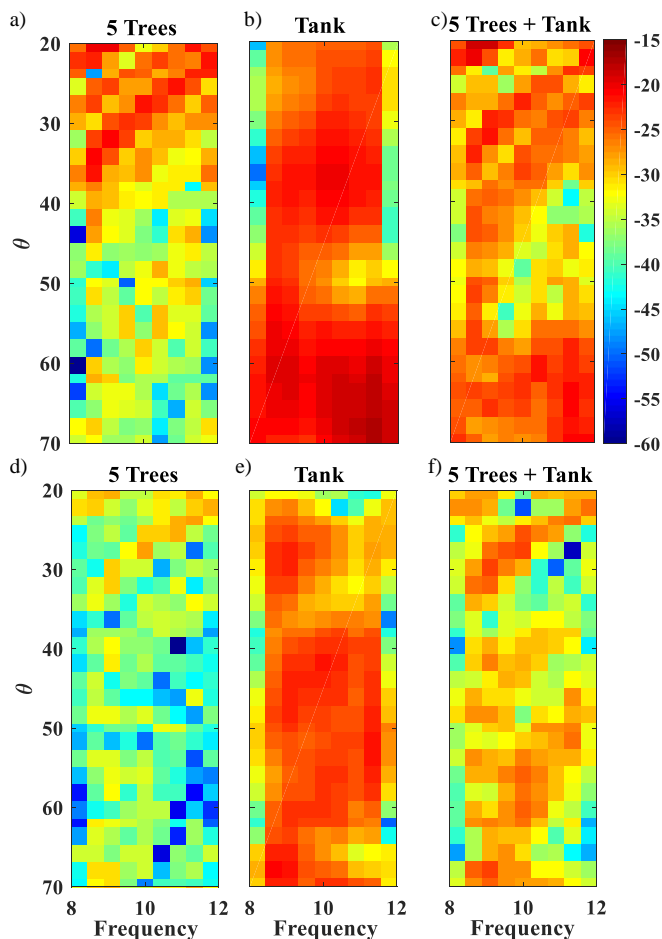


Figure 10: Holographic views of measurements for the frequency band 8-12 GHz and θ varying from 20° to 70° for the tank placed in the middle of 5 trees Legend : (a, d) Only the 5 trees (b, e) only the tank, (c, f) the tank and the 5 trees (a, b, c) HH polarization (d, e, f) and VV polarization.

IV. CONCLUSION

We propose in this paper to compare a hybrid MoM formulation that considers metallic targets inside a forest environment with measurements in an anechoic chamber. In a first step, we give validation of our model with measurements and in a second step an interpretation on measurements on scaled models. In the future, we will consider bi-static configurations and cross polarisations for measurements.

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