



HAL
open science

Automatic Calibration of Bed Friction Coefficients to Reduce the Influence of Seasonal Variation: Case of the Gironde Estuary

Nicolas Huybrechts, Hassan Smaoui, Sylvain Orseau, Pablo Tassi, Fabrice Klein

► **To cite this version:**

Nicolas Huybrechts, Hassan Smaoui, Sylvain Orseau, Pablo Tassi, Fabrice Klein. Automatic Calibration of Bed Friction Coefficients to Reduce the Influence of Seasonal Variation: Case of the Gironde Estuary. *Journal of Waterway, Port, Coastal, and Ocean Engineering*, 2021, 147 (3), pp.05021004. 10.1061/(ASCE)WW.1943-5460.0000632 . hal-03196183

HAL Id: hal-03196183

<https://hal.sorbonne-universite.fr/hal-03196183>

Submitted on 12 Apr 2021

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

1 Automatic calibration of the bed friction coefficients to reduce the influence of their seasonal
2 variation: the case of the Gironde estuary

3 Nicolas Huybrechts¹, Hassan Smaoui², Sylvain Orseau³, Pablo Tassi⁴ and Fabrice Klein⁵

4 ¹ Researcher, Cerema Direction Technique Eau, Mer et Fleuves and Sorbonne Universités, université de
5 technologie de Compiègne, CNRS, FRE 2012 Roberval, Centre de recherche Royallieu, CS 60 319, 60203
6 Compiègne cedex – France. nicolas.huybrechts@cerema.fr

7
8 ² Researcher, Cerema Direction Technique Eau, Mer et Fleuves and Sorbonne Universités, université de
9 technologie de Compiègne, CNRS, FRE 2012 Roberval, Centre de recherche Royallieu, CS 60 319, 60203
10 Compiègne cedex – France. hassan.smaoui@cerema.fr

11
12 ³ Post doc, Cerema Direction Technique Eau, Mer et Fleuves and Sorbonne Universités, université de
13 technologie de Compiègne, CNRS, FRE 2012 Roberval, Centre de recherche Royallieu, CS 60 319, 60203
14 Compiègne cedex – France. sylvain.orseau@cerema.fr

15
16 ⁴ Researcher. Electricity of France, R&D Department, 6 quai Watier, BP 49, 78401 Chatou Cedex, France.
17 Laboratoire d'Hydraulique Saint Venant (ENPC-EDF/R&D-CEREMA), 6 quai Watier, BP 49, 78401 Chatou Cedex,
18 France. pablo.tassi@edf.fr

19
20 ⁵ Engineer. Grand Port Maritime de Bordeaux, 152 quai de Bacalan - CS 41320 – 33082 BORDEAUX CEDEX,
21 France. f-klein@bordeaux-port.fr

22

23

24

25

26

27

28

29

30

31

32 ABSTRACT

33 An automatic procedure to identify the bed friction coefficient is tested on a 2D hydrodynamic
34 model of the Gironde estuary (France). The proposed procedure involves an optimization
35 algorithm based on evolution strategy, namely CMA-ES (Covariance Matrix Adaptation
36 Evolution Strategy). Without optimization, application of the same friction distribution to
37 different hydrological conditions leads to significant relative error in water level prediction up
38 to 20-30%. For the tested configuration, 300 runs seemed to be sufficient to reach an optimal
39 value whereas additional 200 runs would help to gain an accuracy of few millimetres (or 0.3%).
40 In order to reach the same level of accuracy for the different hydrological configurations, it is
41 necessary to adapt for each configuration the bed friction coefficient. Such behaviour tends
42 to confirm a seasonal variation of the friction coefficient and this particularly in the central
43 part of the estuary. Different relationships of the friction coefficient according to the flowrate
44 have been incorporated inside the 2D hydrodynamic model. These relationships effectively
45 allow to maintain an accurate prediction of the water levels close to 10% for a wide range of
46 hydrological configurations.

47

48

49

50

51

52

54 INTRODUCTION

55 The tide propagation inside estuary is mainly affected by the modification of the flow section
56 and by energy losses due to bed friction (Le Floch 1961). Converging sections tend to increase
57 the tidal amplitude whereas bottom friction rather decreases this amplitude (Le Floch 1961).
58 In the estuarine upper part, the interactions between tide and river discharge also impact the
59 tidal propagation (Moldwin 2016). For instance, the flowrate magnitude influences the
60 location of turbidity maximum (TM) and associated mud deposition (Sottolichio et al 2001).
61 The presence of fresh mud deposit induces a modification of the bottom friction (van Rijn
62 2007) and thus the tide attenuation. In contrast, harmonic analysis is generally used by
63 harbours to predict the water level (Moldwin 2016). Prediction based on harmonic analysis is
64 valid for harbours located near the shore but it becomes less accurate for ports located inside
65 the estuary where interaction between river and tide becomes significant. A typical example
66 is the Port of Bordeaux located 100 km upstream the mouth of the Gironde estuary. The
67 macrotidal Gironde Estuary is located in South-West France covering a surface of 635 km²
68 from the Bay of Biscay to 170 km landward (Fig. 1). The estuary is characterized by a complex
69 geomorphology, high turbidity levels up to 20 g.l⁻¹ and a heterogeneous bed composition
70 (Allen 1972, Castaing 1981). Over the years, a large number of hydrodynamic models with
71 different complexity levels have already been developed. These models generally aimed at
72 tracking the turbidity maximum zone (Sottolichio et al 2001, Jalon-Rojas *et al.*, 2015) with two-
73 dimensional vertical (2DV) or three-dimensional approaches (3D) to compute the
74 hydrodynamics, sediment transport, and salt intrusion. Alternatively, Huybrechts *et al.* (2012)
75 proposed a 2D depth-averaged horizontal model (2DH) that showed to be a good compromise
76 between computational cost and accurate solution to efficiently capture the main

77 hydrodynamic processes. Fast and robust models are indeed required in operational tools
78 applied to various alert control systems, including flood control application (Laborie *et al* 2014)
79 and transport processes, such as sediment matter (Huybrechts and Villaret 2013, Orseau *et*
80 *al.* 2020a), or pollutants in the environment. The model developed by Huybrechts *et al.* (2012)
81 has been further applied to forecast the ship welcoming capacity inside the Gironde estuary
82 for an interval of 36 hours (Orseau *et al* 2020b). Huybrechts *et al.* (2012) calibrated the bed
83 friction coefficients by a trial and error procedure in order to reach water level differences
84 lower than 15 cm at the estuary mouth (Verdon, Fig. 1) and at the central part of the estuary
85 (Pauillac, Fig. 1). The calibration and the validation of this model have been performed with
86 field measurements acquired in August 2006 and October-November 2009. These two events
87 are characterized by low river discharges and calm weather conditions. The hydrodynamic
88 model included river and tidal forcing whereas storm surges were not considered. The update
89 of the Huybrechts *et al.*'s model (2012) to recent bathymetric information coming from up-to-
90 day bathymetric surveys makes therefore necessary to assess the validity of the previous
91 friction calibration procedure. In contrast to a flood control application where a robust
92 calibration is needed especially for high water levels or storm conditions, a ship route plan
93 requires a robust calibration for a wider range of hydrological condition. Therefore, the
94 accuracy of the model needs to be evaluated under different flow scenarios and weather
95 conditions. Since the trial and error methodology is not suitable to build a friction calibration
96 procedure valid for different hydrological conditions, it is rather proposed to couple the
97 hydrodynamic model with an optimization tool. As discussed by Dung *et al.* (2011), automatic
98 calibration is becoming popular for water-related applications mainly for groundwater,
99 watershed applications. Application of the proposed methodology to large scale and unsteady
100 hydrodynamic model, as observed for estuaries, is still rare (Dung *et al.* 2011) due to the

101 required computational resources. The automatic calibration of physical coefficients looks for
102 solution of an inverse problem. This solution corresponds to the minimization of the error
103 between the experimental results (field data) and the results estimated by a numerical model
104 (called direct model). To solve this inverse problem, two different methods have been
105 proposed (Fletcher, 1980-1981; Holland, 1975): gradient-based and meta-heuristic methods.
106 The first category uses the objective function gradient to search for the optimum, while the
107 second randomly searches for the optimum in a set of solutions (called the population of
108 individuals). The gradient-based methods require that the objective function satisfies
109 regularity conditions (differentiability, convexity). In addition, if the function has several local
110 optima, these methods will be more likely to converge towards a local optimum than a global
111 one. Meta-heuristic methods have been introduced to circumvent the disadvantages of the
112 gradient-based methods. These methods will not use the calculation of the gradient of the
113 objective function, but will explore the global search space based on stochastic processes
114 on a population of individuals rather than on a single individual (solution). Meta-heuristic
115 methods have the advantage of: (i) they are based on a random search and are therefore able
116 to explore the whole space of the solution; (ii) the objective function does not have to be
117 continuous allowing an efficient search for discrete problems, and (iii) they are robust,
118 offering the guarantee of convergence towards the global optimum. However, these methods
119 have the disadvantage of been computational costly at reaching the optimum since they are
120 based on an iterative procedure with slow convergence (Rudolph, 1994; Smaoui et al. 2018-
121 2019). In Geosciences, several meta-heuristic methods have been proposed, e.g. instance
122 genetic algorithms (GA, Goldberg, 1989); simulated annealing (SA, Kirkpatrick et al., 1982);
123 particle swarm optimization (PSO, Eberhart and Kennedy, 1995); ant colony optimization
124 (ACO, Dorigo and Gambardella, 1997); cat swarm optimization (CSO, Ch and Tsai, 2007),

125 differential evolution (DE, Storn and Price, 1997) and evolution strategy (ES, Baeck et al.
126 2000a, 2000b)

127 In the present study, the Covariance Matrix Adaptation Evolution Strategy (CMA-ES, Hansen
128 and Ostermeier 1996) is applied to the 2DH hydrodynamic model of the Gironde estuary. This
129 meta-heuristic algorithm is first performed on six hydrological events selected between April
130 and August 2015 with different flowrate values. The period was selected based on the
131 availability of storm surges information provided by Météo-France. From these tests, results
132 are analysed in term of accuracy and friction distribution. Finally, the robustness of the
133 methodology is assessed by considering the effect of the mesh discretization and the number
134 of friction zones.

135 **STUDY AREA**

136 The Gironde Estuary's width reaches 20 km at the mouth and decreases to 3 km downstream
137 the confluence of the Dordogne and the Garonne Rivers. The tidal range varies from 1.5 m
138 during neap tides to 5.5 m during spring tides at the mouth. Both Dordogne and Garonne
139 contributions to the freshwater discharge are estimated to 35% and 65%, respectively
140 (Sottolichio, 1999). Based on the bed composition, the estuary can be decomposed in 3
141 different zones comprising (i) a sandy facies in the estuary mouth; (ii) a mixed facies
142 dominated by mud along the central part and (iii) a fluvial estuary, in the most upstream parts,
143 characterised by the presence of sand, pebbles and gravels (Allen 1972). Fine suspended-
144 sediments observed in the Gironde Estuary compose a pronounced Turbidity Maximum Zone
145 (TMZ) with concentrations ranging between 1 and 20 g/l (Sottolichio and Castaing, 1999). Its
146 location along the estuary depends on hydrological conditions (Castaing, 1981; Jalón-Rojas,
147 2015).

148 For the year 2015, a harmonic analysis (Pawlowicz *et al.*, 2002) on measured water levels is
 149 performed month by month at Verdon (mouth), Pauillac (central part) and Bordeaux (Port)
 150 tidal gauge stations (Fig. 1). Variations of the M₂ amplitude according to the monthly averaged
 151 discharge at previous stations are illustrated on Fig. 2.

152 At the mouth, a slight increase of the M₂ amplitude from 1.44 to 1.53 m with the flowrate is
 153 observed. In the central part of the estuary, the M₂ amplitude increases progressively until a
 154 relatively constant value. Conversely, the M₂ amplitude tends to decrease at Bordeaux when
 155 flowrate is increasing from 400 to 1200 m³/s. A maximum value is reached around 300 m³/s.
 156 For the lowest flowrate values, M₂ amplitude is then also decreasing probably due to a
 157 migration of the turbidity maximum further upstream Bordeaux in the Garonne River (Jalón-
 158 Rojas *et al.* 2018).

159 MATERIALS AND METHODS

160 Hydrodynamic model

161 The hydrodynamics is computed by a two-dimensional formulation based on the solution for
 162 the depth-averaged shallow water equations (Eq. 1), with appropriate initial and boundary
 163 conditions:

$$164 \quad \frac{\partial h}{\partial t} + \frac{\partial(hU)}{\partial x} + \frac{\partial(hV)}{\partial y} = 0$$

$$165 \quad \frac{\partial U}{\partial t} + \frac{\partial(UU)}{\partial x} + \frac{\partial(UV)}{\partial y} = -g \frac{\partial Z}{\partial x} + \frac{1}{h} \frac{\partial}{\partial x} \left(hv \frac{\partial U}{\partial x} \right) + \frac{1}{h} \frac{\partial}{\partial y} \left(hv_t \frac{\partial U}{\partial y} \right) - \frac{g}{h} \frac{1}{K^2 h^{\frac{1}{3}}} \|\vec{U}\| U + S_x$$

$$166 \quad \frac{\partial V}{\partial t} + \frac{\partial(UV)}{\partial x} + \frac{\partial(VV)}{\partial y} = -g \frac{\partial Z}{\partial y} + \frac{1}{h} \frac{\partial}{\partial x} \left(hv \frac{\partial V}{\partial x} \right) + \frac{1}{h} \frac{\partial}{\partial y} \left(hv_t \frac{\partial V}{\partial y} \right) - \frac{g}{h} \frac{1}{K^2 h^{\frac{1}{3}}} \|\vec{U}\| V + S_y$$

168 where h is the water depth [m], \vec{U} is the depth-averaged flow velocity vector [m/s], with east-
169 west, north-south components U and V , respectively, $\|\vec{U}\|$ is the velocity norm, g is the
170 gravity acceleration [m²/s], Z is the free surface elevation [m], ν is the momentum diffusion
171 coefficient [m²/s], ρ is the water density [m³/kg], K is the Strickler-Manning coefficient
172 [m^{1/3}/s], S_x and S_y are additional source terms. The Strickler coefficient used for the bed
173 friction is just the inverse of the Manning coefficient. The mathematical system is therefore
174 composed of 3 equations and 5 unknowns (h , U , V , K and ν). Bed friction and diffusion
175 coefficients (K and ν) are provided by additional closure relationships or imposed values. A
176 constant value equal to 1 m²/s is imposed for the diffusion coefficient over the whole
177 numerical domain. In the shallow water equations, the bed friction term is included in the
178 source term of the momentum equation.

179 The module TELEMAC-2D of the TELEMAC-MASCARET modelling system (Hervouet 2007) is
180 applied in this study to solve the shallow water equations (Eq. 1), with the finite element
181 method. The computational domain is comprised from 30 km offshore the estuary mouth to
182 180 km landward up to the limit of the tidal dynamic and extends to 20 km from the North to
183 the South (Fig. 1). The mesh is unstructured and composed of triangular elements. Two
184 different meshes with different element size resolutions are used in this work: the mesh 1
185 containing 28000 nodes and the mesh 2 containing 76000 nodes (Fig. 3). The distance
186 between nodes of mesh 1 ranges within 1000 - 2000 m offshore 300 m in the central part
187 (Fig.3a), and within 75-200 m in the tributaries (Fig. 3c). Mesh 2 features an enhanced
188 resolution along the navigation channel: within 300-2000 m offshore, within 60-300 m in the
189 central part (Fig.3b) and within 33-100m upstream the confluence of both tributaries (Fig. 3d).

190 Measured river discharge is imposed at fluvial boundaries for both Gironde tributaries (Fig. 1).
191 At the maritime boundary, astronomic tide elevation and tidal currents are reconstructed
192 using NEA tidal atlases (North East Atlantic, Pairaud et al 2008, Huybrechts et al 2012) as a
193 superposition of harmonic waves (Schureman 1958) for each of the nodes of the offshore
194 boundary (Eq. 2).

195

$$196 \quad H_{tide} = H_0 + dH_0(t) + \sum_n H_n f_n \cos(\sigma_n t - g_n + V_n - u_n)$$

197

Eq. 2

198 where H_{tide} = the tidal height; H_0 = the mean height of the water level; n = the harmonics
199 number; H_n = the mean amplitude of the n -wave; f_n = the nodal correction for the
200 amplitude; σ_n = the frequency; t = the time; g_n = the phase lag of the equilibrium tide; V_n =
201 the astronomic argument; and u_n = the nodal correction for the phase lag. dH_0 is the storm
202 surge contribution.

203 Sea levels variation due to storm surges are applied to the tidal signal to improve water level
204 predictions. Storm surge data are provided by a Météo-France model and computed every 10
205 minutes at 12 nodes located along the maritime boundary. Linear interpolation is then
206 performed to incorporate surge values for each boundary node. In the previous study,
207 Huybrechts et al (2012) decomposed the bed friction into 4 different zones delineated as:
208 mouth, central part and tributaries. In the present work the number of zones is firstly
209 increased up to 7 zones K_i (Fig. 1b) to better characterize the bed roughness of the estuary's
210 tributaries. Finally, a configuration accounting for two additional friction zones located at the
211 central part of the estuary is considered (Fig. 1c). The delineation between the mouth and the
212 central part of the estuary (respectively zone 1 and zone 2, Fig. 1b) corresponds to a change

213 in the bed material from sand to mud, respectively. Other remaining delineations are
214 arbitrarily defined mainly based on the geometrical features of the water body.

215 **Optimization algorithm**

216 The optimization algorithm implemented in this work is based on the evolutionary strategy
217 algorithm (ESA, Baeck et al. 2000a, 2000b, Dréo et al. 2005). According to the Darwin's theory,
218 evolution will produce at the long-term organisms more adapted to their environment (Dréo
219 et al. 2005). Thus, in order to achieve better results, ESAs evolve in a set (called *population*) of
220 solutions (called *individuals*) and a searching root on a random population instead of an
221 individual. Research on a population increases the probability to find the optimum among
222 individuals. During the iterative process (called generation) leading to the optimal solution,
223 the populations evolve according to selection and variation cycles. From the ESA family, we
224 have adopted the CMA-ES algorithm. This algorithm, due to Hansen and Ostermeier (1996),
225 has been proposed to improve several aspects of the others ESA but specially to overcome
226 the main issues of the optimization solvers based on genetic algorithms (España et al 2017).
227 CMA-ES offers good performance in optimizing functions that are not regular enough or even
228 undefined explicitly. The CMA-ES search space has the advantage of evolving real numbers
229 set, thus avoiding the coding/decoding steps that characterize the genetic algorithms (GA).
230 However, a complete description of the CMA-ES is out of the present scope. It is worth noting
231 that metaheuristic optimization methods such CMA-ES can be effectively coupled with other
232 numerical models to identify some parameters model not accessible from measurements
233 (Bayer and Finkel, 2004; Elshall et al. 2015; Smaoui et al. 2018 and Smaoui et al., 2019).
234 Additional details are provided in the Appendix whereas full descriptions of the algorithm are

235 available in Hansen and Ostermeier (2001); Hansen et al. (2003), Dréo et al. (2005) or Hansen
236 (2006 & 2016).

237 **Coupling between the hydrodynamics module and the optimization algorithm**

238 The coupling interface between the optimization algorithm (CMA-ES) and the hydrodynamic
239 module (TELEMAC-2D) is performed with the multi-paradigm numerical computing
240 environment and proprietary programming language Matlab©, developed by MathWorks
241 (Moler and Little 2020). The specificity of each application relies on the way of building the
242 objective function. In our application involving 2D hydrodynamic modelling, the unknowns are
243 the values of the different bed friction coefficients and the variable to optimize is the
244 difference between measured and computed water levels. The coupling flowchart between
245 the hydrodynamics module and the optimization algorithm is illustrated on Fig. 4.

246 An initial distribution of the bed friction coefficient is provided. A steering subroutine is
247 implemented to build the objective function. This subroutine calls the module TELEMAC-2D
248 for launching the numerical simulations, it post-processes the numerical results and it
249 evaluates the RMSRE (Root Mean Square Relative Error, Eq. 4) between the computed water
250 level depending on the friction distribution (Z_c , Fig. 4) and the measurement (Z_m , Fig. 4). The
251 RMSRE is estimated at 8 tidal gauge stations (Fig. 1): Verdon, Laména, Pauillac, Medoc, Ambes,
252 Bordeaux, Cadillac, Libourne. The first six stations are located along the navigation channel.
253 Cadillac station located more upstream in the Garonne River, while Libourne station located
254 in the Dordogne River.

255 The CMA-ES algorithm searches for minimizing the mean value of the RMSRE of the 8 stations.

256 The minimized value is referred as RMSRE_m (m for mean between the 8 stations). For each

257 station, the RMSRE is computed by (Eq. 3):

258

259

$$RMSRE = \frac{\sqrt{\frac{1}{n} \sum_{i=1}^n (Z_{mi} - Z_{ci})^2}}{Z_m}$$

260

Eq. 3

261 Where Z_{mi} is the measured water levels [m] at a gage station and Z_{ci} is the computed values, n
262 the number of “ i ” observations and Z_m the mean measured value.

263 **RESULTS**

264 **Convergence of the algorithm depending hydrological conditions**

265 Six hydrological events are selected from April to August 2015 with flowrate varying from 150
266 to 1300 m³/s in the Garonne River and from 200 to 1500 m³/s in the central part considering
267 the Dordogne contribution. Each event is simulated with 500 runs covering a period of 6 days.
268 The same initial friction distribution defined from Huybrechts et al (2012) is applied to all
269 configurations. The configuration with 7 friction zones is firstly tested. The evolution of the
270 mean error for the 8 stations during the optimization procedure is illustrated on Fig. 5a for the
271 four events from April to June. Similar evolutions are also plotted on Fig. 5b for Pauillac station.

272 As shown in Fig 5a most of the gain is reached within the first 250 runs. The accuracy gain is
273 more evident with the evolution of the relative error at Pauillac station (Fig. 5b). RMSRE starts
274 around 0.18, then it is decreasing down to lower than 0.1 and it may even reach 0.06 (Fig. 5b).
275 At Pauillac for a mean tidal range of 1.6m, a decrease of 12% in relative error coincides with
276 an absolute gain of 0.19 m. The results with 7 zones (Fig 1b) are summarized in Table 1.

277 Relative error is within the range [0.14 - 0.18] before optimization and [0.09 - 0.12] after
278 optimization (Table 1, Fig. 5a). The global gain is thus within 3 and 8 % and the accuracy gain
279 is increasing with the flowrate. For the 6 hydrological configurations, the mean ratio between
280 final and initial error is 0.7. Along the different station, the mean ratio is almost equal to 1 at
281 Verdon, between 0.51 and 0.59 at Laména, Pauillac and Medoc and within 0.73-0.84 at
282 Ambes, Bordeaux, Cadillac and Libourne. At Verdon, no accuracy gain is observed. It might
283 suggest that improving the accuracy at Verdon through bottom friction coefficient leads to
284 deteriorate the accuracies of the other upstream stations. Improvement at the mouth may
285 probably require enhanced offshore boundary conditions which is a combination of tidal
286 atlases (Huybrechts et al 2012) and prediction of the storm surges. Less accuracy gain could
287 also be expected at the upper estuarine part due to a sparse bathymetry dataset. However,
288 for an application related to ship route and underkeel clearance management inside the
289 estuarine configuration (Orseau et al., 2020b), it is crucial to attain an efficient prediction of
290 water levels at the central part where navigable depths are more restricted.

291 **Variation of the bed friction distribution related to the flowrate**

292 The algorithm allows to reach a mean error relatively constant for the different hydrological
293 conditions. Nonetheless, it requires for each case an adaptation of the values for bed friction
294 coefficient. As suggested in Fig. 2, the flowrate variation might be responsible of the TM
295 migration of the fluid mud deposits, and it thus has an influence on the bottom roughness.
296 Friction coefficients are plotted as a function of the flowrate to find a relationship that could
297 be used to set an operational model. It is performed on Figs. 6 for the distribution with 7
298 friction zones. The zones are gathered as downstream part of the estuary for K1 and K2 (Fig.
299 6a), as Dordogne river for K3 and K4 (Fig. 6b) and as Garonne river for K5-K6 and K7 (Fig. 6c).

300 The evolution of the K1 coefficient (mouth, Fig. 6a) is in agreement with the evolution of M_2
301 amplitude in Verdon: slight linear increase according to the flowrate. Similar patterns are also
302 observed between evolution of K2 and M_2 amplitude at Pauillac.

303 For the Dordogne river (Fig. 6b), a parabolic distribution is obtained for K3 and a third
304 polynomial curve accurately describes the K4 evolution. For the Garonne river (Fig. 6c), K5 and
305 K6 describe a second order decreasing curve according to the flowrate. It means that the
306 friction increases due to the seaward migration of the TM which is in line with M_2 evolution
307 at Bordeaux. Similarly, for the lowest flowrates, the friction coefficient seems to reach a
308 maximum value as observed with M_2 amplitude. The most upstream coefficient K7 describes
309 an inverse behaviour with maximum value around $700 \text{ m}^3/\text{s}$. The plotted regression curves
310 show the general tendencies of the friction evolution. Nonetheless, extrema values for K5 and
311 K6 are not well captured by the simple second order equations. For the operational model, it
312 would be rather suggested to use piecewise linear equations between the 6 optimized values.

313 **Applicability of the methodology to finer mesh discretization and friction distribution**

314 The proposed methodology requires between 250-500 TELEMAC-2D runs to reach the
315 optimized friction distribution. For a 12 cores of 2.4 GHz RAM 48 Go workstation, 500 runs are
316 performed in approximately one-day wall-clock time. Computational efficiency can be gained
317 by avoiding some repetitive steps inside each individual run, by reducing the number of runs
318 or by increasing the computing resources. Nevertheless, alternative way can be suggested to
319 avoid a rough application of the methodology to a finer mesh.

320 The optimized distribution of bed friction obtained on a 28000 nodes is assessed on a finer
321 grid resolution (76000 nodes). The finer mesh is characterized by a better resolution along the
322 navigation channel and upstream the confluence. Table 2 summarises the averaged RMSRE at

323 each station along the navigation channel obtained with the 6 hydrological events after an
324 optimization of the coarser mesh. It reaches values ranging from 7.7% (Pauillac) to 13%
325 (Bordeaux) with a mean value of 9.8 %. Direct application of the optimized values to the finer
326 grid leads to RMSE within 6.9 to 11% with a mean value of 8.7%. It means that the optimized
327 values and associated abacuses are also valid on this finer mesh. As an alternative, the
328 optimized value obtained from the coarse mesh could be used as initial solution for a second
329 optimization with a finer mesh and a shorter number of runs.

330 To address the sensitivity to the number of friction zone, the optimization methodology is
331 applied to the same 6 hydrological events, but with 9 zones (Fig. 1c) on Mesh 1. As detailed in
332 Table 1, no significant differences can be noticed in term of accuracy. However, the values of
333 the friction distributions are different in the central part. To distinguish the friction zone
334 between the methodologies accounting for 7 or 9 zones, friction coefficients for the 9 zone
335 distributions are noted as KK1 to KK9. In fact, K2 extension covers the area sum of KK2, KK3
336 and KK4 whereas KK1 is the same zone as K1. The evolution of the bed friction coefficients in
337 the central part is shown in Fig. 7.

338 KK1 describes a linear relationship whereas KK2 and KK3 describe a parabolic relationship with
339 a maximum value around 800 - 900 m³/s. KK4 rather describes a parabolic relationship with a
340 minimum value. It should be noted that KK1 is smaller than K1 and KK2 higher than K2. It
341 results in a more abrupt transition occurring between the two zones which may affect the
342 numerical results if the model is coupled to a sediment transport and bed evolution module.

343 **Application of time-varying friction coefficients to a medium-term simulation (6 months).**

344 From Fig. 6, a relationship can be built between the friction coefficient and the flowrate for all
345 the 7 friction zones. Concerning the regression, piecewise linear relationships are selected to

346 interpolate the values for all flowrate values. Three simulations are conducted from April 1st
347 to the end of October 2015. The first two simulations are based on steady friction coefficients
348 extracted from the optimization step. The first one corresponds to friction coefficient
349 representative of low flowrate configuration (200 m³/s) and the second one rather
350 corresponds to a configuration representative of mean discharge configuration (800 m³/s).
351 The last and third simulation tests the piecewise linear relationships (PWL).

352 Time series of storm surges and flowrate are imposed at the boundary conditions. The time
353 step of flowrates is equal to 2 hours whereas it is equal to 10 min for the storm surge. Flowrate
354 ranges within 130 and 2700 m³/s during this period. At Verdon, Pauillac and Bordeaux, the
355 RMSRE are evaluated every two tidal cycles (25 hours) to provide an averaged estimation of
356 the accuracy. Values of RMSRE at Bordeaux and Pauillac stations are plotted in regards to
357 flowrate also averaged every 25 hours. At the Verdon station, the accuracy for each simulation
358 is equivalent (not showed here).

359 For the simulation 2 referred as “mean”, the values of friction coefficients are not suited for
360 low flowrates. The RMSRE can increase up to more than 20% (> 30 cm) at Pauillac. A similar
361 behaviour is observed at Bordeaux. In contrast, for the simulation 1 referred as “Low”, the
362 accuracy tends to decrease at Pauillac once values are higher than 500 m³/s, while, at
363 Bordeaux, the accuracy is more variable. However even if the prediction is correct at
364 Bordeaux, the accuracy is not sufficient in the central part. The advantage of the PWL
365 simulation is to maintain a constant accuracy for a wider range of flowrate since it combines
366 the advantage of the two previous simulations.

367 **CONCLUSIONS AND PERSPECTIVES**

368 The CMA-ES algorithm has been coupled to the hydrodynamic module TELEMAC-2D applied
369 to optimize the distribution of the bed friction coefficient inside the Gironde estuary. For the
370 tested configuration, 300 runs seemed to be sufficient to reach an optimal value. Additional
371 200 runs would help to gain an accuracy of few millimetres (or 0.3%). For simulations
372 performed on a 12 core workstation), 500 runs are completed in approximately one-day wall-
373 clock time for 12 tidal cycles. The application of the proposed methodology shows that it is
374 necessary to modify the bed friction coefficient in order to reach the same level of accuracy
375 for the different hydrological configurations. It also confirms a seasonal variation of the
376 friction coefficient and this particularly in the central part of the estuary. Different
377 relationships of the friction coefficient according to the flowrate have been incorporated
378 inside the operational model. These relationships effectively allow to maintain an accurate
379 prediction of the water levels for a wide range of hydrological configurations. However,
380 further investigations on more extreme events, such as flood, storm and long dry periods, are
381 still needed to provide more robust bed friction relationships.

382 For operational models, it would be interesting to further apply the methodology with several
383 flow configurations in order to build a surrogate model providing the friction distribution
384 according to hydro-meteorological forcing (flowrate, tidal range, storm surge) and to compare
385 such variation to data related to the bed texture or water column as bed sample or satellite
386 images of suspended matters.

387 **DATA AVAILABILITY**

388 Data, models, and code scripts used for coupling CMA-ES and TELEMAC-2D developed in this
389 study are available from the corresponding author upon request. Water levels data are
390 available at www.vigicrues.gouv.fr.

391 **ACKNOWLEDGMENTS**

392 The research leading to these results has received funding from the Connecting Europe Facility
393 (CEF) – Transport Sector under agreement (Innovation and Networks Executive Agency) No
394 INEA/CEF/TRAN/M2014/1049680 through the project Gironde XL. The authors thank the
395 National Hydrographic Service (SHOM) and the National Weather Agency (Météo-France) for
396 providing bathymetric datasets, and predictions of tide-surge interactions. Dr. Tom Benson is
397 kindly acknowledged for providing the Matlab toolbox used to post-process TELEMAC-2D
398 results.

399

400 **NOTATIONS**

401 g = gravity acceleration [m/s²] ;

402 h = water depth in [m] ;

403 K = Strickler coefficient for the bed friction in [m^{1/3}/s];

404 $RMSRE$ = Root Mean Square Relative Error [-]

405 \vec{U} = depth-averaged flow velocity vector, with east-west U , north-south V components [m/s].

406 Z = free surface elevation [m];

407 ν_t = momentum diffusion coefficient [m²/s];

408 ρ = density [m³/kg];

409

410 **APPENDIX: BRIEF DESCRIPTION OF THE CMA-ES ALGORITHM**

411 CMA-ES is a meta-heuristic optimization algorithm. It belongs to the class of algorithms called
412 "Evolution Strategies". The research step of these algorithms is carried out in a stochastic way
413 without any gradient calculation. The CMA-ES algorithm operates on a population of
414 individuals rather than on a single individual (as in the case of gradient algorithms).

415 Like all meta-heuristic algorithms, CMA-ES starts from an initial population randomly chosen.
416 To build a new generation of individuals, the CMA-ES algorithm follows on from the selection
417 step in which the new candidate solutions are sampled using a multivariate normal
418 distribution. Then individuals of this generation are evaluated via the objective function and
419 selected according to their fitness (or objective function value) to be part of the next
420 generation. Then comes the recombination stage to select a new mean value for the
421 distribution. The penultimate step of the CMA-ES algorithm is the mutation which consists in
422 adding a random vector acting as a perturbation with zero mean. The adaptation step
423 terminates the algorithm by updating the various parameters involved in the construction of
424 the covariance matrix. From this brief description of CMA-ES algorithm, we conclude that it is
425 the mutation and adaptation stages that make this algorithm a robust and powerful tool for
426 complex numerical optimization. In order to not burden the text and given their importance,
427 we will briefly describe these two stages.

428 **Mutation**

429
 430 The mutation is a step in the CMA-ES algorithm which allows generation of a new population
 431 with the aim of improving the one generated by the selection and recombination steps. It is
 432 certainly the most important step in the algorithm. It adds a random vector deduced from the
 433 multivariate distribution based on the previous generation (selection and recombination). The
 434 mutation guides CMA-ES to move in the search space by rotation and by scaling the adapted
 435 covariance matrix of the generated population. The evolution of this iterative process is
 436 controlled by different parameters (called strategy) which update automatically from
 437 information from previous generations. This process is called “evolution path”. It's this
 438 automatic parameter update that makes this algorithm the most powerful in its class. The user
 439 does not set any parameters for the correct execution of the algorithm.

440 As explained above, the ES algorithms are considered to be slow to converge towards the
 441 global optimum. To accelerate this convergence, the CMA-ES algorithm offers an intermediate
 442 recombination which averages a few vector individuals from the parent population. This
 443 combination is noted by $(\frac{\mu}{\mu_I}, \lambda)$ -CMA-ES where $(\frac{\mu}{\mu_I})$ designates the recombination of μ_I
 444 among μ parents and λ is the number of individuals in the initial population. Thus, for the
 445 algorithm $(\frac{\mu}{\mu_I}, \lambda)$ -CMA-ES the λ individuals of the generation $(g + 1)$ are calculated by:

$$446 \quad p_i^{(g+1)} = \langle p \rangle_{\mu}^{(g)} + \sigma^{(g)} N(0, C^{(g)}) , \quad i = 1, \dots, \lambda$$

447 Eq. 4
 448 With $p_i^{(g+1)}$ is the i th individual of the population of the generation $(g + 1)$, $\langle p \rangle_{\mu}^{(g)}$ is the
 449 mean value of $p^{(g)}$ at generation (g) computed by

$$450 \quad \langle p \rangle_{\mu}^{(g)} = \frac{1}{\mu} \sum_{k=1}^{\mu} p_k^{(g)}$$

451 $\sigma^{(g)}$ is the standard deviation at generation (g) (but for CMA-ES, it is also called step size),

452 $N(0, C^{(g)})$ note the normal distribution with center 0 and covariance $C^{(g)}$ at generation (g) .

453 It should be noted that the covariance matrix is a symmetric definite positive matrix, therefore

454 diagonalizable. In this case the covariance matrix $C^{(g)}$ can be written as:

$$455 \quad C^{(g)} = B^{(g)} D^{(g)} (B^{(g)} D^{(g)})^T$$

456 Eq. 5

457 Where the columns of the matrix $B^{(g)}$ are exactly the eigenvectors of $C^{(g)}$ and $D^{(g)}$ is a

458 diagonal matrix whose diagonal elements are the square root of the eigenvalues of $C^{(g)}$. The

459 combination of expressions (1) and (2) allows to rewrite (1) in the new form as:

460

$$461 \quad p_i^{(g+1)} = \langle p \rangle_\mu^{(g)} + \sigma^{(g)} B^{(g)} D^{(g)} z_i, \quad i = 1, \dots, \lambda$$

462 Eq. 6

463 With $z_i = (B^{(g)} D^{(g)})^T N(0, I)$, $i = 1, \dots, \lambda$

464

465 Finally, the calculation of the covariance matrix at generation $(g + 1)$ is based on the

466 calculation of the evolution of the path p_t at generation $(g + 1)$ according to the following

467 scheme:

$$468 \quad p_t^{(g+1)} = (1 - c) \cdot p_t^{(g)} + c_u \frac{\sqrt{\mu}}{\sigma^{(g)}} \left(\langle p \rangle_\mu^{(g+1)} - \langle p \rangle_\mu^{(g)} \right)$$

469 Eq. 7

$$470 \quad C^{(g+1)} = (1 - c_{cov}) \cdot C^{(g)} + c_{cov} p_t^{(g+1)} \cdot (p_t^{(g+1)})^T$$

471 Eq. 8

472 Where $\frac{1}{c}$ is the cumulative time of the evolution path. The parameter c can be interpreted a

473 weight allowing the smoothing of p_t and can be normalized by $c_u = \sqrt{c(2 - c)}$. $\frac{1}{c_{cov}}$ denotes

474 the average time for the covariance matrix. In the other word, c_{cov} allows the updating of the
475 covariance matrix and it can be considered as the learning rate.

476 **BIBLIOGRAPHY**

- 477 Allen, G.P., (1972). Etude des processus sédimentaires dans l'estuaire de la Gironde. PhD
478 Thesis, University of Bordeaux I, 310.
- 479 Baeck, T. Fogel D. B. and Michalewicz Z. (2000a). Evolutionary Computation 1 : Basic
480 Algorithms and Operators, Institute of Physics Publishing.
- 481 Baeck T., Fogel D. B. and Michalewicz Z. (2000b). Evolutionary Computation 2 : Advanced
482 Algorithms and Operators, Institute of Physics Publishing, 2000b
- 483 Bayer and Finkel, 2004: Evolutionary algorithms for the optimization of advective control of
484 contaminated aquifer zones. Water Resour. Res. 40, W06506, doi:10.1029/2003WR002675
- 485 Castaing, P., (1981). Le transfert à l'océan des suspensions estuariennes – Cas de la Gironde.
486 PhD Thesis, University of Bordeaux I, 530 p.
- 487 Ch, S.C. and Tsai, P.W. (2007). Computational intelligence based on the behavior of cats.
488 International Journal of Innovative computing, information and control. Vol. 3(1), pp.163-
489 173.
- 490 Dorigo, M. and Gambardella, L.M. (1997): Ant colony system: a cooperative learning approach
491 to the traveling salesman problem. IEEE Trans. on Evolutionary Computation 26(1), 53-
492 66.
- 493 Dréo, J., Pétrowski, A., Siarry, P., & Taillard, E. (2005). Metaheuristics for hard optimization.
494 Berlin Heidelberg, Germany: Springer-Verlag.
- 495 Dung, N. V., Merz, B., Bárdossy, A., Thang, T. D., and Apel, H. (2011) Multi-objective automatic
496 calibration of hydrodynamic models utilizing inundation maps and gauge data, Hydrol.
497 Earth Syst. Sci., 15, 1339-1354, <https://doi.org/10.5194/hess-15-1339-2011>
- 498 Eberhart, R. and Kennedy, J. (1995): A new optimizer using particle swarm theory. In: Sixth
499 International Symposium on Micro Machine and Human Science, pp. 39-43
- 500 Elshall, A.S., Pham, H. V., Tsai, F.T.-C., Yan, L., Ye, M., 2015. Parallel Inverse Modeling and
501 Uncertainty Quantification for Computationally Demanding Groundwater-Flow Models
502 Using Covariance Matrix Adaptation. J. Hydrol. Eng. 20, 04014087
- 503 Espana, M., Hernández-Díaz, A.M., Cecilia, J.M. and García-Román, M.D. (2017). Evolutionary
504 strategies as applied to shear strain effects in reinforced concrete beams:, Applied Soft
505 Computing, vol 57, pp:164-176
- 506 Fletcher, R. (1980), Practical methods of optimization: Volume 1 constrained optimization,
507 John Wiley & Sons, New York, USA, 126 p.
- 508 Fletcher, R. (1981), Practical methods of optimization: Volume 2 unconstrained optimization ,
509 John Wiley & Sons, New York, USA, 232 p.

510 Goldberg, D.E.: Genetic Algorithm in Search. Optimization and Machine Learning. Addison-
511 Wesley Publishing Company (1989)

512 Hansen, N., & Ostermeier, A. (1996). Adapting arbitrary normal mutation distributions in
513 evolution strategies: The covariance matrix adaptation. In Proceedings of the Third IEEE
514 International Conference on Evolutionary Computation, IEEE Press, Nagoya (Japan), pp.
515 312–317.

516 Hansen, N., & Ostermeier, A. (2001). Completely derandomized self-adaptation in evolution
517 strategies. *Evolutionary Computation*, 9(2), 159–195.

518 Hansen, N. (2016). "The CMA Evolution Strategy: A Tutorial".
519 <https://arxiv.org/abs/1604.00772>

520 Hansen, N. (2006). The CMA evolution strategy: a comparing review, in: *Towards a New*
521 *Evolutionary Computation*, Springer, 2006, pp. 75–102.

522 Hervouet, J.M., (2007). Hydrodynamic of free surface flows modelling with the finite element
523 method. Wiley ISBN 978-0-470-03558-0

524 Holland, J. H. (1975). *Adaptation in natural and artificial systems: An introductory analysis with*
525 *applications to biology, control, and artificial intelligence*. U Michigan Press.

526 Huybrechts, N., Villaret, C. and Lyard, F., (2012). Optimized predictive 2D hydrodynamic model
527 of the Gironde Estuary (France). *Journal of Waterway, Coast, Port and Ocean engineering*,
528 138 (4), 312-322.

529 Huybrechts, N., and Villaret, C., (2013). Large-scale morphodynamic modelling of the Gironde
530 Estuary, France. *Proceedings of the Institution of Civil Engineers in Maritime Engineering*,
531 166 (2), 51-62.

532 Jalón-Rojas, I., Schmidt, S. and Sottolichio, A., (2015). Turbidity in the fluvial Gironde Estuary
533 (southwest France) based on 10-year continuous monitoring: sensitivity to hydrological
534 conditions, *Hydrology and Earth System Sciences*, (19), 2805-2819.

535 Jalon-Rojas, I., Sottolichio, A., Hanquiez, V., Fort, A., & Schmidt, S. (2018). To what extent
536 multidecadal changes in morphology and fluvial discharge impact tide in a convergent
537 (turbid) tidal river. *Journal of Geophysical Research: Oceans*, 123. [https://doi.org/](https://doi.org/10.1002/2017JC013466)
538 [10.1002/2017JC013466](https://doi.org/10.1002/2017JC013466)

539 Kirkpatrick, S.D. Gelatt, C. and Vecchi, M.P. (1982): Optimization by simulated annealing. IBM
540 Research Report RC 9355, Acts of PTRC Summer Annual Meeting,.

541 Laborie, V., Hissel, F., and Sergent, P., (2014). Impact of climate change on Gironde estuary.
542 *La Houille Blanche*, 6, 34-39.

543 Lane, S. N. (1998). Hydraulic modelling in hydrology and geomorphology: a review of high
544 resolution approaches. *Hydrological Processes*, 12(8), 1131-1150.

545 Le Floch, J. (1961). Propagation de la marée dynamique dans l'estuaire de la Seine et la Seine-
546 Maritime. PhD thesis, Université de Paris. 507p.

547 Moldwin, M. (2016), Tidal river dynamics, *Eos*, 97, <https://doi.org/10.1029/2018EO049541>.

548 Moler C. and Little J. (2020). A history of MATLAB. *Proc. ACM Program. Lang.* 4, HOPL, Article
549 81 (June 2020), 67 pages. DOI:<https://doi.org/10.1145/3386331>

550 Orseau, S., Huybrechts, N., Tassi, P., Pham Van Bang, D. and Klein, F. (2020a) Two-dimensional
551 modeling of fine sediment transport with mixed sediment and consolidation: Application
552 to the Gironde Estuary, France. *International Journal of Sediment Research* (in press).

553 Orseau S., Huybrechts N., Tassi P., Kaidi S., Klein F (2020b). Nav-Tel: an open-source system
554 for ship routing and underkeel clearance management in estuarine channels. *J. of*
555 *Waterway Port Coastal Eng* (In revision).

556 Pairaud, I.L., Lyard, F., Auclair, F., Letellier, T., and Marsaleix, P., (2008). Dynamics of the semi-
557 diurnal and quarter-diurnal tides in the bay of Biscay. *Continental Shelf Research*, 28(10-
558 11), 1294-1315.

559 Pawlowicz R., Beardsley B., and Lentz S., (2002). Classical tidal harmonic analysis including
560 error estimates in MATLAB using T_TIDE. *Computers and Geosciences*, 28 (2002), 929-937.

561 Rudolph., G. (1994). Convergence analysis of canonical genetic algorithms. *IEEE Transactions*
562 *on Neural Networks*, 5:96–101, 1994

563 Smaoui, H., Maqsoud, A., Kaidi, S. (2019), Transmissivity Identification by Combination of
564 CVFEM and Genetic Algorithm: Application to the Coastal Aquifer. *Mathematical Problems*
565 *in Engineering*, 3463607, 14 pages.

566 Smaoui H., Zouhri L., Kaidi S. (2018) Combination of FEM and CMA-ES algorithm for
567 tranmissivity field identification in aquifer systems. *Hyrdological Processes Journal*.
568 32(2):264–277

569 Sottolichio, A., (1999). Modélisation de la dynamique des structures turbides (bouchon vaseux
570 et crème de vase) dans l'estuaire de la Gironde, PhD Thesis, University of Bordeaux I.

571 Sottolichio, A. and Castaing, P., (1999). A synthesis on seasonal dynamics of highly-
572 concentrated structures in the Gironde Estuary, *Comptes Rendus de l'Académie des*
573 *Sciences*, 329, 795-800.

574 Sottolichio, A., Le Hir, P., and Castaing, P., (2001). Modelling mechanisms for the turbidity
575 maximum stability in the Gironde Estuary, France. *Coastal and Estuarine Fine Sediment*
576 *Processes*, 373-386.

577 Schureman, P. (1958). *Manual of harmonic analysis and prediction of tides*, US Department of
578 *Commerce, Coast and Geodetic Survey, Washington, DC.*

579 Storn R. and Price K., (1997). Differential Evolution – A Simple and Efficient Heuristic for global
580 Optimization over Continuous Spaces. *Journal of global optimization*. Vol 1, pp. 341-359

581 van Rijn L.C. (2007) Unified view of sediment transport by currents and waves. I: Initiation of
582 motion, bed roughness, and bed-load transport, *J. Hydraulic Eng.* 133(6), pp. 649-667

583

584

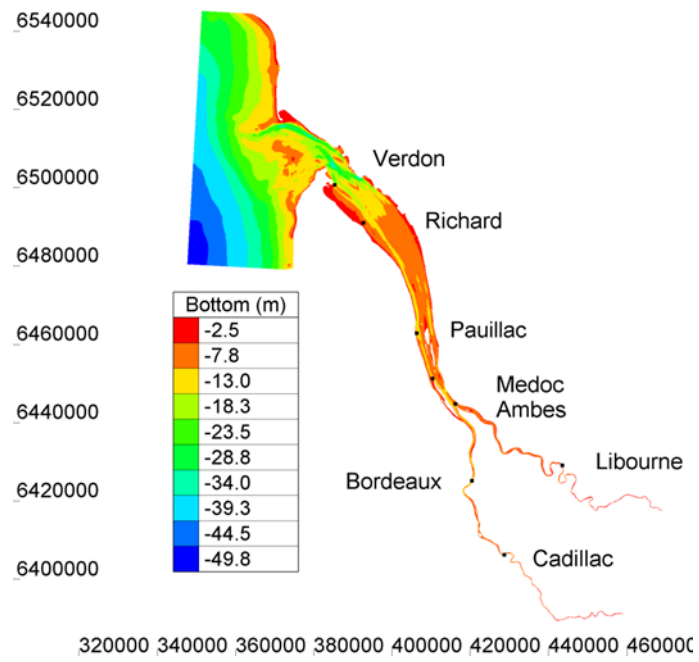
585

586

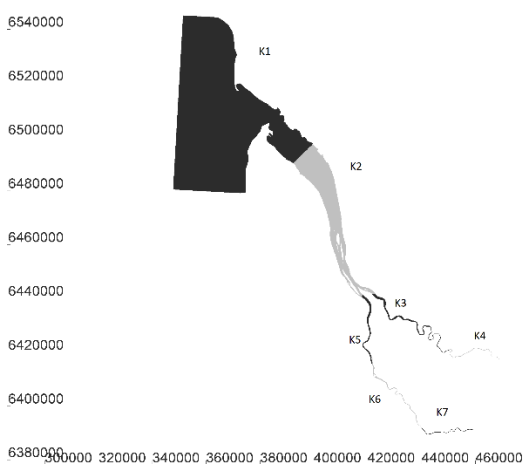
587

588

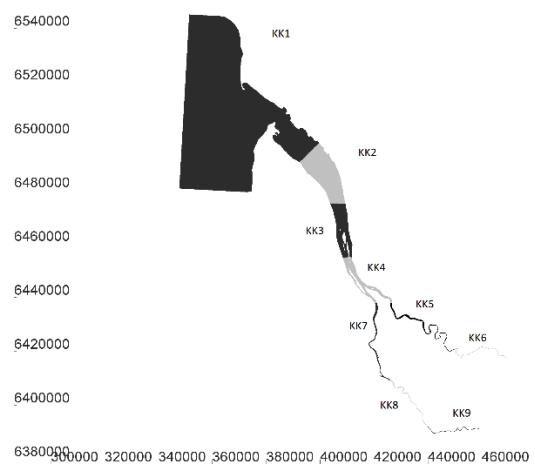
589



1a

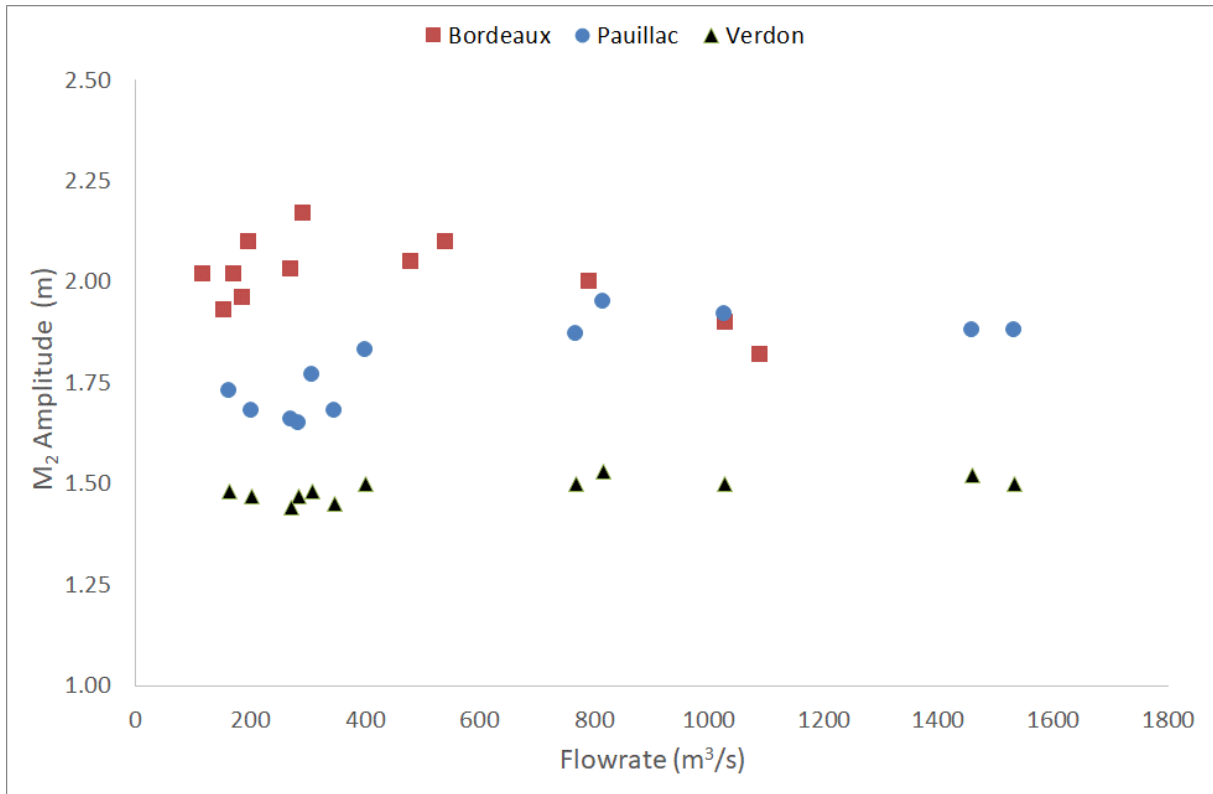


1b



1c

590 Figure 1 Model extension (1a) and bottom friction zones with 7 zones (1b) or 9 zones (1c)



591

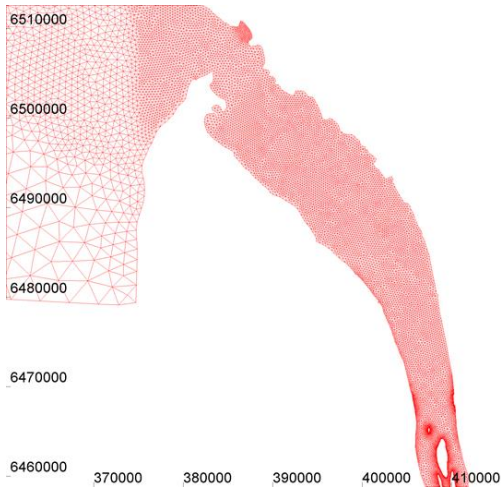
592 **Figure 2** Seasonal variation of M₂ amplitude with the total flowrate at Le Verdon, Pauillac station and with Garonne
 593 **flowrate at Bordeaux station (Fig. 1).**

594

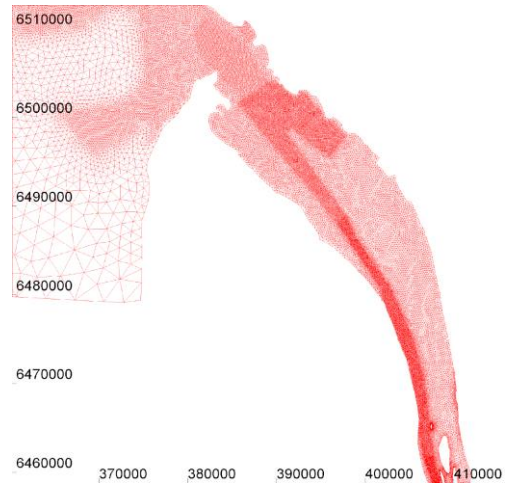
595

596

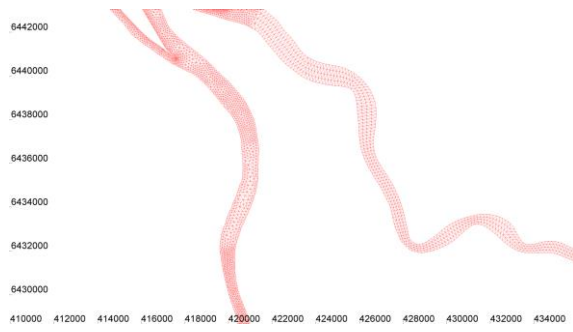
597



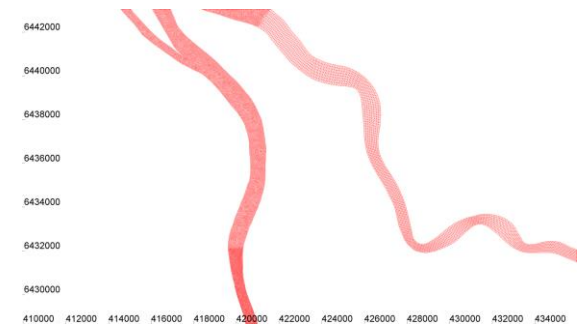
3a



3b



3c

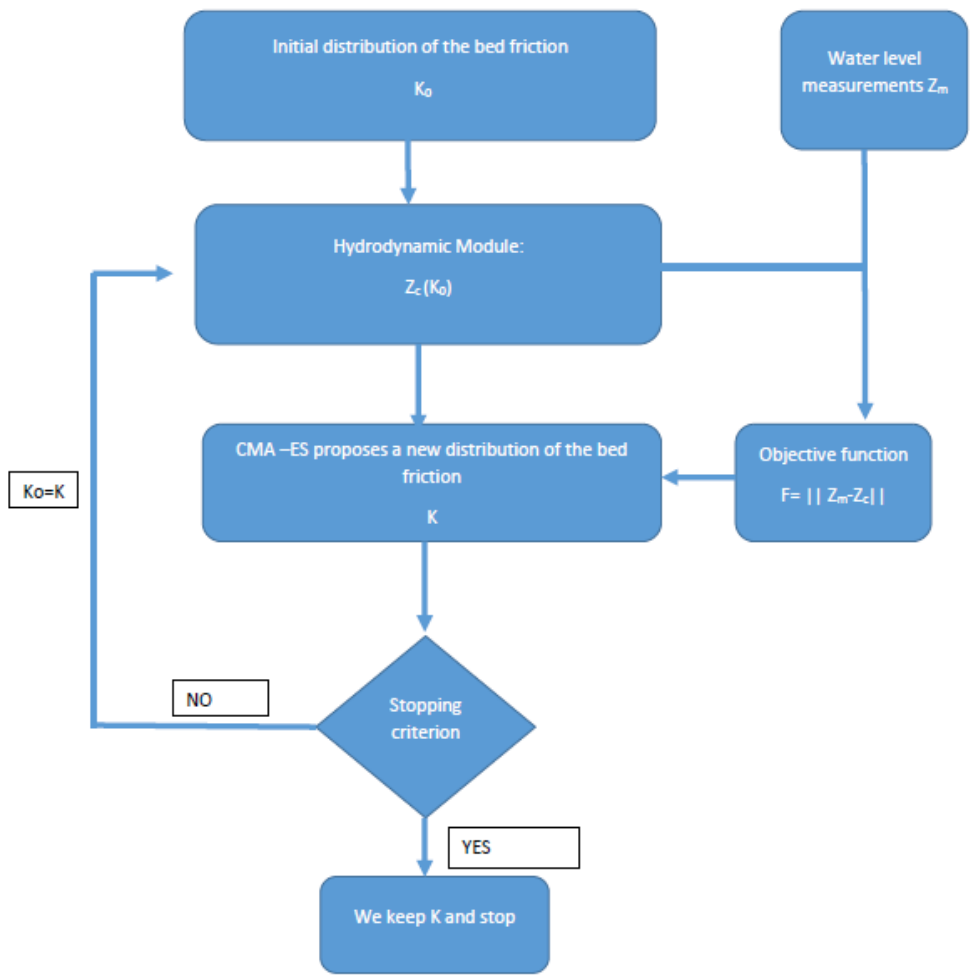


3d

598 Figure 3 Mesh distribution: (3a) mesh 1 with 28000 nodes in the downstream area, (3b) mesh
 599 2 with 78000 nodes in the downstream area, (3c) mesh 1upstream the junction, (3d) mesh 2
 600 upstream the junction.

601

602



603

604 **Figure 4 Flowchart of the coupling between the hydrodynamics module and the optimization algorithm**

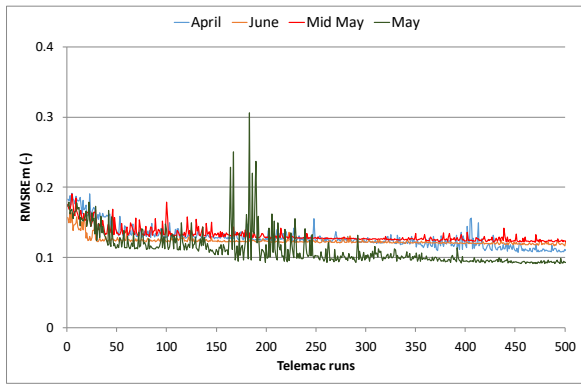
605

606

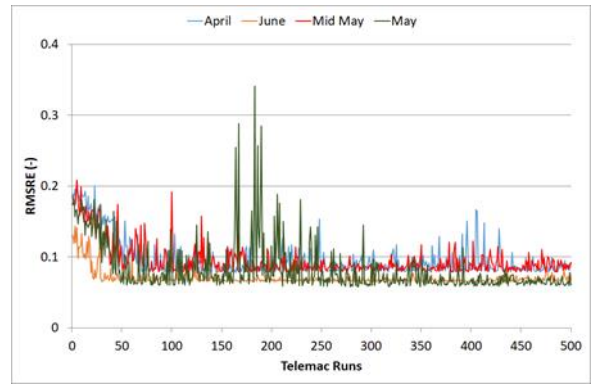
607

608

609



5a



5b

610 **Figure 5 Convergence of the algorithm. 5a mean RMSRE for the 8 stations. 5b RSMRE at Pauillac**

611

612

613

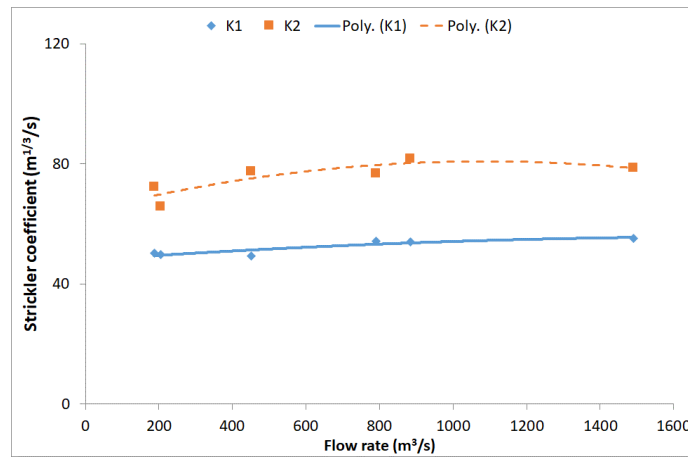
614

615

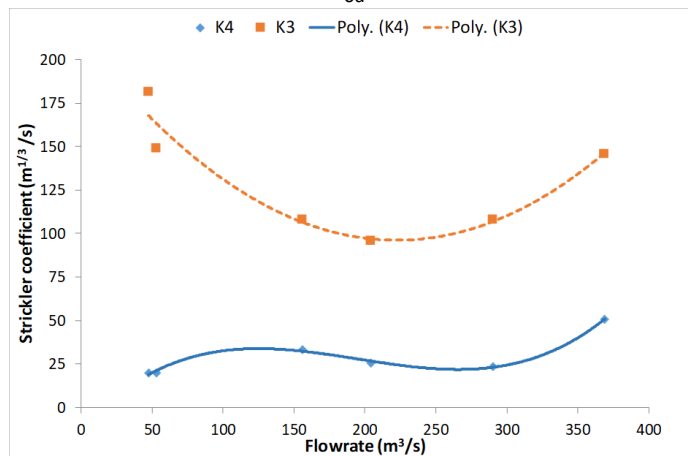
616

617

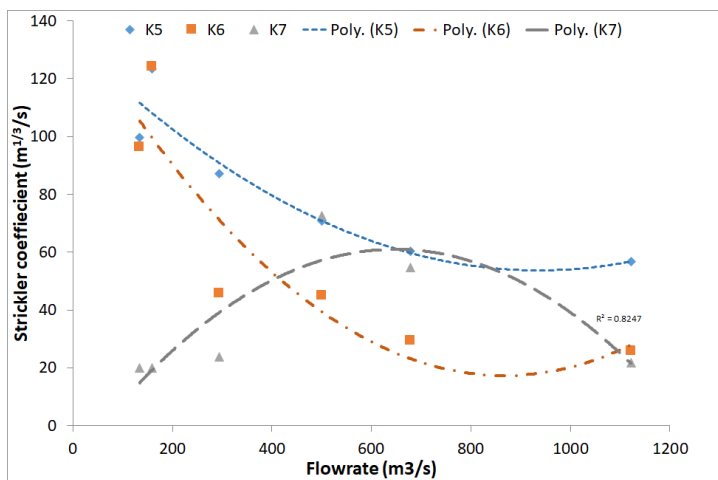
618



6a



6b



6c

619

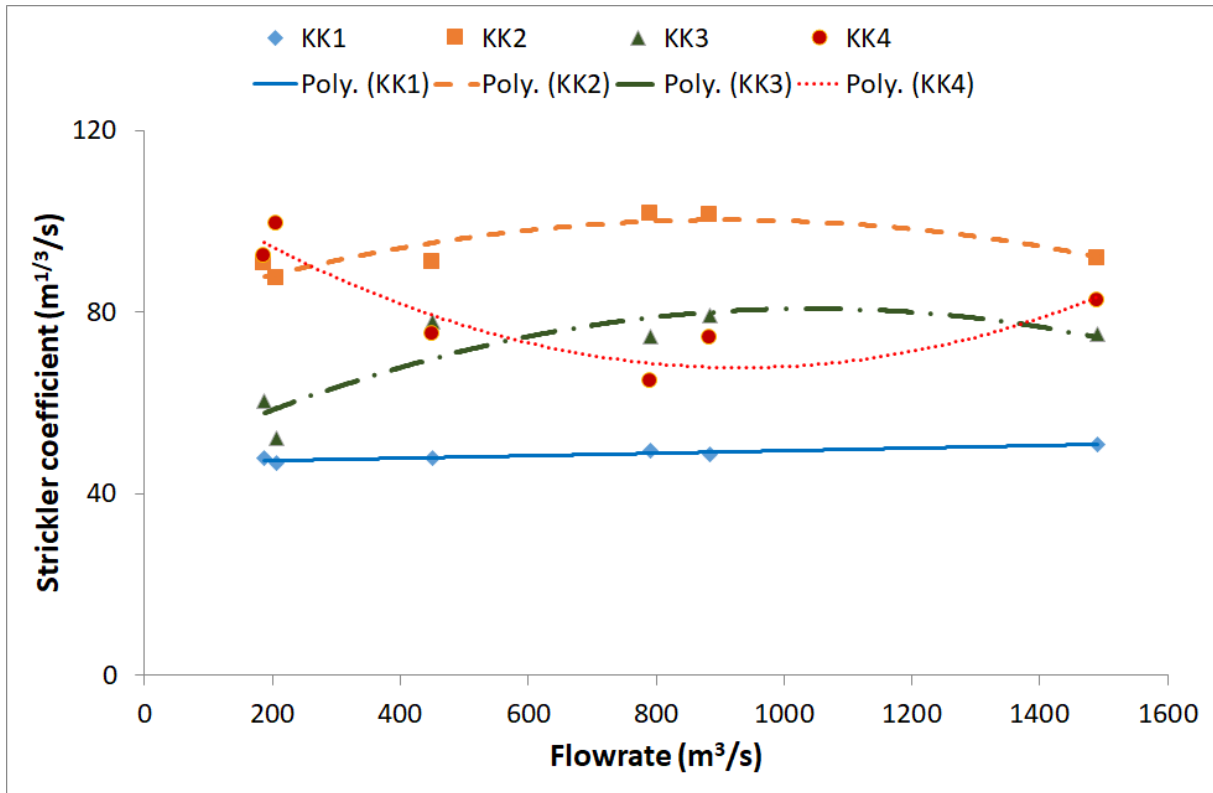
620 Figure 6 Evolution of the values for friction coefficient according to the total flowrate (Garonne and Dordogne). 6a in the
 621 central part with 7 zones distribution. 6b Distribution in the Garonne with 7 zones distribution. 6c in the Garonne for the
 622 7 zones distribution

623

624

625

626



627

628 Figure 7 Evolution of the values for friction coefficient according to the flowrate in the central part with the 9 zones
629 distribution, Strikler coefficients are noted as KK to distinguish them from the 7 zones distribution.

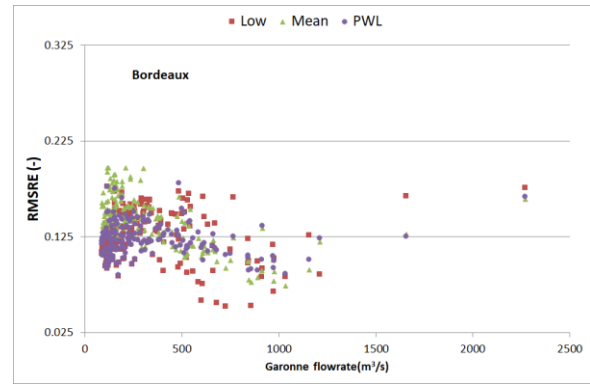
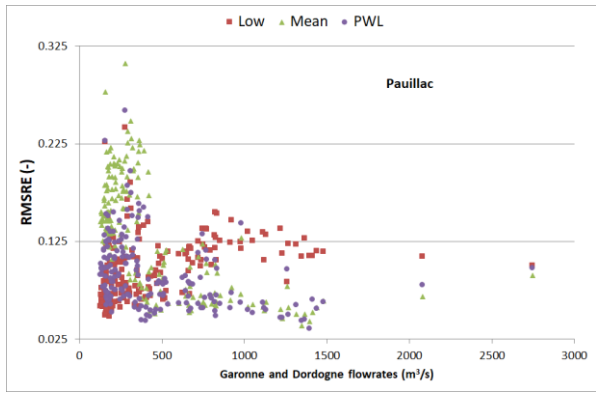
630

631

632

633

634



635

8a

8b

636 **Figure 8. Evolution of the daily RMSRE with the flowrate at Pauillac (8a) and Bordeaux (8b). Daily tidal range**
 637 **are using to estimate the relative accuracy. Flowrate is the sum of Garonne and Dordogne contribution at**
 638 **Pauillac and only Garonne contribution at Bordeaux.**

639

640

641

642

643

644

645

646

647

648

649

Table 1 RMSREm for the different configurations for different flowrate (Garonne and Dordogne contribution)

Total flowrate (m3/s)	RMSREm - 7 zones		RMSREm - 9 zones	
	Before optimization	After Optimization	Before optimization	After optimization
187	0.149	0.119	0.152	0.121
205	0.142	0.123	0.142	0.122
450	0.157	0.117	0.153	0.116
790	0.176	0.122	0.167	0.118
883	0.183	0.107	0.173	0.111
1490	0.173	0.091	0.163	0.089

650

651

652

653

Table 2 Reached RMSE for two different mesh sizes

Mesh	Mean RMSE	Verdon	Laména	Pauillac	Medoc	Ambes	Bordeaux
M1 - 28000 nodes	0.098	0.089	0.094	0.077	0.106	0.092	0.13
M2 - 76000 nodes	0.087	0.090	0.070	0.069	0.100	0.085	0.11

654

655