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► **To cite this version:**

Yuzhe Fan, Haisen Li, Daniel Fuster. Time-delayed interactions on acoustically driven bubbly screens. Journal of the Acoustical Society of America, 2021, 150 (6), pp.4219. 10.1121/10.0008905 . hal-03541971

HAL Id: hal-03541971

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Submitted on 25 Jan 2022

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Time-delayed interactions on acoustically driven bubbly screens

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(Dated: 13 August 2021)

1 We discuss the influence of compressibility effects including time delay on the dy-
2 namics of acoustically excited bubbly screens. In the linear regime, we show that the
3 proposed model recovers the results from the effective medium theory up to second
4 order for infinite bubbly screens when the wavelength is large compared to the inter-
5 bubble distance, and bubbles are equally spaced without the need of introducing any
6 fitting parameter. The effect of boundaries on finite size screens and randomization
7 on the bubble position is shown to lead to the appearance of multiple local resonances
8 and characteristic periodic structures. In the non-linear regime, we treat time-delay
9 effects as a delay-differential equation that is directly solved numerically. We show
10 the appearance the optimal distance for subharmonic emission for crystal structures
11 and discuss the accuracy of effective medium theories in the strong non-linear regime.

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12 I. INTRODUCTION

13 The dynamics of cavities in liquids has attracted a lot of interest over the past few decades
14 (Fuster, 2019; Lohse, 2018). The oscillation of an isolated bubble is well described by the
15 Rayleigh-Plesset (RP) like equations that account for compressibility effects (Gilmore, 1952;
16 Keller and Miksis, 1980; Lauterborn and Kurz, 2010; Prosperetti *et al.*, 1986). However,
17 bubbles often appear in ensembles, and bubble-bubble interactions need to be accounted
18 for as the bubble interface acceleration influences the pressure distribution in the bubble
19 surroundings. One traditional way to account for the influence of interactions is to use
20 the effective medium method. Foldy (1945), Caffisch *et al.* (1985), and Commander and
21 Prosperetti (1989) consider the influence that the dynamic bubble response have on the ef-
22 fective properties of a wave propagating in a bubbly liquid. The multiple interactions among
23 bubbles are described by the interaction between each bubble and the averaged pressure
24 field. However these models are limited to diluted systems and frequencies for which the
25 wavelength is larger than the characteristic bubble radius and the inter-bubble distance.

26

27 In an attempt to generalize the range of applicability of these theories to shorter wave-
28 lengths and capture more accurately the interaction mechanisms among bubbles, some
29 authors propose to solve a coupled system of RP like equations (Fan *et al.*, 2020b; Fuster
30 and Colonius, 2011; Ilinskii *et al.*, 2007; Mettin *et al.*, 1997). These approaches can be even-
31 tually coupled with an Eulerian-Lagrangian approach (Fuster and Colonius, 2011; Maeda
32 and Colonius, 2019) to capture both, short and long wave range interactions and can be

33 considered as two-way coupled model, where bubbles can directly feel the acoustic field
34 emitted by each other. An intrinsic difficulty in these models is how to account for the
35 influence of the liquid compressibility on the multiple interactions among bubbles. Indeed
36 one of the most frequently-used assumption is to resort to the incompressible limit where the
37 interactions among bubbles takes place instantaneously neglecting any time-delay effect due
38 to liquid compressibility. Although this assumption is certainly valid when the wavelength
39 of the excitation pressure wave is much larger than the characteristic size of the bubble
40 cluster, the accuracy and degree of applicability of these models in systems with many
41 bubbles has not been discussed in detail.

42

43 Some numerical studies applied to medical related research such as high-intensity fo-
44 cused ultrasound (Okita *et al.*, 2013), ultrasound contrast agent (Faez *et al.*, 2012), and
45 drug delivery (Coussios and Roy, 2008) point out the importance of compressibility effects,
46 an in particular time-delay effects in real applications (Sujarittam and Choi, 2020). More
47 fundamental studies including experimental works studying the acoustic propagation in the
48 vicinity of a bubble chain (Manasseh *et al.*, 2004) have shown that the time-delay effects
49 considerably change the resonance frequencies and the damping factors of the effective
50 medium (Doinikov *et al.*, 2005; Ooi *et al.*, 2008), so does bubble near boundaries (Dahl and
51 Kapodistrias, 2003; van't Wout and Feuillade, 2021; Ye and Feuillade, 1997). In the context
52 of the development of acoustic metamaterials, two-dimensional bubble layers also known
53 as bubbly screens have also become a widely investigated system since 2009 in a series of
54 papers published by Leroy and coworkers (Leroy *et al.*, 2015, 2009; Lombard *et al.*, 2015).

55 Using the self-consistent approach based on the effective medium theory, the transmission
56 and reflection coefficient measured experimentally in the linear regime can be well captured
57 by accounting for the influence of time-delay effects on the interaction term among bubbles.
58 In non-linear regime, the asymptotic analysis based on effective medium theory ([Miksis](#)
59 [and Ting, 1989](#); [Pham *et al.*, 2021](#)) have shed light into the role of compressibility on the
60 mechanisms of multiple interactions among bubbles. However, these models still face some
61 challenges. For example it is known that, even in the dilute limit, crystal configuration
62 have special acoustic properties ([Devaud *et al.*, 2010](#)). The capability of these models to
63 distinguish between the properties of specific configurations (e.g. crystals) and the ensemble
64 average of randomly distributed systems has not been clarified . Also, it is not clear how
65 well averaged models capture the influence of boundary effects as well as polydispersity
66 effects.

67

68 In this work we discuss the applicability and accuracy of models based on the resolution of
69 a coupled system of RP like equations to capture the response of bubbly screens (Figure 1).
70 After presenting a particularization of the system of Rayleigh-Plesset like equations proposed
71 in [Fuster and Colonius \(2011\)](#) to solve for the dynamic response of the bubbles, we show that
72 this model is able to recover the second order solution predicted by the effective medium
73 theory in the linear oscillating regime without the need of introducing any fitting parameter.
74 Then the influence of boundary effects and randomness on the accuracy of the predictions
75 from the effective medium theory are discussed in the linear regime. In the non-linear
76 regime, we present numerical results of the solution of the system of equations using a delay-

77 differential equation solver showing examples that reveal the importance of compressibility
78 effects to correctly predict the bubble dynamic response.

79 II. BUBBLY SCREEN MODEL

80 The dynamics of an oscillating spherical bubble is described using the Keller-Miksis like
81 equation (Keller and Miksis, 1980) which is a differential equation for the bubble radius of
82 the i th bubble in a weakly compressible liquid characterized by its speed of sound c and
83 density ρ

$$\rho \left(R_i \ddot{R}_i \left(1 - \frac{\dot{R}_i}{c} \right) + \frac{3\dot{R}_i^2}{2} \left(1 - \frac{\dot{R}_i}{3c} \right) \right) - \left(1 + \frac{\dot{R}_i}{c} + \frac{R_i}{c} \frac{d}{dt} \right) (p_{i,B} - p_\infty) = \rho I_i(t_d). \quad (1)$$

84 In the equation above, $p_\infty(t) = p_0 + f(t)$ is the pressure excitation, $p_{i,B}$ is the liquid pres-
85 sure at the interface of the i th bubble, which we describe using a simple polytropic law
86 $p_{i,B} = \left(p_0 + \frac{2\sigma}{R_{i,0}} \right) \left(\frac{R_{i,0}}{R_i} \right)^{3\kappa} - \frac{2\sigma}{R_i} - \frac{4\mu\dot{R}_i}{R_i}$, where p_0 is the static pressure; $R_{i,0}$ is the i th bubble
87 radius at equilibrium; σ is the surface tension; μ is the liquid viscosity.

88

89 The interaction term $I(t_d)$ represents the pressure fluctuation induced by the presence
90 of the surrounding bubbles, which has to be evaluated at the deferred time $t_d = t - d_{ij}/c$,
91 where $d_{ij} = |\vec{x}_i - \vec{x}_j|$ represents the distance from the i th bubble located at \vec{x}_i to the j th
92 bubble located at \vec{x}_j . Following Fuster and Colonius (2011), it can be readily shown that

$$I_i = I_{i,0} + I_{i,1}, \quad (2)$$

93 where both terms have to be evaluated at the deferred time t_d

$$\begin{aligned}
I_{i,0}(t_d) &= - \sum_{j \neq i}^N \frac{R_j}{D_{ij}} \left(R_j \ddot{R}_j + 2\dot{R}_j^2 \right), \\
I_{i,1}(t_d) &= -\frac{1}{c} \left[\sum_{j \neq i}^N \frac{R_j}{D_{ij}} \dot{R}_j \left[R_j \ddot{R}_j + \frac{\dot{R}_j^2}{2} - \frac{(p_{j,B} - p_\infty)}{\rho} \right] - \sum_{j \neq i}^N \frac{R_j^2}{D_{ij}} \frac{d}{dt} \frac{(p_{j,B} - p_\infty)}{\rho} + \dot{R}_i I_{i,0} \right] \quad (3)
\end{aligned}$$

94 In the equations above, we only keep first order compressibility correction terms in the
95 intensity of the collapse of bubbles, which scale as a function of the Mach number $Ma = \frac{\dot{R}}{c}$,
96 and time-delay effects. Neglecting time-delay effects (e.g. $t_d = t$) leads to a coupled system
97 of equations that needs to be solved. In the limit of $c \rightarrow \infty$ we recover the classical form of
98 the interaction term $I_i \approx I_{i,0}$ evaluated at t (Bremond *et al.*, 2006; Ida *et al.*, 2007; Yasui
99 *et al.*, 2008). Otherwise, as explained in Section IV, it is required to solve a differential
100 equation with time delay.

101 III. COMPRESSIBILITY EFFECTS IN THE LINEAR OSCILLATION REGIME

102 A. General case

103 In this section, we start considering the dynamics of a finite bubbly screen with monodis-
104 perse bubbles excited by a weak perturbation, where $R_{i,0} = R_{j,0} = R_0$. Bubbles are arranged
105 in N_l layers in the $x = 0$ plane ($N_l = 3$ in Figure 1). For a system with N bubbles of the
106 same equilibrium radius, the coupled set of equations that needs to be solved is

$$R_i \ddot{R}_i - \left(1 + \frac{R_i}{c} \frac{d}{dt} \right) \frac{p_{i,B} - p_\infty}{\rho} = - \sum_{j \neq i}^N \frac{R_j^2(t_d)}{d_{ij}} \ddot{R}_j(t_d) + \sum_{j \neq i}^N \frac{R_j(t_d)}{d_{ij}} \frac{R_j(t_d)}{c} \frac{d}{dt} \frac{(p_{j,B}(t_d) - p_\infty(t_d))}{\rho}, \quad (4)$$

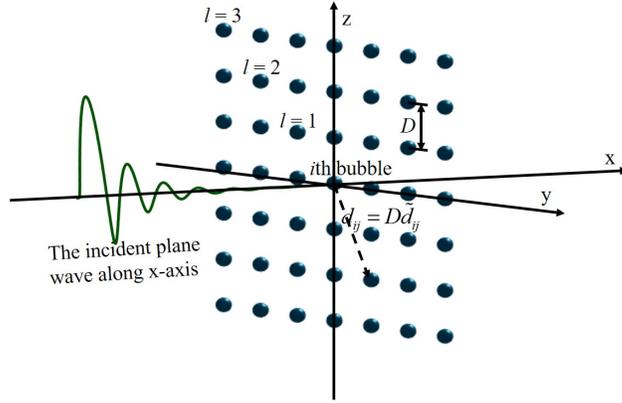


FIG. 1. A typical crystal distributed bubbly screen located at $x = 0$ plane.

107 where $R_i(t) = R_0(1 + r'_i e^{i\omega t})$, $R_i(t_d) = R_0(1 + r'_i e^{i\omega(t - d_{ij}/c)})$. For simplicity, we consider a pla-
 108 nar wave such that $p_\infty = p_0(1 + p' e^{i\omega t})$, neglect viscous, thermal, and surface tension terms
 109 during linear analysis, and thus have $p_{i,B} - p_0 = -3\gamma p_0 r'_i e^{i\omega t}$. For a given physical system
 110 at constant reference pressure, the dimensionless wavenumber $kR_0 = \frac{\omega}{\omega_0} \frac{1}{c} \sqrt{\frac{3\kappa p_0}{\rho}}$ depends
 111 on the frequency ratio between the excitation frequency, ω , and the resonance frequency
 112 of single isolated oscillating bubble $\omega_0 = \sqrt{\frac{3\gamma p_0}{R_0^2 \rho}}$. For air bubbles in water at atmospheric
 113 conditions $\frac{1}{c} \sqrt{\frac{3\kappa p_0}{\rho}} \approx 10^{-2}$ and therefore $kR_0 < 1$ is usually a reasonable assumption. This
 114 parameter will be held constant in what follows, where we show the solution for particu-
 115 lar configurations of the bubbly screen. We can also define an alternative dimensionless
 116 wavenumber using the averaged inter-bubble distance D as $kD = \frac{D}{R_0} \frac{\omega}{\omega_0} \frac{1}{c} \sqrt{\frac{3\kappa p_0}{\rho}}$, which is not
 117 always small in diluted systems.

118

A first remark is that, in the linear regime, the influence of the compressibility correction term in the interaction is not null, and it is not sufficient to retain the incompressible

interaction term only. Neglecting terms of order $(kR_0)^2$, the set of equations above can be written in matrix form as

$$(\mathbf{A}^{(0)} + ikR_0\mathbf{A}^{(1)})\vec{r}' = \vec{B}p',$$

119 where the coefficients of the matrices $\mathbf{A}^{(0)}$ and $\mathbf{A}^{(1)}$ and vector \vec{B} are defined introducing
 120 the local variable $\mathfrak{K}_i = \frac{R_0}{D} \sum_{j \neq i}^N \frac{e^{-ikD\tilde{d}_{ij}}}{\tilde{d}_{ij}}$, the wavenumber $k = \omega/c$ and the nondimensional
 121 distance $\tilde{d}_{ij} = |\vec{x}_i - \vec{x}_j|/D$ (see appendix A for the full expressions).

122

If we only consider the solution of a planar incident wave, this linear set of equations can be numerically solved for an arbitrary constant value of the RHS to find all r'_i . Once these values are obtained, we can define the complex quantity

$$Q_i^* = \frac{\sum_{j \neq i}^N (r'_i - r'_j) \frac{e^{-ikD\tilde{d}_{ij}}}{\tilde{d}_{ij}}}{r'_i \sum_{j \neq i}^N \frac{e^{-ikD\tilde{d}_{ij}}}{\tilde{d}_{ij}}}$$

123 to express the solution of the system as

$$F_i(\omega/\omega_0)r'_i = -\frac{p_0}{\rho R_0^2 \omega_0^2} p', \quad (5)$$

124 where

$$F_i(\omega/\omega_0) = 1 - \left(\frac{\omega}{\omega_0}\right)^2 - \left(\frac{\omega}{\omega_0}\right)^2 K_i^* \quad (6)$$

125 is defined for each bubble depending on the complex function

$$K_i^* = \mathfrak{K}_i(1 - Q_i^*) - ikR_0 \left[(1 + \mathfrak{K}_i)^2 - \mathfrak{K}_i Q_i^* \left(1 + \mathfrak{K}_i + \frac{\omega_0^2}{\omega^2} \right) \right]. \quad (7)$$

126 The real and imaginary parts of K_i^* are typically used to define the resonance frequency
 127 $\omega_{i,res}$ and the damping coefficient ζ_i for the i th bubble as

$$\omega_{i,res}^2 = \frac{\omega_0^2}{1 + \Re(K_i^*)}; \quad \zeta_i = -\Im(K_i^*). \quad (8)$$

128 It is easy to verify that, when $\mathfrak{R}_i \rightarrow 0$, we recover the limit of an isolated bubble where
 129 $\omega_{i,res} = \omega_0$ and $\zeta_i = \zeta_0 = kR_0$ representing the acoustical damping of a single bubble due to
 130 compressibility effects.

131

For systems where F_i is not uniform for all the bubbles, multiple local resonances (corresponding to zeros of the real part of F_i function) appear. Writing an equation for the bubble volume evolution, $V_i = V_0(1 + V'_i e^{i\omega t})$ with V_0 the bubble volume at equilibrium, we can define a global resonance and a global damping factor using the averaged change of gas volume per bubble

$$\frac{V_0}{N} \sum_{i=1}^N V'_i = \frac{4\pi R_0^3}{N} \sum_{i=1}^N r'_i = -\frac{4\pi R_0 p_0}{\rho_l \omega_0^2} \left\langle \frac{1}{F_i} \right\rangle p'$$

132 which can be also written as

$$\frac{1}{\left\langle \frac{1}{F_i} \right\rangle} \frac{1}{N} \sum_{i=1}^N r'_i = -\frac{p_0}{\rho_l R_0^2 \omega_0^2} p', \quad (9)$$

where $\left\langle \frac{1}{F_i} \right\rangle = \frac{1}{N} \sum_{i=1}^N \frac{1}{F_i(\omega/\omega_0)}$ denotes the average over all the bubbles in the screen. By introducing an averaged coefficient K^* defined from

$$\frac{1}{\left\langle \frac{1}{F_i} \right\rangle} = 1 - \left(\frac{\omega}{\omega_0} \right)^2 - \left(\frac{\omega}{\omega_0} \right)^2 K^*,$$

133 the global resonance and the global damping factor based on the definitions in Eq. 8 are
 134 given as:

$$\omega_{res}^2 = \frac{\omega_0^2}{1 + \Re(K^*)}; \quad \zeta = -\Im(K^*). \quad (10)$$

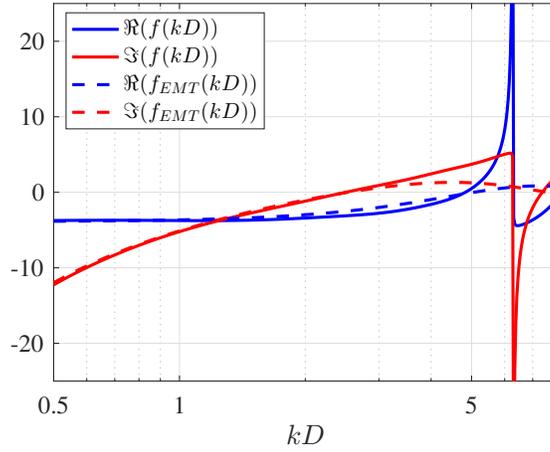


FIG. 2. Real and imaginary part of the function $f(kD)$. For reference we include the predictions of the effective medium theory. The solid line is corresponding to the $f(kD)$ and the dashed line is corresponding to EMT. The blue line is the real part, and the red line is the imaginary part. $N_l = 12000$ is used to keep $f(kD)$ converge.

135 B. Synchronous solution for an infinite bubbly screen with crystal configuration

136 We start considering the synchronous solution with equal amplitude for all bubbles ($Q_i^* =$
 137 0 for all bubbles). In this limit the solution of the system is given by the simplified expression
 138 of $F_i \rightarrow F$

$$F(\omega/\omega_0) = 1 - \left(\frac{\omega}{\omega_0}\right)^2 - \left(\frac{\omega}{\omega_0}\right)^2 (\mathfrak{K} - ikR_0(1 + \mathfrak{K})^2), \quad (11)$$

139 where $\mathfrak{K}_i \rightarrow \mathfrak{K} = \frac{R_0}{D} f(kD)$ is a function that is proportional to the bubble inter-spacing
 140 parameter R_0/D and the function

$$f(kD) = \sum_{j \neq i}^{\infty} \frac{e^{-ikD\tilde{d}_{ij}}}{\tilde{d}_{ij}}, \quad (12)$$

141 which depends on the dimensionless wavenumber kD and the particular geometry considered
 142 only. In the particular case of the crystal structure represented in Figure 1, $f(kD)$ becomes

$$f(kD) = \sum_{l=1}^{\infty} \frac{4}{l} e^{-\imath kDl} \left(1 + \sum_{q=1}^l \frac{2}{\sqrt{1 + (q/l)^2}} e^{\imath kDl(1 - \sqrt{1 + (q/l)^2})} \right), \quad (13)$$

143 which needs to be evaluated numerically except in very particular cases. For instance for
 144 $kD = 2\pi n$, with n being an integer, the first term is a diverging harmonic series implying zero
 145 resonance frequency and infinite attenuation. We identify this phenomenon with a resonance
 146 phenomenon in the cavities within the bubbles. The convergence properties of this series
 147 in a general case are discussed in Appendix B. It is interesting to note that the results
 148 obtained are in agreement with the expression proposed by Leroy *et al.* (2009) in the small
 149 kD limitation neglecting the correction of order $(kR_0 \cdot \mathfrak{K})$ without the need of introducing
 150 any fitting parameter. Using an homogenization approach and introducing a cutoff length
 151 $b = D/\sqrt{\pi}$, Leroy *et al.* (2009) obtain \mathfrak{K} using the bubble density $n_d = 1/D^2$ (number of
 152 bubbles per unit area in the screen) as

$$\mathfrak{K}_{\text{EMT}} = \frac{R_0}{D} f_{\text{EMT}}(kD) \approx \int_b^{\infty} \frac{R_0}{r} e^{-\imath kr} 2\pi r n_d dr = -\frac{R_0}{D} f_{\text{EMT}}(kD), \quad (14)$$

$$f_{\text{EMT}}(kD) = \frac{2\pi}{kD} (\sin(kb) + \imath \cos(kb)). \quad (15)$$

153 As shown by Pham *et al.* (2021), this expression is similar to the extension of the asymptotic
 154 analyses proposed by Cafisch *et al.* (1985) and later extended by Miksis and Ting (1989)
 155 to the second order, where the correction due to the collective effects of the bubbly screen
 156 is (Pham *et al.*, 2021)

$$f_{\text{EMT}}(kD) = -3.9 - \imath \frac{2\pi}{kD}. \quad (16)$$

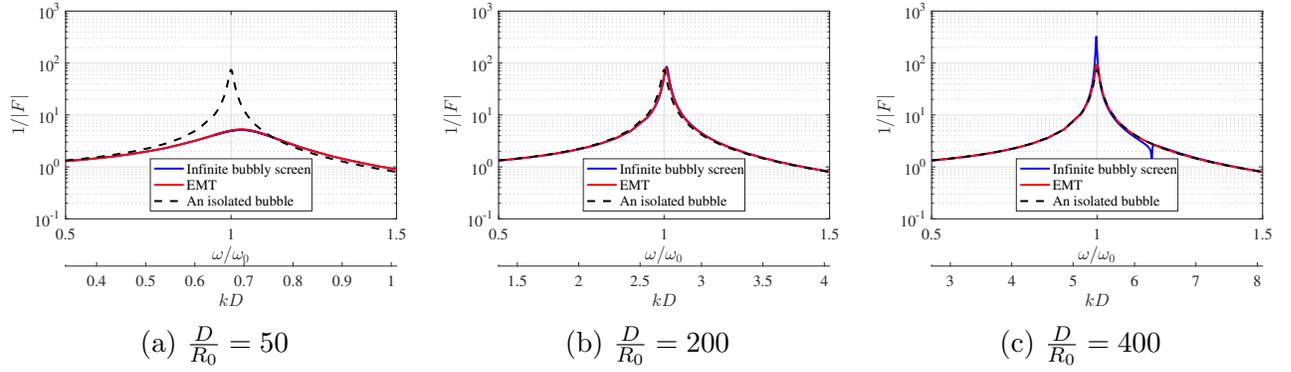


FIG. 3. $1/|F|$ v.s. ω/ω_0 for three different concentrations. The series are evaluated using $N_l = 12000$ layers.

157 Using the small angle approximation, it is straightforward to see that eqs. 16 and 15 are
 158 equivalent and, as shown in Figure 2, reproduce well the values of the series for $kD \lesssim 3$. In
 159 what follows we denote the predictions of this model as effective medium theory (EMT).

160

161 Figure 3 represents $1/|F|$ as a function of the frequency for three different concentrations.
 162 For high concentrations ($D/R_0 = 50$) the resonance peak is damped, this effect being well
 163 captured by the EMT. As the bubble concentration is decreased, the curve tends to recover
 164 the result of an isolated bubble. Remarkably, the intensity of the peak at resonance becomes
 165 much more important than the one predicted by the EMT for $kD \approx 2\pi$. To gain further
 166 insight, Figure 4 shows the influence of D/R_0 at constant forcing frequency on the global res-
 167 onance and the global damping factor. By changing the inter-bubble distance, the proposed
 168 model recovers well the predictions of the effective medium approximation for $kD \lesssim 3$, while
 169 for large values of kD both models give different predictions. This discrepancy is attributed
 170 to the difference between crystal structure and the random bubble distribution as discussed

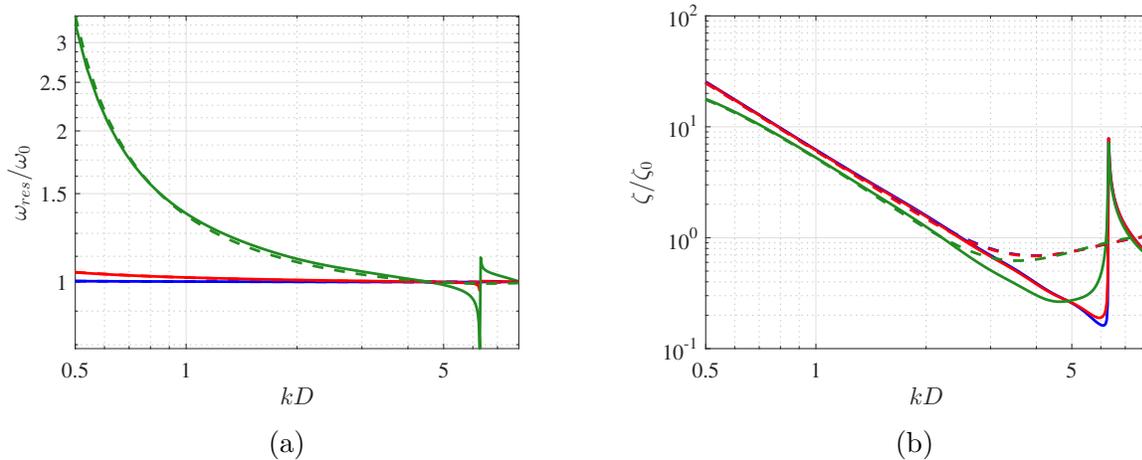


FIG. 4. (Left) Concentration effects on ω_{res}/ω_0 and (right) on ζ/ζ_0 . Solid lines are used for the approximated exact solution ($N_l = 12000$). Dashed lines represent the solution provided by the effective medium theory. The frequencies used are $\omega/\omega_0 = 0.0785, 0.785, 7.85$ for blue, red and green line respectively.

171 later on for a finite bubbly screen. In the effective medium approximation, bubbles are
 172 continuously and homogeneously distributed in the space, and the oscillating term $e^{-ikD\vec{d}_{ij}}$
 173 is thus smoothed out. The current model is able to capture the resonance effects originated
 174 for particular configurations. In the particular example shown here, it is expected to find a
 175 first resonance for $kD = 2\pi$, corresponding to the appearance of the resonance within the
 176 distance between bubbles.

177

178 C. Finite size bubbly screens

179 In many applications, the size of the bubbly screens is limited to few tens or hundreds
 180 of bubbles, and the infinite screen limit may not be applicable. In addition, these systems

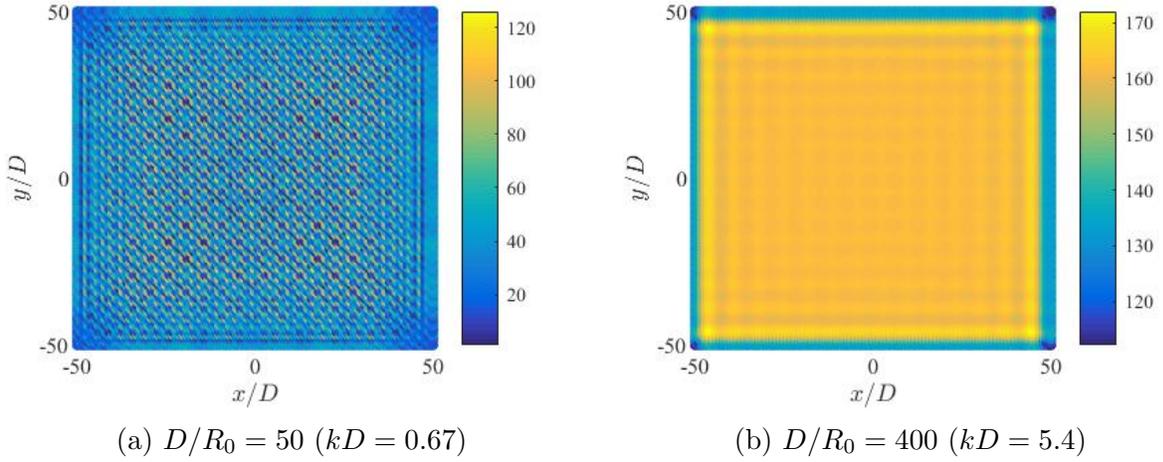


FIG. 5. Distribution of $1/|F_i|$ for $\omega/\omega_0 = 1$ in a 101×101 bubbly screen.

181 present the appearance of multiple resonance frequencies as a consequence of the boundary
 182 effects on the dynamics of the bubbles. Figure 5 shows an example of the distribution of
 183 function $1/|F_i|$ for a 101×101 bubbly screen excited at the single bubble resonance frequency
 184 for two different values of the dimensionless wavenumber: $kD < 1$ and near $kD \approx 2\pi$. This
 185 function, which is directly proportional to the intensity of the bubble oscillation, presents
 186 characteristic spatial patterns that are especially visible in the diluted limit when $kD \approx 2\pi$
 187 ($D/R_0 = 400$ in this case).

188 The influence of spatial structures is discussed using variable Q_i^* , which integrates the
 189 influence of interactions on the dynamics of a given bubble due to phase lag and amplitude
 190 changes among the other bubbles, and tends to zero in the limit of an infinite bubbly screen
 191 for crystal configurations. Figure 6 shows that the intensity of the mean value of $|Q_i^*|$
 192 becomes maximum at resonance, tends to a plateau at larger frequencies and quickly decays
 193 for low frequencies. Characteristic patterns are easily identified at resonance conditions but
 194 also become visible for other values of the forcing frequency. Notice that it also is possible

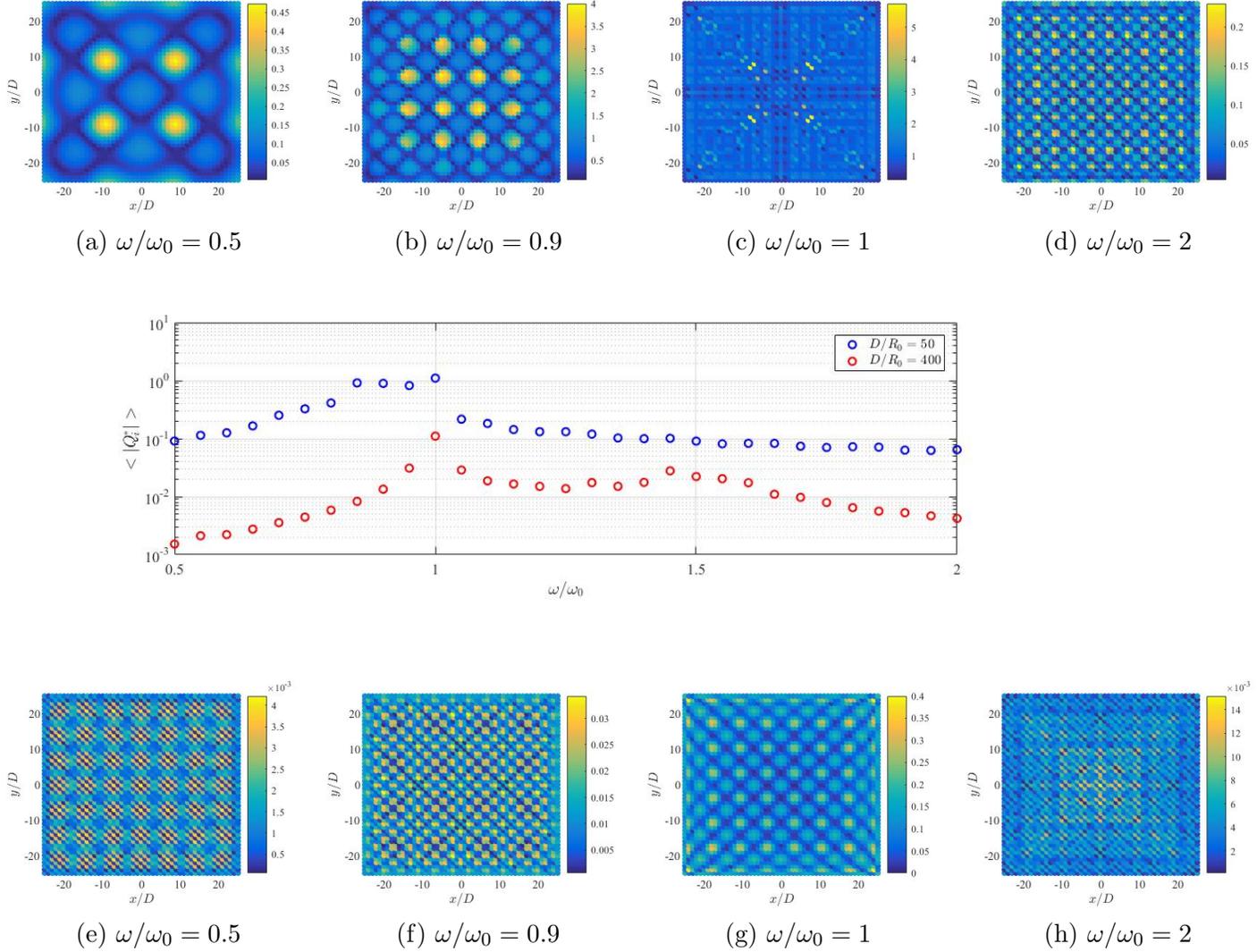


FIG. 6. The middle Figure shows the mean value of $|Q_i^*|$ of a 51×51 bubbly screen as a function of frequency for $D/R_0 = 50$ and $D/R_0 = 400$. Top Figures show the $|Q_i^*|$ maps for $D/R_0 = 50$; bottom ones are corresponding to $D/R_0 = 400$.

195 to find frequencies at which spatial patterns are difficult to identify (Figure 6c). Besides,
 196 bubble concentration shifts the resonance peak which also leads to a shift in the structures
 197 shown for a given frequency (Figure 6).

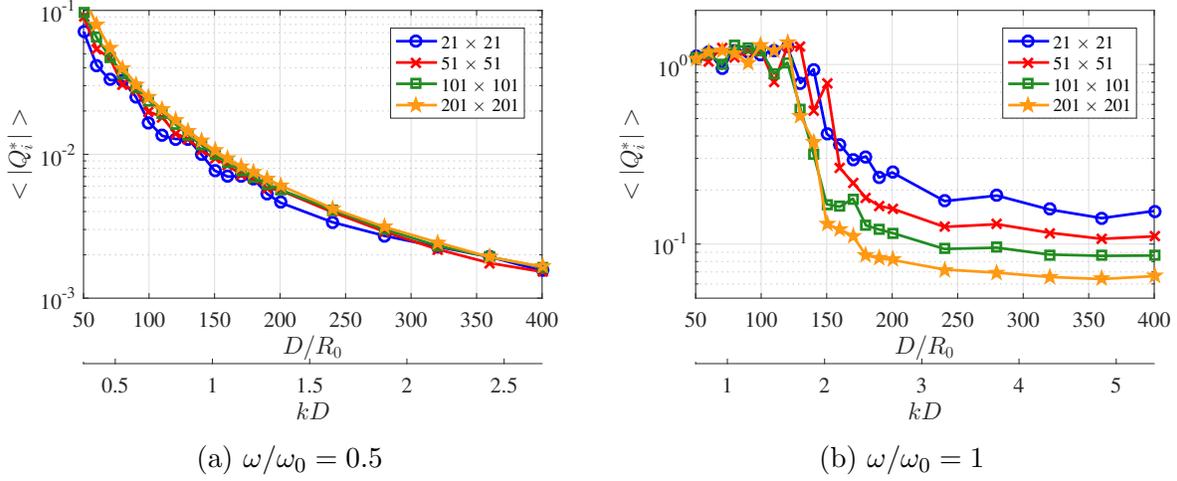


FIG. 7. Influence of concentration on $\langle |Q_i^*| \rangle$ for various finite size bubbly screens and two different values of ω/ω_0 .

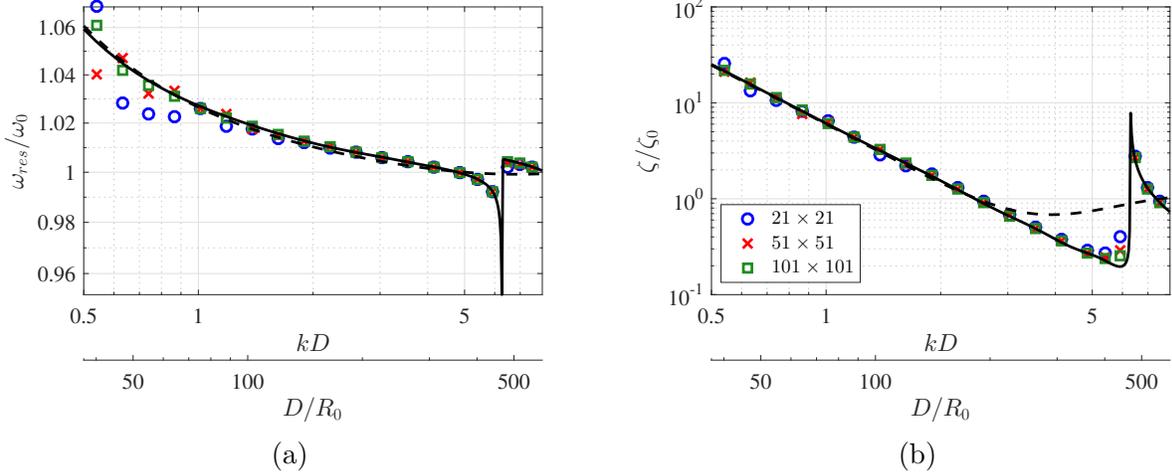


FIG. 8. Global resonance frequency and the global acoustical damping factor of finite bubbly screen with different screen sizes for $\omega/\omega_0 = 1$. 21×21 (blue circle), 51×51 (red cross sign) and 101×101 (green square). The theoretical curves calculated for an infinite system (black solid line, $N_l = 12000$) and effective medium theory are included for reference (dashed line).

198 The role of the concentration on $\langle |Q_i^*| \rangle$ is shown in Figure 7. At resonance (figure 7b),
 199 we observe a sharp transition between $kD \leq 2$, where the fluctuations of $\langle |Q_i^*| \rangle$ become
 200 of order unity, and $kD > 2$, where $\langle |Q_i^*| \rangle$ takes significantly smaller values. Remarkably,
 201 in the regime of $kD \leq 2$, we do not see any clear asymptotic convergence to $\langle |Q_i^*| \rangle \rightarrow 0$
 202 as we increase the number of bubbles in the screen. Below resonance (figure 7a), the value
 203 of $\langle |Q_i^*| \rangle$ is small but no clear convergence to zero is observed for the screens considered.
 204 One of the reasons for the slow convergence may be the excitation of non-uniform modes
 205 induced by boundary effects. The consequences of perturbation on the plane containing the
 206 bubbles in the infinite case (we have imposed an unperturbed planar wave in the y-z plane)
 207 is left for future works.

208

209 The effect of finite size effects on the global resonance frequency and damping factor can
 210 be seen in Figure 8 for $\omega/\omega_0 = 1$. The infinite bubbly screen limit captures accurately the
 211 averaged bubble response of the screen, only observing some small disagreement for very
 212 concentrated systems, where we have seen the non-uniformity on the bubble response is
 213 important.

214 D. Randomization

215 We discuss now the influence of the randomness on the position of the bubbles. To that
 216 end, we perturb the position of each bubble by a random number $-\Theta < \theta < \Theta$ with respect
 217 to the crystal configuration so that i th bubble is located at $\vec{x}_i = (0, y_i^{(c)} + \theta_{y,i}D, z_i^{(c)} + \theta_{z,i}D)$,
 218 where the superscript (c) stands for variables corresponding to the crystal configuration.

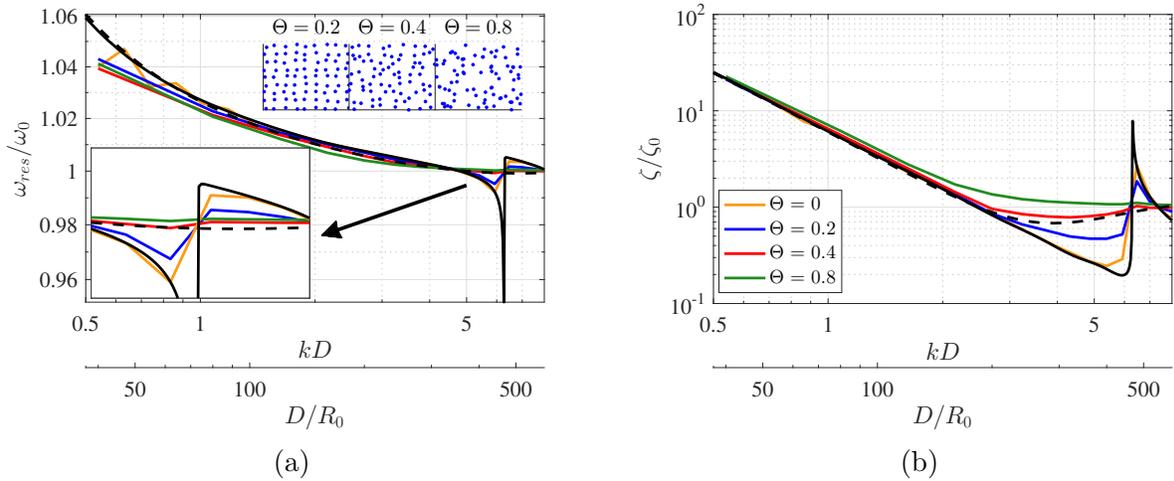


FIG. 9. Influence of randomness for (a) the global resonance and (b) the damping coefficient of a finite screen size 51×51 and $\omega/\omega_0 = 1$. An example of the spatial distribution of the bubble positions is given in the inset of (a). For reference we include curves calculated for an infinite system (black solid line, $N_l = 12000$) and effective medium theory (dashed line).

219 Figure 9 shows the global factors defined in equation 10 averaged over 100 realizations
 220 for $\omega/\omega_0 = 1$ using a finite screen with 51×51 bubbles with different concentrations. As
 221 expected, the resonance effects observed at $kD = 2\pi$ quickly vanish as the randomization
 222 parameter increases. Remarkably, the results obtained differ from the effective medium
 223 theory for large values of the randomization parameter and intermediate values of kD , the
 224 effect of randomization being especially visible on the effective damping coefficient.

225 In this case, both matrix $\mathbf{A}^{(0)}$ and matrix $\mathbf{A}^{(1)}$ can be further decomposed as a globally
 226 uniform value given by the crystal structure and a correction directly attributed to ran-
 227 domization (see Appendix A). While the expectation of $\mathbf{A}^{(0)}$ is zero, the non-linear term
 228 in the $\mathbf{A}^{(1)}$ matrix with respect to the position perturbation amplitude makes the averaged
 229 response of the system to be different from the crystal situation for small perturbations.

230 For large perturbations, the expectation of both $\mathbf{A}^{(0)}$ and $\mathbf{A}^{(1)}$ are a-priori different from
 231 zero, and converge to different number with different Θ . In such a situation, the differ-
 232 ence between the fluctuation around the crystal configuration and the completely random
 233 distribution also makes the averaged response of the system to be different from EMT. In
 234 Figure 9 we see that the randomization intensity parameter Θ mainly increases the effective
 235 damping for $kD > 1$.

236 IV. COMPRESSIBILITY EFFECTS IN THE NON-LINEAR REGIME

237 A. Numerical methods for differential equations with time delay

238 In the non-linear regime, it is no longer possible to find analytical solutions and one needs
 239 to solve the set of ODEs numerically. The differential equations considered can be written
 240 as

$$\dot{y}(t) = f(t, y(t), y(t - \tau_1), \dots, y(t - \tau_n), \dot{y}(t - \tau_1), \dots, \dot{y}(t - \tau_n)), \quad (17)$$

241 where y is called state variable representing bubble radius or bubble wall velocity in our
 242 case. Traditionally, Eq. 17 is usually solved as ordinary differential equations, and the
 243 time-delay effect thus has to be ignored ($\tau_1, \dots, \tau_n = 0$). In this work, when non-linear
 244 effects become important, Eq. 17 is directly solved, treated as neutral delay-differential
 245 equation (NDDE), which will reduce to general delay-differential equation (DDE) if $\dot{y}(t) =$
 246 $f(t, y(t), y(t - \tau_1), \dots, y(t - \tau_n))$ and extend to state dependent NDDE if any of (τ_1, \dots, τ_n)
 247 is a function of state variable (Bellen and Zennaro, 2013). Integration of DDEs cannot be
 248 based on the mere adaption of some standard ODE code to the presence of delayed terms,

249 which may dramatically modify the accuracy and stability of the underlying ODE method.

250 To deal with NDDE, we first rewrite the Eq. 17 as:

$$\dot{y}(t) = f(y(t), y(t - \tau_1), \dots, y(t - \tau_n), \frac{y(t - \tau_1) - y(t - \tau_1 - \delta_t)}{\delta_t}, \dots, \frac{y(t - \tau_n) - y(t - \tau_n - \delta_t)}{\delta_t}) \quad (18)$$

251 which is the dissipative approximation of the NDDE and named as retarded DDE. For small
252 enough δ_t , the retarded DDE solver will be stable as long as the neutral DDE is stable.

253 Based on Eq. 18, implicit Runge–Kutta formulas taking advantage of continuous extensions
254 is used, and the retarded DDE is solved accordingly with residual control. The works of
255 [Shampine \(2005, 2008\)](#) are recommended for detailed mathematical principles.

256 B. Numerical results

257 1. *Weakly non-linear regime*

258 One important aspect on the dynamic response of bubbly liquids is the appearance of
259 subharmonics, which ultimately indicate the first transition route to the chaotic response
260 obtained for large enough amplitude of excitation ([Lauterborn and Cramer, 1981](#); [Lauterborn and Koch, 1987](#)). The harmonic components of the acoustic wave scattered by bubbles
261 or ultrasound contrast agents is also important in medical applications ([Halldorsdottir et al., 2011](#); [Nio et al., 2019](#)). The harmonics emitted by bubbles has been described by many
262 authors (see [Lauterborn and Kurz \(2010\)](#) for a review), including studies for contrast agents
263 in a free field ([Andersen and Jensen, 2009](#); [Katiyar and Sarkar, 2011](#)). More recently [Fan et al. \(2020a\)](#) has revealed the impact of compressibility and bubble-wall interaction effects
264 on the subharmonic emission of a bubble in a rigid tube. However, the influence of collective
265
266
267

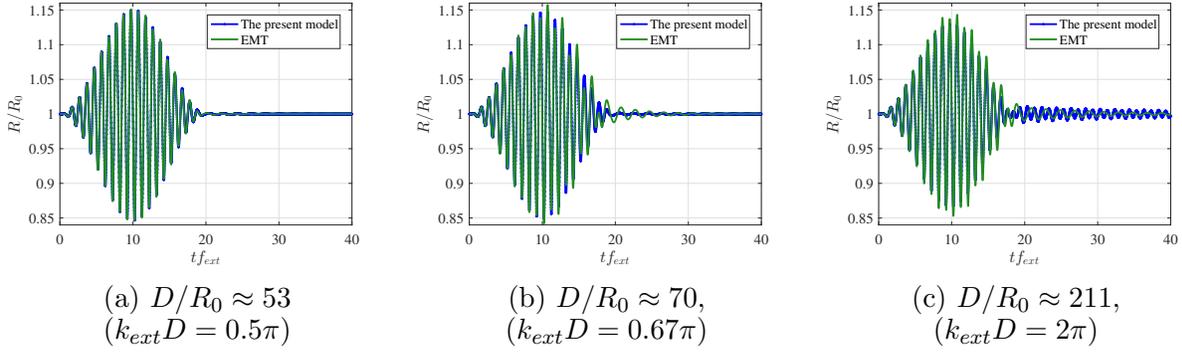


FIG. 10. The radius v.s. time curves. $p_a/p_0 = 2$.

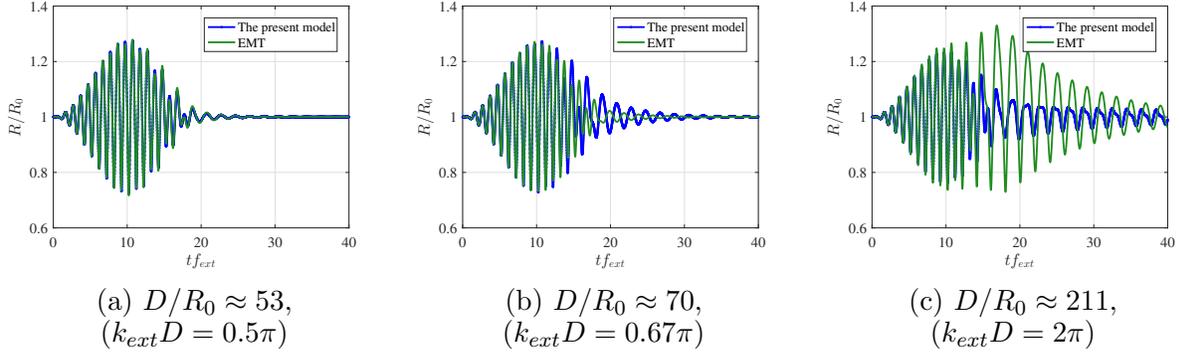


FIG. 11. The radius v.s. time curves. $p_a/p_0 = 3.5$.

268 effects on the subharmonic emission has not been investigated in detail yet.

269

270 In this section, we compare the results obtained from the model presented for infinite
 271 bubbly screens imposing synchronous motion ($R_i = R_j = R$) with the results obtained from
 272 the EMT in non-linear regimes (Pham *et al.*, 2021) where

$$I_{EMT} = -2\pi c \dot{R} \frac{R^2}{D^2} + 3.9 \frac{R}{D} (2\dot{R}^2 + \ddot{R}R). \quad (19)$$

273 To that end, we excite the bubbly screen with an incident pulse of the form

$$p_\infty(t) = p_0 - p_a \frac{1}{2} \left[1 - \cos\left(\frac{\omega_{ext}}{N_c} t\right) \right] \sin(\omega_{ext} t), \quad (20)$$

274 where $N_c = 20$, and $\omega_{ext} = 2\omega_0$ in order to favor the appearance of a stable subharmonic
 275 response. For simplicity, in this subsection we will only consider the response of an infinite
 276 bubble screen.

277

278 In Figures 10-11, we can see the influence of concentration on the dynamic response of
 279 an infinite bubbly screen for two different excitation amplitudes. Consistent with the results
 280 in the linear regime, the effective medium model converges to the present model when the
 281 value of D/R_0 , and therefore, $k_{ext}D$ is small. The differences between two models become
 282 significant as p_a/p_0 and $k_{ext}D$ increases. Even in the case, where the differences between the
 283 two models are important (figure 11c), both models fit relatively well for small times, and
 284 gradually become different only after some time. One explanation could be that in-phase
 285 and out-phase interactions coming from different layers at different time cancel each other
 286 and increase oscillatingly. Besides, the fact that the differences between models become
 287 visible after some time seem to indicate the differences of the EMT and the current model
 288 on the bifurcation diagrams (Lauterborn and Kurz, 2010).

289

290 Figure 12 shows the energy in the frequency spectrum of the infinite bubbly screen as a
 291 function of the bubble concentration from the radiated pressure (Pham *et al.*, 2021):

$$p_{rad} = 2\pi\rho c \frac{R^2\dot{R}}{D^2}. \quad (21)$$

292 The energy is calculated as $E = 20\log_{10}(\frac{|\mathfrak{F}(p_{rad})|}{|\mathfrak{F}(p_{rad})_{max}|})$, where $\mathfrak{F}(\cdot)$ is the Fourier transform,
 293 and $|\mathfrak{F}(p_{rad})_{max}|$ is highest energy observed among all simulations. Because the frequency
 294 of the subharmonic slightly shifts from $\frac{\omega_{ext}}{2}$ with the increasing of the amplitude of the

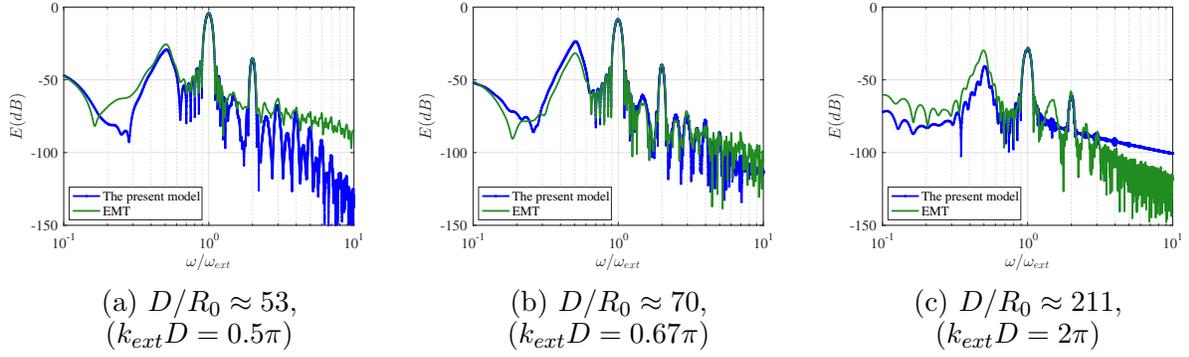


FIG. 12. The frequency spectrum of the present model and EMT using $p_a/p_0 = 3.5$. The energy is calculated by $E = 20\log_{10}(\frac{|\mathfrak{F}(p_{rad})|}{|\mathfrak{F}(p_{rad})_{max}|})$, where $|\mathfrak{F}(p_{rad})_{max}|$ is highest energy observed among all simulations.

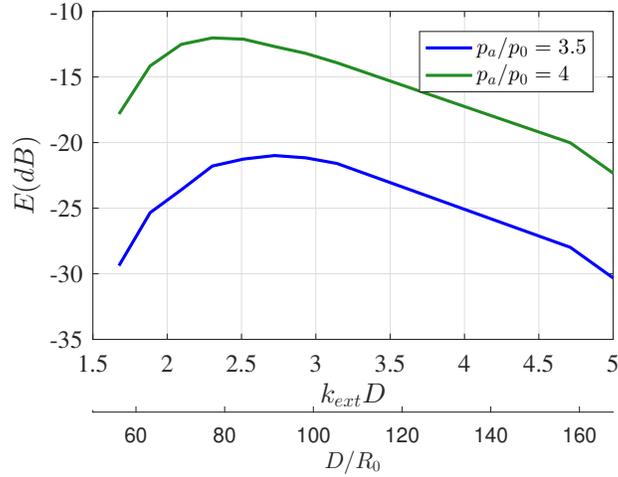


FIG. 13. Energy of the subharmonic as a function of concentration for a constant excitation frequency in a crystal structure.

295 driving pressure wave, the corresponding energy are chosen according to the peak amplitude
 296 rather than energy at $\frac{\omega_{ext}}{2}$. As expected the energy on the fundamental component increases
 297 as D/R_0 decreases due to the increase of bubble concentration (Figure 12). The overall
 298 spectrum is well reproduced by the EMT except for $kD = 2\pi$, where we clearly see how

299 the spectrum predicted by the EMT contains a significantly higher level of energy mainly
 300 concentrated at the subharmonic. In Figure 13, we show that optimal subharmonic emission
 301 conditions appears for $k_{ext}D = [0.65, 0.75]\pi$ as a consequence of the crystal configuration.
 302 This effect is not captured by the EMT.

303

304 2. Strongly non-linear regime

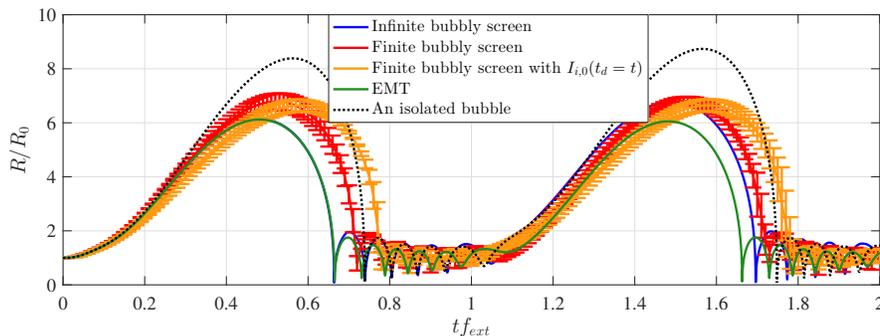


FIG. 14. Radius versus time curves predicted by different models for $\omega_{ext}/\omega_0 = 0.1$, $p_a/p_0 = 2$, $D/R_0 = 134$ for an infinite bubbly screen oscillating synchronously and a 11×11 bubbly screen. In the later case, we show the averaged and the standard deviation of the bubble radius using the full model (red line) and the incompressible model with $I_i = I_{i,0}$ and $t_d = t$ (yellow line).

When the excitation frequency is decreased ($\omega_{ext}/\omega_0 = 0.1$) the response of the bubbles become highly non-linear with a clear distinction between the expansion phase and the collapse and rebound region. In order to reduce the simulation time and transient effects, in this section we excite a bubbly screen with a perfect crystal configuration with an incident

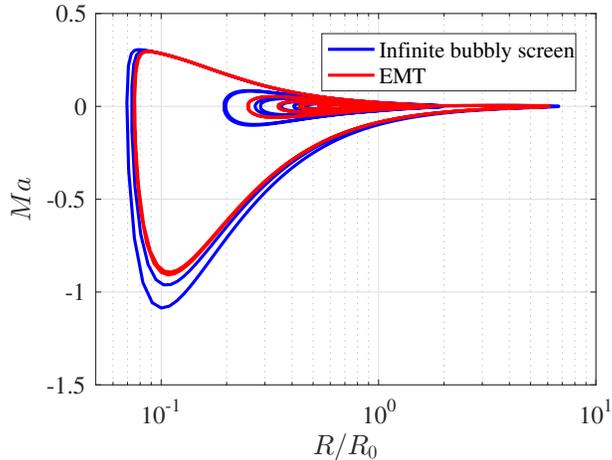


FIG. 15. Comparison of the trajectory of the averaged bubble radius versus $Ma = \dot{R}/c$ for the current model and the EMT.

planar wave represented by

$$p_{\infty}(t) = p_0 - p_a \sin(\omega_{ext}t).$$

305 The predictions of the temporal evolution of the bubble radius predicted by different models
 306 are given in Figure 14 for both infinite bubbly screens and finite bubbly screens. The am-
 307 plitude of the initial expansion in all cases is decreased compared to the isolating oscillating
 308 bubble. The results from the EMT fit well the results of the infinite bubbly screen in the
 309 first expansion. The difference of the radial dynamics between different models appear in
 310 the rebound stage (Figure 15), when the Mach number(\dot{R}/c) becomes important, so does
 311 the first order compressibility correction terms.

312

313 For completeness, in Figure 14 we also include the full simulation of a 11×11 bubbly
 314 screens. Because in this case bubble motion is no longer assumed to be synchronous, we

315 represent the averaged bubble radius among all bubbles in the screen as well as the standard
316 deviation in one realization. The influence of the screen is reduced in the expansion and is
317 less strong than in the infinite case. Compressible effects play a visible role despite the long
318 wavelength of the incident wave, and the classical incompressible bubble interaction model
319 tends to over-predict the collapse time.

320 V. CONCLUSION

321 In this work, the compressibility effect on the bubble-bubble interaction is discussed. The
322 model proposed in [Fuster and Colonius \(2011\)](#) is particularized to explicitly write a system
323 of equations that account for first order correction compressibility effects. These effects are
324 shown to be important compared with the classical incompressible interaction mechanism
325 in Rayleigh–Plesset models.

326

327 In the linear regime, time delay effects are always critical to capture the overall system
328 response of large bubble screens. We show that the current model recovers the effective
329 medium theory results up to second order for infinite crystal structures at large wavelengths
330 ($kD \ll 1$). In addition, the model is able to capture resonant conditions in diluted systems
331 due to crystal configurations that are not captured by averaged models. Randomization
332 on the bubble position and boundary effects on bubbly screens of finite are shown to be
333 responsible to the appearance of characteristic periodic structures in the screen. These
334 effects can modify the effective damping measured under some conditions.

335

336 In the non-linear oscillating regime, we numerically solve the proposed model as a neutral
 337 delay-differential set of equations (NDDE). The fully incompressible model seems to be only
 338 suitable to predict the expansion phase, while during the strong collapse compressibility
 339 effects play a major role and need to be included. Boundary size effects are shown to limit
 340 the applicability of the effective medium theory valid only for infinite systems.

341 ACKNOWLEDGMENTS

342 This research has been supported by NSFC, Project No. U1809212, No. U1709203 and
 343 No. 41576102.

344 APPENDIX A:

The system of equations 4 can be written in matrix form $\mathbf{A}\vec{r} = \vec{B}p'$ after imposing that the incident wave is $p_\infty = p_0(1 + p'e^{i\omega t})$ with $p' \ll 1$. The final system of equations becomes

$$\mathbf{A} = \mathbf{A}^{(0)} + ikR_0\mathbf{A}^{(1)} = \vec{B}p'$$

where

$$B_i = -\frac{p_0}{\rho R_0^2 \omega_0^2},$$

$$A_{ij}^{(0)} = \begin{cases} 1 - \left(\frac{\omega}{\omega_0}\right)^2 & \text{if } i = j, \\ -\left(\frac{\omega}{\omega_0}\right)^2 S_{ij} & \text{otherwise,} \end{cases}$$

$$A_{ij}^{(1)} = \begin{cases} \left(\frac{\omega}{\omega_0}\right)^2 (1 + \mathfrak{K}_i) - \mathfrak{K}_i & \text{if } i = j, \\ \left(\left(\frac{\omega}{\omega_0}\right)^2 (1 + \mathfrak{K}_i) + 1\right) S_{ij} & \text{otherwise,} \end{cases}$$

345 with $S_{ij} = \frac{R_0}{D} \frac{e^{-ikD\tilde{d}_{ij}}}{\tilde{d}_{ij}}$ and $\mathfrak{K}_i = \sum_{j \neq i}^N S_{ij}$.

346

In a general case where bubbles do not necessarily oscillate synchronously, it is possible to rewrite this system by separating variables S_{ij} and \mathfrak{K}_i into a uniform contribution and a spatially fluctuating part attributed to the perturbation of bubbles position

$$S_{ij} = S_{ij}^{(c)} + S'_{ij}$$

,

$$\mathfrak{K}_i = \mathfrak{K}_i^{(c)} + \mathfrak{K}'_i = \sum_{j \neq i}^N S_{ij}^{(c)} + \sum_{j \neq i}^N S'_{ij},$$

347 where the superscript (c) stands for variables corresponding to the crystal configuration, and

348 and the distances between bubbles is written as $\tilde{d}_{ij} = \tilde{d}_{ij}^{(c)} + \tilde{d}'_{ij}$. In this case matrix \mathbf{A} can

349 be further decomposed as $\mathbf{A} \approx \mathbf{A}^{(C)} + \mathbf{A}'$ where $\mathbf{A}^{(C)}$ represents the value of \mathbf{A} obtained

350 with the values of a crystal structure and \mathbf{A}' is the non-uniform part

$$A'_{ij} = \begin{cases} 0 & \text{if } i = j, \\ -\left(\frac{\omega}{\omega_0}\right)^2 S'_{ij} & \text{otherwise,} \end{cases}$$

$$A'^{(1)}_{ij} = \begin{cases} \left(\left(\frac{\omega}{\omega_0}\right)^2 - 1\right) \mathfrak{K}'_i & \text{if } i = j, \\ \left(\left(\frac{\omega}{\omega_0}\right)^2 + 1\right) S'_{ij} + \left(\frac{\omega}{\omega_0}\right)^2 (\mathfrak{K}'_i S'_{ij} + \mathfrak{K}_i^{(c)} S'_{ij} + \mathfrak{K}'_i S_{ij}^{(c)}) & \text{otherwise.} \end{cases}$$

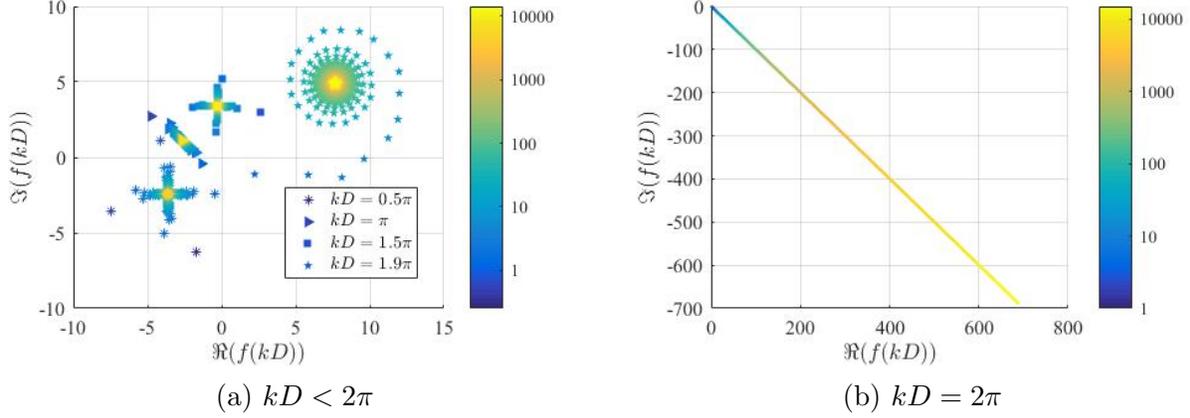


FIG. 16. Influence of the truncation N_l on the evaluation of the series in Eq. 13 for a crystal infinite screen and different values of kD . The colorbar is $N_l \frac{D}{\lambda}$.

When the position perturbation is small, taking advantage of Taylor expansion, we have:

$$S'_{ij} \approx -ikD \tilde{d}_{ij}^l \frac{R_0}{D} \frac{e^{-ikD \tilde{d}_{ij}^{(c)}}}{\tilde{d}_{ij}^{(c)}}.$$

351 In such a situation, the expectation of $A_{ij}^{(0)}$ is zero as long as the expectation of \tilde{d}_{ij}^l is zero.
 352 However the expectation of the $\Re'_i S'_{ij}$ term appearing in $A_{ij}^{(1)}$, which acts like a variance
 353 term, is different from zero even for the small perturbations. Obviously when the amplitude
 354 of perturbation \tilde{d}_{ij}^l is large, the expectation of both $A_{ij}^{(0)}$ and $A_{ij}^{(1)}$ are a-priori different from
 355 zero.

356 APPENDIX B:

357 The convergence of the infinite series

$$f(kD) = \sum_{l=1}^{\infty} \frac{4}{l} e^{-ikDl} \left(1 + \sum_{q=1}^l \frac{2}{\sqrt{1 + (q/l)^2}} e^{ikDl(1 - \sqrt{1 + (q/l)^2})} \right)$$

358 is discussed as follows. For sufficiently large value of l , because quantity $p = \sqrt{1 + (q/l)^2}$ is
 359 bounded between 1 and $\sqrt{2}$, we can approximate the series as

$$\sum_{q=1}^l \frac{2}{\sqrt{1 + (q/l)^2}} e^{\imath k D l (1 - \sqrt{1 + (q/l)^2})} \approx \int_1^{\sqrt{2}} \frac{2}{p} e^{\imath k D l (1-p)} dp = 2e^{\imath k D l} \left(E_{1/2}(\imath k D l) - 2^{1/4} E_{1/2}(\sqrt{2} \imath k D l) \right),$$

where $E(x)$ is the exponential integral function. Taking the limit for $l \rightarrow \infty$, we readily find
 that

$$\lim_{l \rightarrow \infty} \left(E_{1/2}(\imath k D l) - 2^{1/4} E_{1/2}(\sqrt{2} \imath k D l) \right) = 0$$

implying that this term always converges. The convergence of the series is then discussed
 in terms of the convergence of

$$\sum_{l=1}^{\infty} \frac{4}{l} e^{-\imath k D l} = \sum_{l=1}^{\infty} \frac{z^l}{l} = \ln \left(\frac{1}{1-z} \right)$$

360 where $z = e^{-\imath k D}$. For $kD = 2\pi n$ the series diverges and it converges otherwise. The influ-
 361 ence of the number of layers considered on the series is reported in Figure 16 for different
 362 values of kD . In general, a very large value of the number of layers is required to accurately
 363 represent the infinity limit.

364

365

366 Andersen, K. S., and Jensen, J. A. (2009). “Ambient pressure sensitivity of microbubbles
 367 investigated through a parameter study,” *The Journal of the Acoustical Society of America*
 368 **126**(6), 3350–3358.

369 Bellen, A., and Zennaro, M. (2013). *Numerical methods for delay differential equations*
 370 (Oxford university press).

371 Bremond, N., Arora, M., Ohl, C.-D., and Lohse, D. (2006). “Controlled multibubble surface
372 cavitation,” *Physical review letters* **96**(22), 224501.

373 Caffisch, R. E., Miksis, M. J., Papanicolaou, G. C., and Ting, L. (1985). “Effective equations
374 for wave propagation in bubbly liquids,” *Journal of Fluid Mechanics* **153**, 259–273.

375 Commander, K. W., and Prosperetti, A. (1989). “Linear pressure waves in bubbly liquids:
376 Comparison between theory and experiments,” *The Journal of the Acoustical Society of*
377 *America* **85**(2), 732–746.

378 Coussios, C. C., and Roy, R. A. (2008). “Applications of acoustics and cavitation to nonin-
379 vasive therapy and drug delivery,” *Annu. Rev. Fluid Mech.* **40**, 395–420.

380 Dahl, P. H., and Kapodistrias, G. (2003). “Scattering from a single bubble near a rough-
381 ened air–water interface: Laboratory measurements and modeling,” *The Journal of the*
382 *Acoustical Society of America* **113**(1), 94–101.

383 Devaud, M., Hocquet, T., and Leroy, V. (2010). “Sound propagation in a monodisperse
384 bubble cloud: From the crystal to the glass,” *The European Physical Journal E* **32**(1),
385 13–23.

386 Doinikov, A. A., Manasseh, R., and Ooi, A. (2005). “Time delays in coupled multibubble
387 systems (1),” *The Journal of the Acoustical Society of America* **117**(1), 47–50.

388 Faez, T., Emmer, M., Kooiman, K., Versluis, M., van der Steen, A. F., and de Jong, N.
389 (2012). “20 years of ultrasound contrast agent modeling,” *IEEE transactions on ultrason-*
390 *ics, ferroelectrics, and frequency control* **60**(1), 7–20.

391 Fan, Y., Li, H., and Fuster, D. (2020a). “Optimal subharmonic emission of stable bubble
392 oscillations in a tube,” *Physical Review E* **102**(1), 013105.

393 Fan, Y., Li, H., Zhu, J., and Du, W. (2020b). “A simple model of bubble cluster dynamics
394 in an acoustic field,” *Ultrasonics sonochemistry* **64**, 104790.

395 Foldy, L. L. (1945). “The multiple scattering of waves. i. general theory of isotropic scat-
396 tering by randomly distributed scatterers,” *Physical review* **67**(3-4), 107.

397 Fuster, D. (2019). “A review of models for bubble clusters in cavitating flows,” *Flow, Tur-
398 bulence and Combustion* **102**(3), 497–536.

399 Fuster, D., and Colonius, T. (2011). “Modelling bubble clusters in compressible liquids,”
400 *Journal of Fluid Mechanics* **688**, 352–389.

401 Gilmore, F. R. (1952). “The growth or collapse of a spherical bubble in a viscous compress-
402 ible liquid,” .

403 Halldorsdottir, V. G., Dave, J. K., Leodore, L. M., Eisenbrey, J. R., Park, S., Hall, A. L.,
404 Thomenius, K., and Forsberg, F. (2011). “Subharmonic contrast microbubble signals for
405 noninvasive pressure estimation under static and dynamic flow conditions,” *Ultrasonic
406 imaging* **33**(3), 153–164.

407 Ida, M., Naoe, T., and Futakawa, M. (2007). “Suppression of cavitation inception by gas
408 bubble injection: A numerical study focusing on bubble-bubble interaction,” *Physical
409 Review E* **76**(4), 046309.

410 Ilinskii, Y. A., Hamilton, M. F., and Zabolotskaya, E. A. (2007). “Bubble interaction dy-
411 namics in lagrangian and hamiltonian mechanics,” *The Journal of the Acoustical Society
412 of America* **121**(2), 786–795.

413 Katiyar, A., and Sarkar, K. (2011). “Excitation threshold for subharmonic generation from
414 contrast microbubbles,” *The Journal of the Acoustical Society of America* **130**(5), 3137–

415 3147.

416 Keller, J. B., and Miksis, M. (1980). “Bubble oscillations of large amplitude,” The Journal
417 of the Acoustical Society of America **68**(2), 628–633.

418 Lauterborn, W., and Cramer, E. (1981). “Subharmonic route to chaos observed in acous-
419 tics,” Physical Review Letters **47**(20), 1445.

420 Lauterborn, W., and Koch, A. (1987). “Holographic observation of period-doubled and
421 chaotic bubble oscillations in acoustic cavitation,” Physical Review A **35**(4), 1974.

422 Lauterborn, W., and Kurz, T. (2010). “Physics of bubble oscillations,” Reports on progress
423 in physics **73**(10), 106501.

424 Leroy, V., Strybulevych, A., Lanoy, M., Lemoult, F., Tourin, A., and Page, J. H. (2015).
425 “Superabsorption of acoustic waves with bubble metascreens,” Physical Review B **91**(2),
426 020301.

427 Leroy, V., Strybulevych, A., Scanlon, M., and Page, J. (2009). “Transmission of ultrasound
428 through a single layer of bubbles,” The European Physical Journal E **29**(1), 123–130.

429 Lohse, D. (2018). “Bubble puzzles: From fundamentals to applications,” Physical review
430 fluids **3**(11), 110504.

431 Lombard, O., Barrière, C., and Leroy, V. (2015). “Nonlinear multiple scattering of acoustic
432 waves by a layer of bubbles,” EPL (Europhysics Letters) **112**(2), 24002.

433 Maeda, K., and Colonius, T. (2019). “Bubble cloud dynamics in an ultrasound field,”
434 Journal of fluid mechanics **862**, 1105.

435 Manasseh, R., Nikolovska, A., Ooi, A., and Yoshida, S. (2004). “Anisotropy in the sound
436 field generated by a bubble chain,” Journal of Sound and Vibration **278**(4-5), 807–823.

437 Mettin, R., Akhatov, I., Parlitz, U., Ohl, C., and Lauterborn, W. (1997). “Bjerknes forces
438 between small cavitation bubbles in a strong acoustic field,” *Physical review E* **56**(3), 2924.

439 Miksis, M. J., and Ting, L. (1989). “Effects of bubbly layers on wave propagation,” *The*
440 *Journal of the Acoustical Society of America* **86**(6), 2349–2358.

441 Nio, A. Q., Faraci, A., Christensen-Jeffries, K., Raymond, J. L., Monaghan, M. J., Fuster,
442 D., Forsberg, F., Eckersley, R. J., and Lamata, P. (2019). “Optimal control of sonovue
443 microbubbles to estimate hydrostatic pressure,” *IEEE transactions on ultrasonics, ferro-*
444 *electrics, and frequency control* **67**(3), 557–567.

445 Okita, K., Sugiyama, K., Takagi, S., and Matsumoto, Y. (2013). “Microbubble behavior
446 in an ultrasound field for high intensity focused ultrasound therapy enhancement,” *The*
447 *Journal of the Acoustical Society of America* **134**(2), 1576–1585.

448 Ooi, A., Nikolovska, A., and Manasseh, R. (2008). “Analysis of time delay effects on a linear
449 bubble chain system,” *The Journal of the Acoustical Society of America* **124**(2), 815–826.

450 Pham, K., Mercier, J.-F., Fuster, D., Marigo, J.-J., and Maurel, A. (2021). “Scattering of
451 acoustic waves by a nonlinear resonant bubbly screen,” *Journal of Fluid Mechanics* **906**.

452 Prosperetti, A., Lezzi, A. *et al.* (1986). “Bubble dynamics in a compressible liquid. part 1.
453 first-order theory,” *J. FLUID MECH.*, 1986, **168**, 457–478.

454 Shampine, L. (2005). “Solving odes and ddes with residual control,” *Applied Numerical*
455 *Mathematics* **52**(1), 113–127.

456 Shampine, L. F. (2008). “Dissipative approximations to neutral ddes,” *Applied Mathematics*
457 *and Computation* **203**(2), 641–648.

458 Sujarittam, K., and Choi, J. J. (2020). “Angular dependence of the acoustic signal of a
459 microbubble cloud,” *The Journal of the Acoustical Society of America* **148**(5), 2958–2972.

460 van’t Wout, E., and Feuillade, C. (2021). “Proximity resonances of water-entrained air
461 bubbles near acoustically reflecting boundaries,” *The Journal of the Acoustical Society of*
462 *America* **149**(4), 2477–2491.

463 Yasui, K., Iida, Y., Tuziuti, T., Kozuka, T., and Towata, A. (2008). “Strongly interacting
464 bubbles under an ultrasonic horn,” *Physical Review E* **77**(1), 016609.

465 Ye, Z., and Feuillade, C. (1997). “Sound scattering by an air bubble near a plane sea
466 surface,” *The Journal of the Acoustical Society of America* **102**(2), 798–805.