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1           **Highly porous seeding-free boron-doped ultrananocrystalline diamond used**  
2 **as high-performance anode for electrochemical removal of carbaryl from water**

3  
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26        **Abstract**

27        Boron-doped diamond (BDD) electrodes are regarded as the most promising catalytic materials that are  
28 highly efficient and suitable for application in advanced electrochemical oxidation processes targeted at the  
29 removal of recalcitrant contaminants in different water matrices. Improving the synthesis of these electrodes  
30 through the enhancement of their morphology, structure and stability has become the goal of the material  
31 scientists. The present work reports the use of an ultranano-diamond electrode with a highly porous structure  
32 (B-UNCD<sub>ws</sub>/TDNT/Ti) for the treatment of water containing carbaryl. The application of the proposed  
33 electrode at current density of 75 mA cm<sup>-2</sup> led to the complete removal of the pollutant (carbaryl) from the  
34 synthetic medium in 30 min of electrolysis with an electric energy per order of 4.01 kWh m<sup>-3</sup> order<sup>-1</sup>. The  
35 results obtained from the time-course analysis of the carboxylic acids and nitrogen-based ions present in the  
36 solution showed that the concentrations of nitrogen-based ions were within the established maximum levels  
37 for human consumption. Under optimal operating conditions, the proposed electrode was successfully  
38 employed for the complete removal of carbaryl in real water. Thus, the findings of this study show that the  
39 unique, easy-to-prepare BDD-based electrode proposed in this study is a highly efficient tool which has  
40 excellent application potential for the removal of recalcitrant pollutants in water.

41

42

43        *Keywords:* Recalcitrant pollutants; Water treatment; Advanced oxidation processes; Electrochemical  
44 technologies; Boron-doped diamond synthesis.

45

## 1. Introduction

Anodic oxidation (AO) is one of the major electrochemically-driven technologies which have been widely applied for the remediation of recalcitrant organic substances - including dyes, personal care and pharmaceutical products, and pesticides, usually present in water bodies (Sirés and Brillas, 2012; Sirés et al., 2014; Baddouh et al., 2018; Garcia-Segura et al., 2018b; Martínez-Huitle and Panizza, 2018; dos Santos et al., 2021b;). AO is considered an environmentally friendly technique as the process does not require the use of chemicals and oxidants are electrogenerated *in situ*. Several studies have shown that the electrocatalytic properties of the anode material are among the main factors that determine the efficiency of the AO process (Panizza and Cerisola, 2009; Sirés et al., 2014; Moreira et al., 2017; dos Santos et al., 2019, 2021a). In this context, boron-doped diamond (BDD) anode is regarded as the best material for application in AO due to its excellent properties including high stability, inert surface, and large O<sub>2</sub> overpotential window (Kapałka et al., 2009). The large O<sub>2</sub> overpotential window of BDD anode helps generate a huge amount of oxidant species such as physisorbed hydroxyl radicals (M(<sup>•</sup>OH), Eq. (1) which can attack organic pollutants (R) non-selectively, turning them into non-hazardous products or even leading them to complete combustion, as shown in Eq. (2) below (do Vale Júnior et al., 2019; Brillas, 2021; Karim et al., 2021; Mostafa et al., 2021).



The properties of BDD can be enhanced considerably by varying the concentration of boron, film thickness, and sp<sup>2</sup>/sp<sup>3</sup> ratio, as well as the electrode morphology and porosity (Baluchová et al., 2019; Mei et al., 2019). As pointed out in the literature, one can promote the contact between the electrolyte and the electrode by increasing the electrochemical surface area through the adjustment of the film porosity from macro to nanoporous depending on both the porosity of the substrate and specific post-growth treatment on the diamond surface. So far, a number of studies reported in the literature have employed the seeding substrate pre-treatment mechanism to boost the diamond growth through the application of the chemical vapor deposition technique (Wei et al., 2009; Szunerits et al., 2015; Yang et al., 2016). This pre-treatment mechanism involves the use of diamond powder to improve diamond growth since diamond is unable to grow naturally on non-diamond substrates. Due to the fast deposition kinetics, this seeding substrate pre-treatment procedure, which boosts the diamond growth, favors the formation of agglomerated structures; on the other hand, the fast deposition

74 kinetics makes it harder to obtain structures with nano or ultranano-porosity which are more suitable and  
75 efficient for improving the efficiency of the AO process (May and Mankelevich, 2008; Luong et al., 2009;  
76 Macpherson, 2015).

77 As an alternative to the typical BDD synthesis method, in a previous study (Vernasqui et al., 2022), our  
78 research group proposed the use of an innovative boron-doped ultrananocrystalline diamond grown on titanium  
79 dioxide nanotube without the seeding substrate pre-treatment procedure (B-UNCD<sub>ws</sub>/TDNT/Ti). The use of  
80 titanium dioxide nanotubes (TDNT) allows spontaneous diamond growth under slower deposition kinetics  
81 compared to the seeding process, and this enables one to have higher control of deposition and the ability to  
82 produce extremely thin films, in addition to maintaining the porosity of the substrate material. This approach  
83 represents a major step forward in the synthesis of BDD and helps explore the unique properties of BDD when  
84 it comes to the treatment of recalcitrant pollutants. Thus, this study evaluates the efficiency of the innovative  
85 B-UNCD<sub>ws</sub>/TDNT/Ti electrode when applied for the removal of carbaryl (CBR) pesticide in both synthetic  
86 and real media under the AO process. Carbaryl is a broad-spectrum N-methyl carbamate insecticide applied  
87 worldwide for the control of pests during the production of crops (cotton, corn, soybean, nut, fruits, and  
88 vegetables) and for the protection of lawns, home gardens and other ornamental plants (Koshlukova and Reed,  
89 2014).

90 CBR ranks second among the insecticides that are commonly detected in surface water (Nair et al., 2022).  
91 CBR can dissolve in water, migrate through soil, and find its way into groundwater, contaminating it (Wu et  
92 al., 2019). People are mostly exposed to CBR through the intake of food and water or other liquids. Depending  
93 on the individual and the dose of CBR ingested into the body, the person may experience a variety of symptoms  
94 which range from weakness to reduced heart and lung function. In view of that, it is essentially important to  
95 develop techniques that are capable of removing this type of contaminant from food and water so as to prevent  
96 excessive human exposure to this pollutant and the occurrence of severe health problems in humans. To  
97 analyze the efficiency and viability of the proposed anode in terms of CBR degradation, different current  
98 densities were tested, and the best operating conditions were applied for the analysis of real drinking water  
99 with a view to evaluating the potential of the technique in real applications. The presence of different oxidants  
100 in the system was evaluated using scavenger compounds. Energetic figures of merit were calculated, and the  
101 evolution of intermediates produced during the treatment process was also thoroughly monitored. For

102 comparison purposes, the study also provides comprehensive data related to the physical and electroanalytical  
103 characterization of the proposed B-UNCD<sub>ws</sub>/TDNT/Ti anode.  
104

## 105 **2. Materials and methods**

### 106 *2.1 Chemical reagents*

107 Carbaryl (CBR) pesticide (99 % purity, Sigma-Aldrich) was used as a model pollutant. Analytical grade  
108 potassium sulfate – acquired from Neon, was used as supporting electrolyte; methanol (MeOH) and *tert*-  
109 butanol (TBH), both acquired from Sigma Aldrich, were used as scavengers; and acetonitrile – obtained from  
110 Merck, was used as mobile phase for the conduct of high-performance liquid chromatography (HPLC)  
111 analysis. All reagents were used directly without extra purification. Ultrapure water from a Millipore Milli-Q  
112 system (electric resistivity >18 M $\Omega$  cm at 25 °C) was used to prepare the aqueous solutions.

### 113 *2.2 B-UNCD<sub>ws</sub>/TDNT/Ti synthesis and characterization*

114 The synthesis of the B-UNCD<sub>ws</sub>/TDNT/Ti electrode was performed under a two-step approach. The first  
115 step involved obtaining anodized TDNTs and the second step involved the deposition of diamond through the  
116 application of the hot filament chemical vapor deposition (HFCVD) technique as described by (Vernasqui et  
117 al., 2022). A commercial microcrystalline BDD thin film doped on a silicon substrate (acquired from NeoCoat)  
118 were employed for comparison purposes. The synthesized anode material (B-UNCD<sub>ws</sub>/TDNT/Ti) was  
119 analyzed by field emission gun scanning electron microscopy (FEG-SEM, TESCAN Mira 3), Raman  
120 scattering spectroscopy - using 514.5 nm line of argon ion-laser (Lab- RAMHR evolution from Horiba  
121 Scientific), and X-ray diffraction (XDR – PANanalytical model X'Pert Pro MPD diffractometer with CuK $\alpha$   
122 radiation). Cyclic voltammetry (CV), linear scan voltammetry (LSV), and electrochemical impedance  
123 spectroscopy (EIS) measurements were performed using N<sub>2</sub>-saturated H<sub>2</sub>SO<sub>4</sub> or K<sub>2</sub>SO<sub>4</sub> solutions with the aid of  
124 an Autolab PGSTAT128N potentiostat/galvanostat equipped with FRA2.X module. The electrochemical  
125 assays were carried out in a three-electrode electrochemical cell which consisted of the following: B-  
126 UNCD<sub>ws</sub>/TDNT/Ti, Pt plate (Degussa) and Ag/AgCl (~3.0 M KCl, Analyser Co.) used as working, counter,  
127 and reference electrodes, respectively. The specific capacitance values were determined by the double-layer  
128 capacitance (C<sub>dl</sub>) method as described in (McCrory et al., 2013). The LSV analyses were performed in a  
129 potential window ranging from 0 to 3.0 V *vs.* Ag/AgCl at scan rate of 20 mV s<sup>-1</sup>. The impedance analyses were  
130 conducted at 2.3 V *vs.* Ag/AgCl, with potential perturbation of 25 mV (rms) and frequency range of 10 mHz  
131 to 100 kHz. The EIS data were analyzed using an electric equivalent circuit (EEQC) with the aid of the Nova®

132 2.1.4 software. Water contact angle measurements were performed using Attension Theta Flex tensiometer by  
133 pouring water droplets (of 5  $\mu\text{L}$ ) on the B-UNCD<sub>WS</sub>/TDNT/Ti electrode.

### 134 2.3 Anodic oxidation experimental setup and analytical techniques

135 The electrochemical treatment of CBR in 50 mM  $\text{K}_2\text{SO}_4$ , at  $\text{pH} = 7.0$ , was carried out in a 250 mL lab-scale  
136 glass reactor operated at 400 rpm magnetic stirring rate, at 25 °C. The anode/cathode pair employed for the  
137 conduct of the experiments was as follows: B-UNCD<sub>WS</sub>/TDNT/Ti (geometric area of 2.0  $\text{cm}^2$ ) – as anode, and  
138 a platinum wire – as cathode. The electrodes were positioned vertically with 1.0 cm distance between them.  
139 All experiments were performed at constant current density ( $j$ ) using a power supply from MINIPA (MPL-  
140 3305). Prior to the conduct of each experiment, the electrodes were cleaned using a 50 mM  $\text{K}_2\text{SO}_4$  solution at  
141  $j=100 \text{ mA cm}^{-2}$  for 20 min. The drinking water used in the experiments was obtained from the water treatment  
142 plant in the city of Bariri, São Paulo State, Brazil – the effluent was stored at 4 °C. Table 1 shows the physical  
143 chemical characterization of the real effluent. At predetermined periods of time (0, 5, 10, 15, 20, 30, 40, 50  
144 and 60 min), the samples were collected, filtered, and injected into the Shimadzu High-Performance Liquid  
145 Chromatograph (HPLC) for the analysis of the rate/degree of carbaryl removal. A C18 column (250 $\times$ 4.6, 5  
146  $\mu\text{m}$ ) was used for the HPLC analysis, and the mobile phase employed consisted of a mixture of  
147 water/acetonitrile (ratio 60:40) applied at a flow rate of 1.0  $\text{mL min}^{-1}$ . The electric energy per order (EE/O), a  
148 figure of merit established by the IUPAC (Lanzarini-Lopes et al., 2017), was estimated based on Eq. (3) in  
149 order to determine the economic viability of the AO process.

$$150 \quad EE/O = (\text{kWh m}^{-3} \text{order}^{-1}) = \frac{E_{\text{cell}} I t}{V_s \log(c_0/c_f)} \quad (3)$$

151 where  $E_{\text{cell}}$  is the cell potential (V),  $I$  is the current intensity (A),  $t$  is the experiment time (s),  $V_s$  is the solution  
152 volume (L), and  $c_0$  and  $c_f$  correspond to the initial and final concentrations of CBR (Garcia-Segura et al., 2018).

153 The mineralization of the pollutant was evaluated by the Total Organic Carbon (TOC) technique using the  
154 Shimadzu VCPN TOC equipment. Carboxylic acids and nitrogenous species were detected using the Metrohm  
155 Ion Chromatography system, as described by (dos Santos et al., 2021a).

156



157 **Table 1.** Physical-chemical characterization of the drinking water employed in the experiments.

<b>Physical Characteristics</b>	<b>Values</b>
pH	7.50
Conductivity (uS cm <sup>-1</sup> )	129.7
Total organic carbon (mg C L <sup>-1</sup> )	0.45
<b>Chemical Characteristics</b>	<b>Values (mg L<sup>-1</sup>)</b>
Ammonia (NH <sub>4</sub> <sup>+</sup> )	0.134
Calcium (Ca <sup>2+</sup> )	12.79
Magnesium (Mg <sup>2+</sup> )	2.94
Potassium (K <sup>+</sup> )	1.23
Sodium (Na <sup>+</sup> )	4.47
Chloride (Cl <sup>-</sup> )	3.31
Nitrate (NO <sub>3</sub> <sup>-</sup> )	0.72
Sulfate (SO <sub>4</sub> <sup>2-</sup> )	1.55

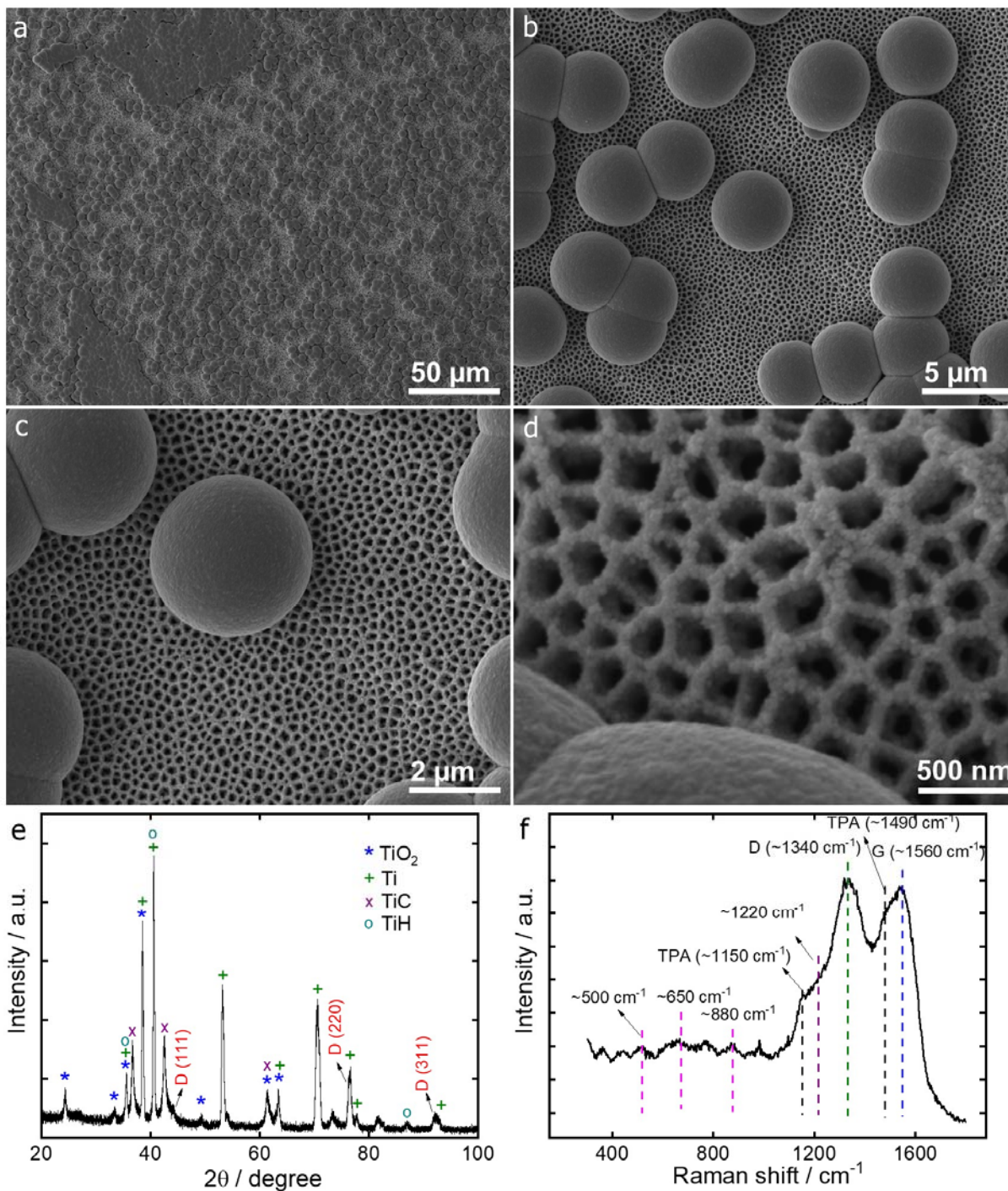
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### 159 **3. Results and discussion**

#### 160 *3.1. Morphological, physical, and electrochemical characterizations of the B-UNCD<sub>WS</sub>/TDNT/Ti*

161 Figure 1(a-d) shows the remarkable homogeneous morphology of the UNCD<sub>WS</sub>/TDNT/Ti with different  
 162 growth planes obtained after chemical vapor deposition on TDNT in different magnifications. As can be  
 163 observed, the entire surface of the electrode is covered by a thin layer, and one will notice the presence of a  
 164 diamond film in the pore walls which helps maintain the porosity of the electrode surface. Furthermore, one  
 165 can see clusters of ballas diamond which are distributed on the sample surface. In the XRD analysis (Fig. 1e),  
 166 the crystalline peaks observed were identified as TiO<sub>2</sub>, TiC, TiH, and Ti –based on the Inorganic Crystal  
 167 Structure Database (ICSD: 9658, 044494, 044747, and 076144, respectively). The diamond peaks (111), (220),  
 168 and (311) present in  $2\theta = 44.1^\circ$ ,  $76.3^\circ$ , and  $91.9^\circ$  can be found convoluted with other peaks (Ownby et al.,  
 169 1992). The (220) preferential orientation in the diffractogram is related to the high nucleation process which  
 170 is enhanced by the TiC – derived from the formation of TiO<sub>2</sub> on the TDNT substrate, present on the electrode  
 171 surface (Vernasqui et al., 2022). Fig. 1f shows the Raman spectra obtained at the standard 514 nm wavelength.  
 172 As expected, the sample exhibited a typical ultranano-diamond behavior, with signal bands attributed to the  
 173 formation of trans-poly-acetylene at around 1,150 and 1,490 cm<sup>-1</sup> and a band at around 1,220 cm<sup>-1</sup> which is  
 174 attributed to the inclusion of boron in the diamond lattice, in addition to the usual G band (1,560 cm<sup>-1</sup>, attributed  
 175 to E<sub>2g</sub> vibration). The diamond peak typically located at 1,332 cm<sup>-2</sup> for microcrystalline films is completely  
 176 hidden in the sample by the D band attributed to amorphous sp<sup>2</sup> bonds, which is usually expected for these

177 films. In addition, one will observe the presence of three other peaks at around 500, 650, and 880  $\text{cm}^{-1}$  linked  
 178 to B dimers vibrations (Mermoux et al., 2002; Crisci et al., 2008; dos Santos et al., 2022).



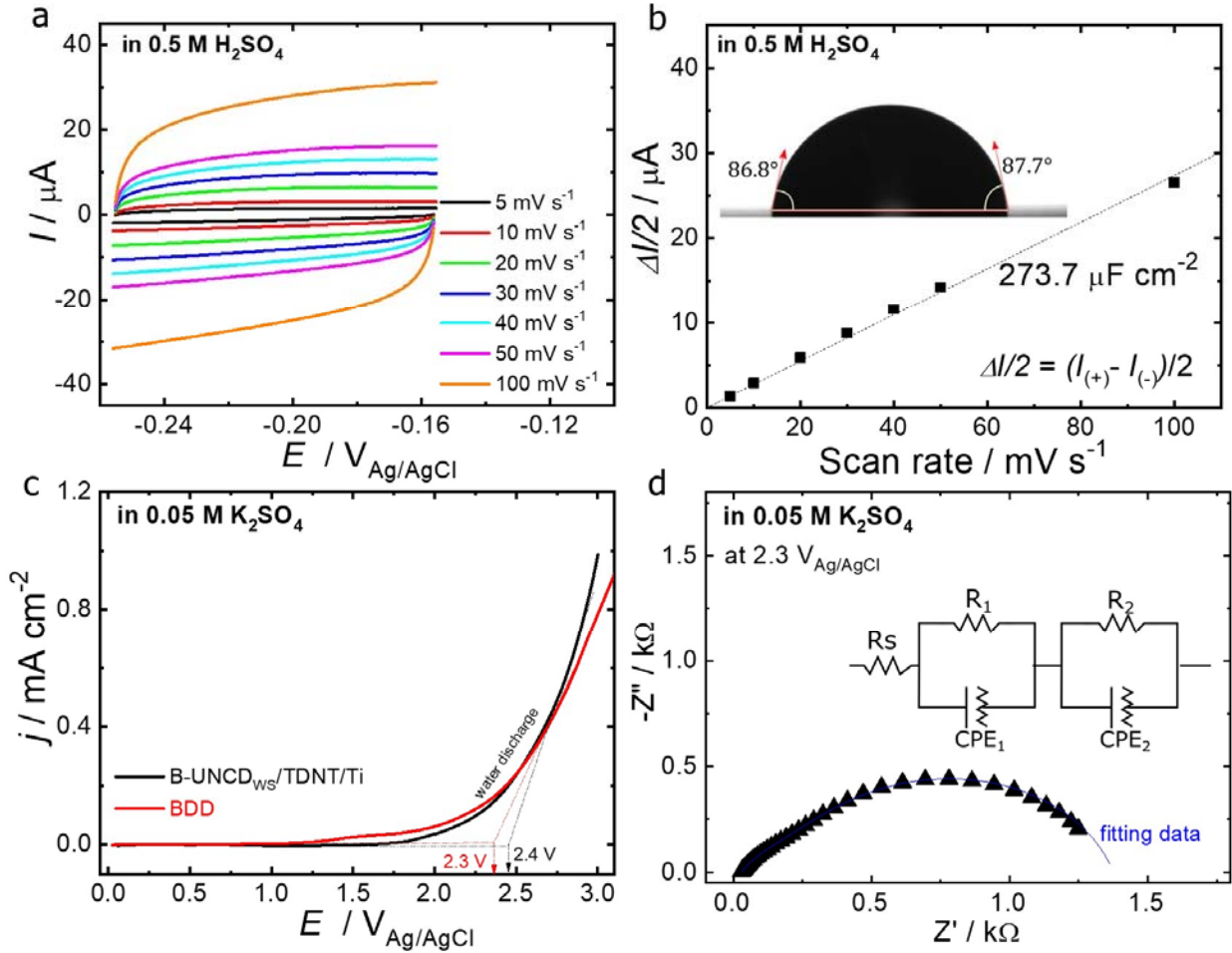
179

180 **Fig 1.** Physical characterization of the B-UNCD<sub>ws</sub>/TDNT/Ti electrode. (a-d) Representative FEG-SEM  
 181 images, (e) XRD pattern, and (f) Raman spectra.

182

183 Fig. 2a shows the capacitive features of the surface of the B-UNCD<sub>WS</sub>/TDNT/Ti electrode which was  
184 evaluated in N<sub>2</sub>-saturated 50mM H<sub>2</sub>SO<sub>4</sub> solution. The CVs recorded at different scan rates in the double layer  
185 region (centered at the open circuit potential) point to the capacitive effect of the electrode. Based on the plot  
186 of average peak current *versus* scan rate in Fig. 2b, the B-UNCD<sub>WS</sub>/TDNT/Ti electrode recorded specific  
187 capacitance of ca. 274 μF cm<sup>-2</sup>; this value is higher than the specific capacitance value obtained for micro and  
188 nanocrystalline diamond films (115 μF cm<sup>-2</sup>, on average) previously reported in the literature (dos Santos et  
189 al., 2022). The high specific capacitance values obtained for the electrode reflect the existence of high surface  
190 roughness and high active surface area, which provides the electrolyte solution access to the electrode surface  
191 (Frackowiak and Béguin, 2001; Siuzdak et al., 2015). The inset of Fig. 2b shows the hydrophobicity/wettability  
192 of the surface of the B-UNCD<sub>WS</sub>/TDNT/Ti electrode; this was evaluated using the water contact angle  
193 measurement procedure. A water contact angle of ca. 87° shows that the B-UNCD<sub>WS</sub>/TDNT/Ti material is a  
194 reasonably wettable substrate. A surface with intermediate wettability can provide the electrolyte solution easy  
195 access to the electrode surface and facilitated mass transport of gaseous species formed on the electrode surface  
196 which, when combined together, lead to the improvement of the electrolysis efficiency efficiency (Almeida et  
197 al., 2008; Watanabe et al., 2010). Linear scan voltammetry (LSV) measurements were recorded in N<sub>2</sub>-saturated  
198 50 mM K<sub>2</sub>SO<sub>4</sub> solution, as shown in Fig. 2c. As can be observed, the B-UNCD<sub>WS</sub>/TDNT/Ti electrode exhibited  
199 an onset potential for water discharge at 2.45 V *vs.* Ag/AgCl; this value is slightly higher than the values  
200 previously reported for diamond films with different morphologies (dos Santos et al., 2022) and for commercial  
201 microcrystalline BDD thin film - which exhibited an onset potential of 2.35 V *vs.* Ag/AgCl. Onset potential  
202 values for water discharge greater than 1.23 V *vs.* SHE (ca. 1.03 V *vs.* Ag/AgCl) are expected to favor the  
203 generation of reactive oxygen species (i.e •OH) rather than oxygen evolution during the electrolysis process  
204 (Kapałka et al., 2007). The seeding-free production of diamond allows the formation of highly porous  
205 ultranano-structures - which are in line with the surface characteristics of the substrate used, favoring the  
206 formation of extremely thin diamond films. In fact, this behavior is observed in the B-UNCD<sub>WS</sub>/TDNT/Ti  
207 electrode, since an extremely thin-porous diamond film covering the TDNT gives rise to relatively lower  
208 current densities for water discharge compared to the current densities typically presented by micro- and nano-  
209 diamonds (dos Santos et al., 2022) .

210



211

212 **Fig 2.** Electrochemical characterization of the B-UNCD<sub>ws</sub>/TDNT/Ti electrode. (a) Cyclic voltammograms  
 213 obtained from the application of N<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> as supporting electrolyte at different scan rates. (b)  
 214  $\Delta I/2$  vs. scan rate plot; inset: water contact angle measurement. (c) LSV curves for B-UNCD<sub>ws</sub>/TDNT/Ti and  
 215 commercial BDD electrodes obtained in N<sub>2</sub>-saturated 0.05 M K<sub>2</sub>SO<sub>4</sub> (employed as supporting electrolyte) and  
 216 scan rate of 20 mV s<sup>-1</sup>. The scan started at 0 V vs. Ag/AgCl. (d) Complex-impedance plane representation;  
 217 inset: simulated electric equivalent circuit (EEQC).

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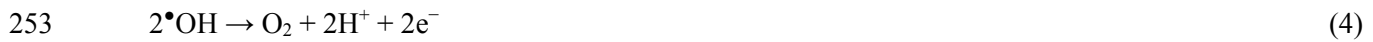
219 Fig. 2d shows the complex-impedance plot obtained for the B-UNCD<sub>ws</sub>/TDNT/Ti electrode in N<sub>2</sub>-  
 220 saturated 50 mM K<sub>2</sub>SO<sub>4</sub> close to the water discharge onset potential. The EIS response revealed the capacitive-  
 221 resistive character of the ultranano-diamond electrode, which is characterized by two structural layers linked  
 222 to the presence of TDNT/Ti. The simulated electric equivalent circuit (EEQC) can be represented by a  
 223 resistance related to the electrolyte and two RQ components, where both are connected in series (Ennaceri et  
 224 al., 2020) (R(RQ)(RQ) circuit, c.f. inset of Fig. 2d). The first RQ component is associated with large porous

225 spherical ultranano-diamond structures; these structures consist of a charge transfer resistance and a constant  
226 phase element (CPE) which is linked to the double layer capacitance (Almeida et al., 2008). The second RQ  
227 component, which exhibits a more resistive character, is linked to porous TDNT which is finely coated by  
228 ultranano-diamond film probably with some exposed TDNT dots (Ennaceri et al., 2020). The results obtained  
229 from the physical and electrochemical characterization analyses show that the B-UNCD<sub>ws</sub>/TDNT/Ti electrode  
230 has outstanding physical-chemical properties, and this makes it highly suitable for application in  
231 electrocatalytic water technologies as will be discussed in the next section.

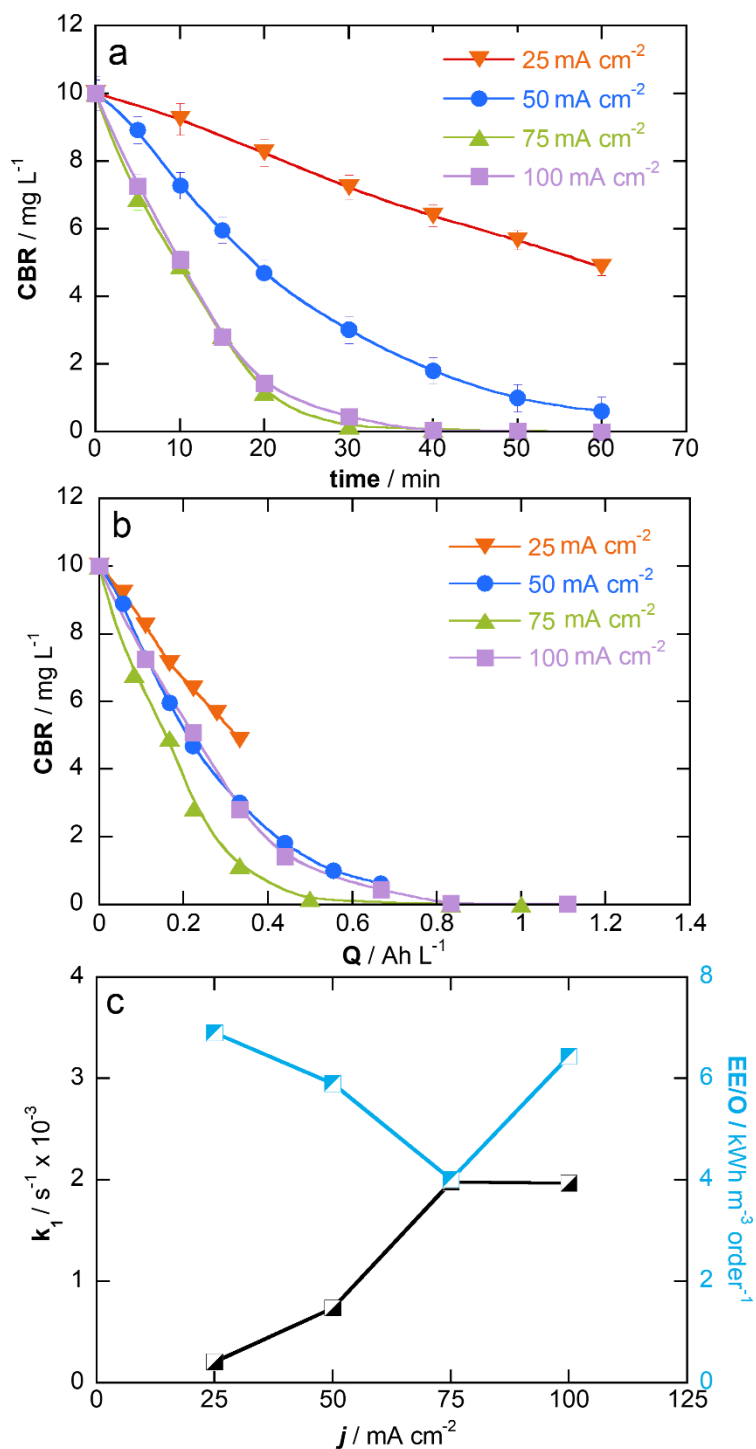
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### 233 3.2. Electrochemical treatment of CBR using the B-UNCD<sub>ws</sub>/TDNT/Ti anode.

234 In electrochemical advanced oxidative processes (EAOPs), current density ( $j$ ) is an essentially important  
235 electrokinetic parameter; this parameter controls the quantity of electrons circulating in the system, and  
236 consequently, the amount of  $\bullet\text{OH}$  that can be generated. Bearing that in mind, the efficiency of the B-  
237 UNCD<sub>ws</sub>/TDNT/Ti anode was assessed based on the application of different current densities for the treatment  
238 of 10 mg L<sup>-1</sup> of carbaryl (CBR) in 50 mM K<sub>2</sub>SO<sub>4</sub> (used as supporting electrolyte) at pH = 7.0. Looking at the  
239 results shown in Fig. 3a, one will observe that the application of the B-UNCD<sub>ws</sub>/TDNT/Ti anode effectively  
240 resulted in CBR degradation irrespective of the current density applied. Interestingly though, after 30 min of  
241 treatment, there were changes in the degradation pattern. The following degradation rates (in decreasing order)  
242 were obtained under the application of different current densities: 75 mA cm<sup>-2</sup> (99.9 %) > 100 mA cm<sup>-2</sup> (97.5  
243 %) > 50 mA cm<sup>-2</sup> (69.9 %) > 25 mA cm<sup>-2</sup> (27.8 %). An approximately 9-fold increase was observed in CBR  
244 degradation from the current density of 25 to 75 mA cm<sup>-2</sup> over time; this was certainly due to the increase in  
245 the amount of  $\bullet\text{OH}$  generated in the electrolysis (Eq. (1)). However, the two highest applied current densities  
246 (75 and 100 mA cm<sup>-2</sup>) exhibited a quite similar behavior in terms of CBR removal; this behavior can be  
247 attributed to the presence of parasitic/non-oxidative reactions. Indeed, the occurrence of parasitic reactions is  
248 favored by the increase in current density due to the competition between  $\bullet\text{OH}$  with O<sub>2</sub> evolution (Eq. (4)).  
249 Another point worth mentioning is that due to its non-selective character,  $\bullet\text{OH}$  can react with each other  
250 (dimerization reaction), producing hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>), which is a weaker oxidant compared to  $\bullet\text{OH}$  –  
251 see reaction 5 below (Brillas et al., 2010; Srivastava et al., 2021). Both reactions 4 and 5 decrease the oxidative  
252 power of the system once they consume  $\bullet\text{OH}$ .



255 From the viewpoint of the applied charge, the pattern of CBR degradation shown in Fig. 3b is quite similar  
256 to that observed in Fig. 3a. At 0.33 Ah L<sup>-1</sup>, the final CBR concentrations obtained from the application of  
257 current densities of 25, 50, 100 and 75 mA cm<sup>-2</sup> were 4.87, 3.01, 2.81, 1.16 mg L<sup>-1</sup>, respectively. In fact, the  
258 optimal *j* value that promoted a complete removal of CBR was 75 mA cm<sup>-2</sup>, with charge consumption of 0.50  
259 Ah L<sup>-1</sup>; for comparison purposes, the application of the current density of 100 mA cm<sup>-2</sup> requires charge  
260 consumption of 0.84 Ah L<sup>-1</sup> to obtain a complete removal of CBR. Taking a closer look at the relationship  
261 between the pseudo-first-order kinetics constant (*k*<sub>1</sub>) and EE/O (Fig. 3c), one will observe that when *k*<sub>1</sub>  
262 increases, EE/O decreases – see the following results obtained at different current densities: 25 mA cm<sup>-2</sup>  
263 (2.1x10<sup>-4</sup> s<sup>-1</sup>, R<sup>2</sup> = 0.994; 6.90 kWh m<sup>-3</sup> order<sup>-1</sup>), 50 mA cm<sup>-2</sup> (7.4x10<sup>-4</sup> s<sup>-1</sup>, R<sup>2</sup> = 0.991; 5.87 kWh m<sup>-3</sup> order<sup>-1</sup>),  
264 100 mA cm<sup>-2</sup> (1.8x10<sup>-3</sup> s<sup>-1</sup>, R<sup>2</sup> = 0.983; 6.44 kWh m<sup>-3</sup> order<sup>-1</sup>) and 75 mA cm<sup>-2</sup> (1.9x10<sup>-3</sup> s<sup>-1</sup>, R<sup>2</sup> = 0.987; 4.01  
265 kWh m<sup>-3</sup> order<sup>-1</sup>). These results clearly show that high *j* values are required for the effective degradation of  
266 CBR; in essence, this finding shows that there is a mass transfer mechanism controlled by diffusion in which  
267 the porosity plays a fundamental role by increasing the anode effective surface and favoring the pollutants-  
268 oxidant contact. The supply of energy above *j* = 75 mA cm<sup>-2</sup> does not translate into better performance and  
269 greater cost-effectiveness of the process, as observed in Figs. 3a-c. In fact, the application of current densities  
270 above 75 mA cm<sup>-2</sup> may fuel the occurrence of non-oxidizing reactions as previously discussed; in contrast, the  
271 application of current densities below 75 mA cm<sup>-2</sup> may cause resistance in the system probably due to the low  
272 level of boron on the anode surface. Thus, the current density of 75 mA cm<sup>-2</sup> was selected for the conduct of  
273 further experiments.



274 **Fig 3.** Effect of current density on the degradation of CBR concentration relative to (a) electrolysis time  
 275 and (b) applied charge. (c) Pseudo-first order kinetic decay of CBR and electrical energy per order versus  
 276 current density. Operating conditions: 10 mg L<sup>-1</sup> of CBR; 50 mM of K<sub>2</sub>SO<sub>4</sub> (used as supporting electrolyte) at  
 277 pH = 7.0.

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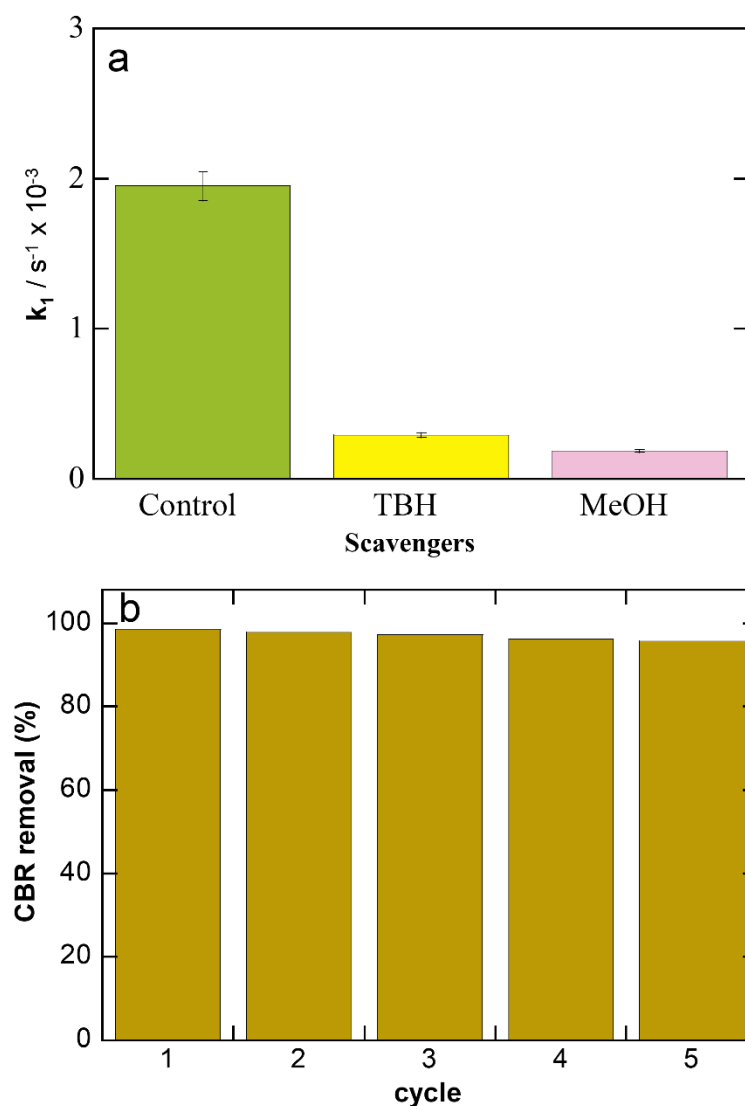
279 The AO process allows the in-situ generation of radical species. To gain a meaningful understanding  
 280 regarding the contribution of these radical species in the degradation of CBR, TBH was used to scavenge  $\bullet\text{OH}$ ,  
 281 while MeOH was used to scavenge  $\bullet\text{OH}$  and  $\text{SO}_4^{\bullet-}$ . Different pollutant:scavenger ratios (1:50, 1:100, 1:200,  
 282 1:400) were used to find the optimal testing concentration. The  $k_1$  values obtained for CBR removal were found  
 283 to be influenced by the presence of scavengers up to the ratio 1:200; the values then remained constant at  
 284 higher concentrations – after 1:200 (data not shown). So, when the ratio of 1:200 was employed, the application  
 285 of the TBH and MeOH scavengers led to a reduction in the  $k_1$  value from  $1.9 \times 10^{-3} \text{ s}^{-1}$  to  $2.9 \times 10^{-4} \text{ s}^{-1}$  and  $1.8 \times 10^{-4}$   
 286  $\text{ s}^{-1}$  (Fig. 4a), respectively. A careful analysis of these results showed that  $\bullet\text{OH}$  - the main oxidant, represented  
 287 84.7% of the results ( $= 100 \times (k_{1,\text{control}} - k_{1,\text{TBH}})/k_{1,\text{control}}$ ), while  $\text{SO}_4^{\bullet-}$  represented only 5.8% ( $((k_{1,\text{TBH}} -$   
 288  $k_{1,\text{MeOH}})/k_{1,\text{control}})$ ), and the rest accounted for 9.5%. It should be noted that  $\text{SO}_4^{\bullet-}$  can be electrogenerated through  
 289 direct oxidation via one-electron of sulfate - see Eq. (6). The remaining 9.5% can be attributed to non-radical  
 290 oxidation which is associated with the direct oxidation of the pollutant and persulfate activation - both  
 291 phenomena occurring on the anode surface (Song et al., 2018).



293 The stability of the *B-UNCD<sub>WS</sub>/TDNT/Ti* electrode for longer operation periods was evaluated using five  
 294 consecutive fed-batch tests of 60 min duration. During all the tests, the operating conditions were kept  
 295 unchanged. As can be seen in Fig. 4b, the carbaryl removal rate was practically the same (around 100%) for  
 296 the first five tests; this result points to the efficient performance and long-term stability of the *B-*  
 297 *UNCD<sub>WS</sub>/TDNT/Ti* electrode applied for the degradation of recalcitrant compounds in water.

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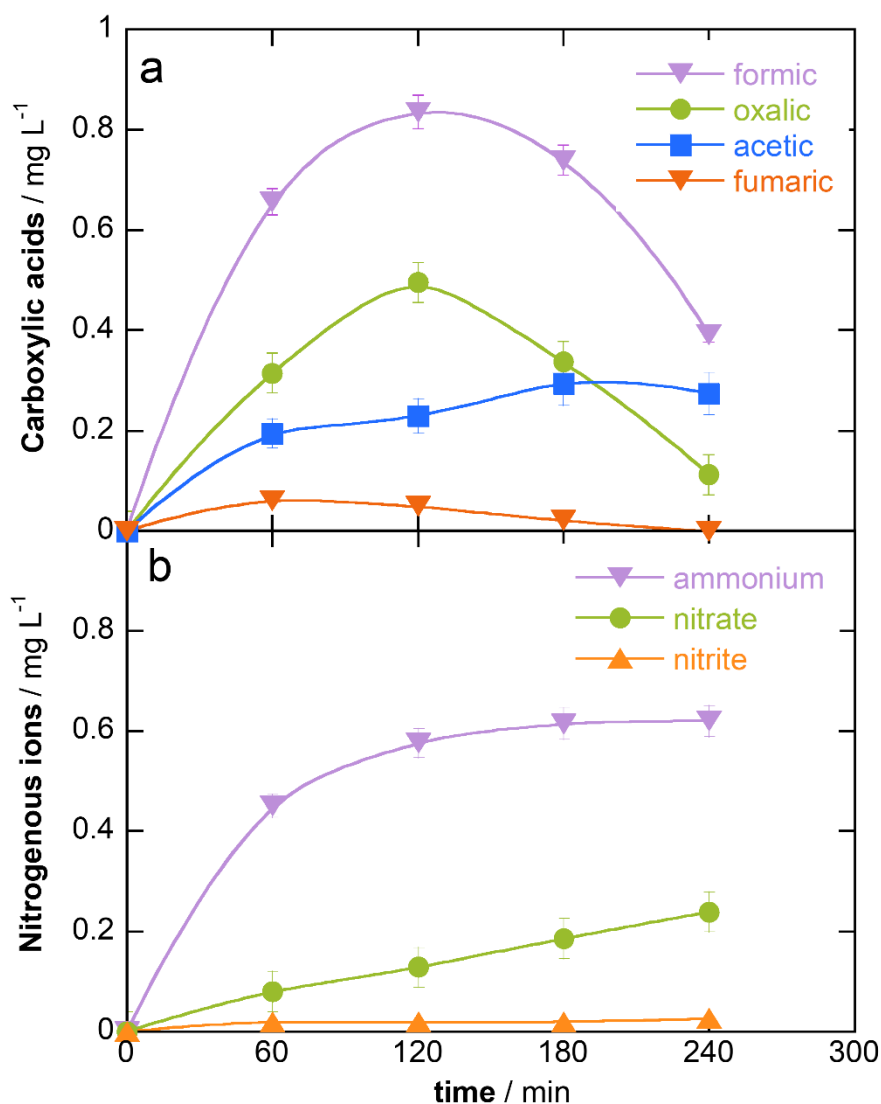


299 **Fig 4.** (a) Effect of the application of different scavengers on the pseudo-first order kinetic decay of CBR.  
 300 (b) Effect of the B-UNCD<sub>WS</sub>/TDNT/Ti electrode on CRB removal over 5 cycles of electrolysis. Operating  
 301 conditions: 10 mg L<sup>-1</sup> of CBR; 50 mM of K<sub>2</sub>SO<sub>4</sub> at pH = 7.0 (employed as supporting electrolyte).

302

303 Although complete CBR degradation was obtained, the environmental problem has still not yet to be  
 304 addressed. In certain treatment processes, the final by-products obtained after the treatment are found to be  
 305 more persistent than the original pollutant. In view of that, a thorough analysis was performed to study the  
 306 mineralization process ( $\approx 95\%$  - data not shown) and identify/quantify the final by-products generated after  
 307 the pollutant treatment process. Fig 5a shows the time-course of the evolution of the concentration of short  
 308 linear carboxylic acids derived from the opening of the naphthalene group present in the CBR. The results  
 309 obtained from the mineralization analysis pointed to the presence of a mixture of oxalic, fumaric, formic, and

310 acetic acids, with maximum concentrations of 0.496 mg L<sup>-1</sup> (120 min), 0.061 mg L<sup>-1</sup> (60 min), 0.835 mg L<sup>-1</sup>  
311 (120 min) and 0.295 mg L<sup>-1</sup> (180 min), respectively, which were partially converted to CO<sub>2</sub>, with the exception  
312 of the fumaric acid which was completely mineralized. In addition, an analysis was also performed in order to  
313 study the evolution of nitrogenous ions – see the results obtained in Fig. 5b. Looking at the results shown in  
314 Fig 5b, one will observe that the initial amount of nitrogen in the CBR (0.649 mg L<sup>-1</sup>) was mostly converted  
315 to ammonia (0.62 mg L<sup>-1</sup> - 74.30%), followed by nitrate (0.23 mg L<sup>-1</sup> - 8.32%) and nitrite (0.026 mg L<sup>-1</sup> -  
316 1.23%). The remaining 16.15% of the total mass was probably related to volatile N-products, as reported in  
317 previous studies (Çelebi et al., 2015; Oriol et al., 2021). Depending on their concentration levels, the exposure  
318 to nitrate, nitrite, and ammonia ions may pose serious risks to human health. However, it is worth mentioning  
319 that the remaining concentrations of nitrate and nitrite after the electrochemical treatment were found to be  
320 below the maximum contamination level (MCL) stipulated for drinking water according to the US  
321 Environmental Protection Agency (EPA): 10.0 and 1.0 mg N L<sup>-1</sup>, respectively. According to the same agency,  
322 there is no legally established MCL for ammonia.



324 **Fig 5.** Time course of the evolution of (a) short linear carboxylic acids and (b) nitrogenous species  
 325 during the treatment of 10 mg L<sup>-1</sup> of CBR in 50 mM K<sub>2</sub>SO<sub>4</sub>, with pH = 7.0 (employed as supporting  
 326 electrolyte), and  $j = 75 \text{ mA cm}^{-2}$ .

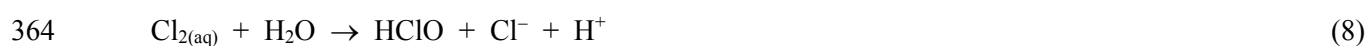
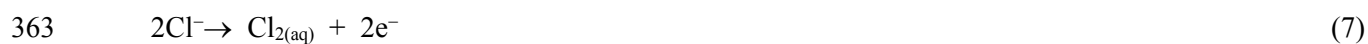
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### 328 3.3. Electrochemical treatment of CBR in real medium

329 Clearly, the experiments conducted using ultrapure water helped us understand the degree of efficiency of  
 330 the treatment process applied in this study and its mechanism of operation for the removal of CBR in synthetic  
 331 medium. However, conducting experiments in synthetic aqueous medium alone is not sufficient for us to have  
 332 a more realistic understanding of the treatment process and the impact of the presence of other compounds  
 333 (i.e., inorganic ions, natural organic matter) on the pollutant degradation. Thus, based on the satisfactory results  
 334 obtained from the experiments conducted using synthetic medium, we evaluated the efficiency of the *B*-

335 *UNCDWS/TDNT/Ti* anode when applied for the treatment of real effluents. The analysis was conducted using  
336 the optimal current density of  $75 \text{ mA cm}^{-2}$  in real drinking water spiked with different concentrations of CBR  
337 ( $5.0 - 20 \text{ mg L}^{-1}$ ). As can be observed in Fig. 6, irrespective of the initial concentration of CBR, there was a  
338 sharp decrease in the pollutant concentration in the first 15 min of reaction; thereafter, the decrease in the  
339 pollutant concentration took a more gradual pattern. The initial concentration of CBR is a parameter of interest  
340 since it provides one with fundamental information regarding the range of pollutant concentration that can be  
341 efficiently treated in reasonable periods of time. For instance, in 30 min of treatment, the pollutant removal  
342 rates obtained were 99.8 %, 93.5 % and 89.4% for the initial concentrations of 5.0, 10, and  $20 \text{ mg L}^{-1}$ ,  
343 respectively.

344 The analysis of real water samples shows the presence of other compounds besides the pollutant and the  
345 electrolyte, and this can positively or negatively affect the removal of the contaminant. A comparison of the  
346 results obtained from the experiments conducted using real effluent with the results obtained from the  
347 experiments conducted using synthetic medium under the same operating conditions showed that the span of  
348 time required to obtain a complete removal of the pollutant was 1.2 times higher in the real effluent than in the  
349 synthetic medium (with a reduction of  $k_1$  from  $1.9 \times 10^{-3} \text{ s}^{-1}$  to  $1.6 \times 10^{-3}$  for the experiment in real effluent and  
350 in synthetic medium, respectively). The presence of natural organic matter in the real medium (Table 1)  
351 competes for the electrogenerated oxidants, undermining the efficiency of the process. On the other hand, the  
352 presence of chloride in real medium allows the electrogeneration of active chlorine species ( $\text{Cl}_{2(\text{aq})}$  – Eq. (7);  
353  $\text{HClO}$  – Eq. (8);  $\text{OCl}^-$  – Eq. (9)), which may enhance the performance of the system. Generally, these species  
354 are generated at the following pH levels:  $\text{pH} \leq 3$  ( $\text{Cl}_{2(\text{aq})}$ ), pH range 3-8 ( $\text{HClO}$ ), and  $\text{pH} > 8$  ( $\text{ClO}^-$ ). Thus, the  
355 oxidation of organic matter mediated by active chlorine species is found to be stronger in acidic than in alkaline  
356 media due to the higher standard potential of  $\text{Cl}_{2(\text{aq})}$  ( $E^\circ = 1.36 \text{ vs SHE}$ ) and  $\text{HClO}$  ( $E^\circ = 1.49 \text{ vs SHE}$ ) compared  
357 to that of  $\text{ClO}^-$  ( $E^\circ = 0.89 \text{ vs SHE}$ ) (Burgos-Castillo et al., 2018; Garcia-Segura et al., 2018b). However, it  
358 seems that the presence of chlorine species in the medium did not have such a significant impact on CBR  
359 removal; this was probably because of the low initial concentration of chloride, which was not enough to  
360 induce the electrogeneration of high amount of active chlorine species. It is interesting to note that at the end  
361 of the experiment, no chloro oxyanions, such as chlorate and perchlorate, were detected in the solution; this is  
362 evidently reassuring because these species are carcinogenic.

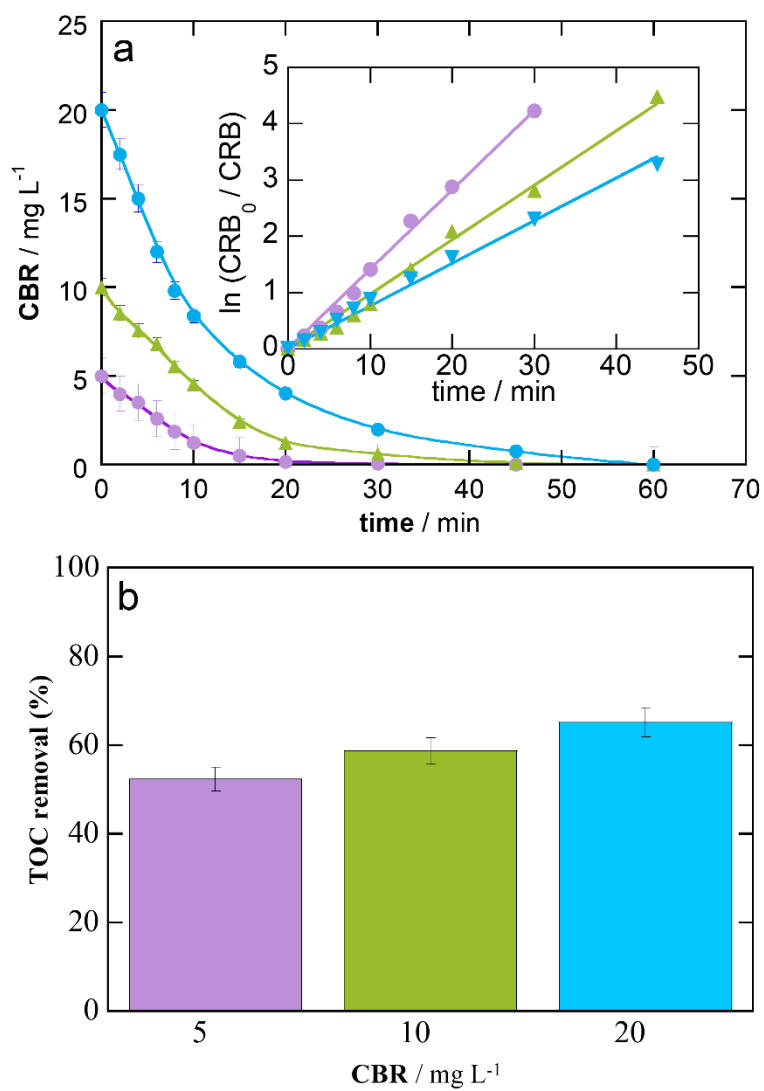


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367 With regard to the mineralization tests performed using the real effluent (Fig. 6b), the results obtained showed  
368 that none of the experiments yielded 100% removal rates. In fact, at the end of the treatment, TOC removal  
369 rates of 52.3, 58.7 and 65.2% were obtained for the tests conducted using 5, 10 and 20 mg L<sup>-1</sup> of CBR,  
370 respectively. Increasing the concentration of CBR may lead to the generation and accumulation of a huge  
371 number of intermediates and by-products, and these additional compounds compete with the pollutant  
372 molecules to react with the same amount of •OH radicals, thus decreasing the removal efficiency of the process.  
373 It is worth pointing out that the pattern of TOC removal was found to be entirely different from that observed  
374 in CBR degradation. In the mineralization experiments, the removal efficiency was found to be higher for the  
375 test with higher initial CBR concentration. The mineralization phenomenon is boosted in the presence of higher  
376 organic load, diminishing the extent/magnitude of parasitic reactions. Based on the results obtained in this  
377 study, it is clear that the *B-UNCD<sub>WS</sub>/TDNT/Ti* electrode has proven to be highly efficient when applied for the  
378 removal of different concentrations of CBR. Regarding CBR mineralization, the application of the proposed  
379 electrode was found to require longer treatment times to obtain satisfactory results; still, the TOC removal  
380 rates of 52.3– 65.5 % obtained in 60 min of treatment are found to be reasonable considering that this is the  
381 first time the proposed electrode has been employed for CBR degradation. The encouraging results obtained  
382 in this study (based on the application of the proposed electrode for CBR removal) can be most likely attained  
383 when the proposed technique is applied for the treatment of other recalcitrant water pollutants.

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387 **Fig 6.** (a) Carbaryl degradation over time and (b) mineralization after 60 min treatment of real water with  
 388 different CBR concentrations at current density of  $75 \text{ mA cm}^{-2}$ .

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#### 4. Conclusions

The present work reported the synthesis of B-UNCD<sub>ws</sub>/TDNT/Ti electrodes with extremely thin diamond films using an innovative methodology without seeding substrate pre-treatment and their successful application for the treatment of water containing recalcitrant compounds. The material proposed in this study was found to possess suitable electrochemical properties, including highly porous ultranano-structures, improved specific capacitance (274  $\mu\text{F cm}^{-2}$ ) and high onset potential for water discharge (ca. 2.4 V vs. Ag/AgCl); these properties favored the generation of reactive oxygen species during the electrolysis process. Owing to the combination of the aforementioned properties, the application of the proposed electrode at the current density of 75 mA cm<sup>-2</sup> contributed effectively toward the complete removal of CBR in synthetic medium in 30 min ( $Q=0.5 \text{ Ah L}^{-1}$ ) with electric energy consumption per order of 4.01 kWh m<sup>-3</sup> order<sup>-1</sup>. The use of scavengers in the treatment process helped confirm that  $\bullet\text{OH}$  was the main oxidant species (with effective contribution of  $\approx 84.7\%$ ) that took part in the degradation of the pollutant. The results obtained from the analysis of the final by-products of the electrolysis pointed to the presence of carboxylic acids, including acetic, formic, fumaric and oxalic acids, but zero or minimal concentrations of these acids were detected at the end of the electrochemical treatment. The concentrations of nitrogenated species monitored over the treatment period were found to be within the maximum contamination level for drinking water; this evidently helps reduce the health risks posed by the presence of these substances in water. The results obtained from the application of the proposed electrode for the removal of CBR in real effluents were found to be satisfactory; complete degradation was obtained within 20-60 min treatment of effluents containing 5 – 20 mg L<sup>-1</sup> of CBR while TOC removal rates of 52.3– 65.5 % were obtained after 60 min of treatment. This work highlights the advantages of improving the synthesis of BDD electrode and its contribution toward enhancing the effectiveness and competitiveness of electrochemical advanced oxidation processes when applied for the degradation of recalcitrant pollutants.

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