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# Highly coherent phase-lock of an 8.1 $\mu\text{m}$ quantum cascade laser to a turn-key mid-IR frequency comb

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A continuous-wave Fabry-Perot quantum cascade laser (QCL) emitting at 8.1  $\mu\text{m}$  operating in single mode regime has been coherently phase locked to a turn-key low-noise commercial mid-Infrared (mid-IR) optical frequency comb. The stability of the comb used as a reference is transferred to the QCL resulting in an integrated residual phase error of 0.4 rad. The laser linewidth is narrowed by more than two orders of magnitude reaching 300 Hz at 1ms observation time, limited by the spectral purity of the mid-IR comb. Our experiment is an important step towards the development of both powerful and metrology-grade QCLs as well as fully-stabilized QCL frequency comb, and opens perspectives for precision measurements and frequency metrology in the mid-IR.

## 1. Introduction

High-spectral-purity narrow-linewidth continuous-wave (cw) lasers are crucial for both fundamental research and technological applications in many fields of science, such as atomic, molecular, quantum and optical physics. They play in particular a major role in precision measurement physics, in the development of quantum technologies, and in time and frequency metrology. For these applications, the free-running linewidth determined by the laser short-term stability is often not adequate and active frequency stabilization is required. In the near-infrared and visible domain, this is routinely achieved by locking the laser to the resonance of a high-finesse Fabry-Perot cavity, or to a narrow atomic or molecular resonance.

Frequency-stabilized sources in the mid-infrared (mid-IR, from 3 to 20  $\mu\text{m}$ ) domain are also needed, in particular for conducting ultra-high resolution molecular spectroscopy measurements in the so-called molecular fingerprint region with far-reaching applications ranging from fundamental physics<sup>1-6</sup> and metrology<sup>7-9</sup> to astrophysics, remote sensing and Earth sciences<sup>10,11</sup>. Quantum cascade lasers (QCLs) are a robust technology that cover the mid-IR spectrum, offer wide tuning capabilities and have cw output powers as high as several watts but QCLs show substantial frequency fluctuations<sup>12-19</sup>. Phase/frequency stabilized QCLs have been demonstrated<sup>20</sup>, either by phase-locking to a CO<sub>2</sub> laser<sup>21,22</sup>, frequency locking to a sub-Doppler molecular transition<sup>23</sup>, optical injection locking<sup>24</sup> or phase-locking to an optical frequency comb, either calibrated to a commercial Rb frequency standard or H-Maser steered to a global navigation satellite system (GNSS)<sup>18,19,25-29</sup>, or stabilized to a near-infrared metrology-grade frequency reference traceable to primary frequency standards<sup>30-32</sup>. References<sup>31,32</sup> report

ultimate sub-Hz stabilities and accuracies, and linewidth narrowing down to the 0.1 Hz level. Locking to a frequency comb typically necessitates sophisticated non-linear optical setups requiring very delicate alignment procedures, and often penalizing the QCL output power, most of it being required for generating non-linear signals.

In this Letter, we measure the free-running frequency noise power spectral density of an 8.1  $\mu\text{m}$  Fabry-Perot QCL operating in single mode regime and demonstrate coherent phase locking of this source to a tooth of a commercially available low-noise mid-IR optical frequency comb synthesizer (OFCS), by processing a beat-note signal generated directly in a mid-IR photodetector. This allows the spectral performances of the OFCS to be transferred to the QCL without the need to pass the QCL beam through a complex dedicated non-linear optical setup, thus allowing less than 1% of its optical power to be used for locking, keeping most of it at disposal for further experiments. Locking to such a low-noise comb results in a linewidth narrowing of the QCL by a factor of 250, from  $\sim 100$  kHz down to the few hundreds of hertz level. This corresponds to a 2 orders of magnitude linewidth improvement compared to reference<sup>25</sup> that reports phase locking of a distributed feedback QCL to a home-built mid-IR comb. Locking the OFCS to a remote near-infrared ultra-stable frequency reference traceable to the atomic fountain clocks of the French metrology institute, as demonstrated in reference<sup>31,32</sup> will eventually provide a both powerful and metrology-grade QCL to be used in different applications such as high precision spectroscopy, quantum optics measurements or LIDAR (light detection and ranging).

## 2. Experiment

The experimental setup is shown in Fig. 1(a). A turn-key offset-free mid-IR OFCS from Menlo Systems, spanning the 7.4 to 9.4  $\mu\text{m}$  spectral window (full-width-half-maximum FWHM  $\sim 4.29$  THz), is used as an optical reference. The mid-infrared comb is generated by difference frequency mixing in a non-linear crystal between a low noise 1.5  $\mu\text{m}$  Erbium doped fiber frequency comb and its extension in a wavelength shifting fiber towards the 1.8  $\mu\text{m}$  window. The mid-IR comb delivers an average output power of 2.2 mW, resulting in tens of nanoWatts comb modes. The comb repetition rate,  $f_{\text{rep}} = 100$  MHz, is stabilized against a radio-frequency (RF) synthesizer using the electronic control unit of the comb. This corrects the slow frequency drift without affecting the laser linewidth. The QCL is a Fabry-Perot source grown and processed at ETH Zürich (more details about this laser are given in the supplementary material). It is typically operated close to threshold at a temperature of 263 K (threshold current is 400 mA), and delivers up to 45 mW in a continuous wave single mode oscillating at a wavelength of  $\sim 8.16$   $\mu\text{m}$ . Fig. 1(b) shows the optical spectrum of the mid-IR comb that overlaps with the single longitudinal mode of the QCL. The QCL and the mid-IR-OFCS beams are superimposed by means of a 70/30 germanium beam splitter. Both beam splitter outputs are optically filtered with a 50 GHz resolution monochromator, and focused onto an 800-MHz bandwidth

mercury-cadmium-telluride (MCT) detector (VIGO System PVI-4TE-10.6) (see supplementary material). The QCL beam is attenuated and a total power of about only 100  $\mu\text{W}$  is hitting the detector. The resulting beat-note signals obtained on detector 1 and 2 in Fig. 1(a) oscillate at:

$$f_{\text{beat}} = \nu_{\text{QCL}} - n \times f_{\text{rep}}$$

with  $\nu_{\text{QCL}}$  the QCL frequency and  $n \sim 370\,000$  the tooth number of the mid-IR-OFCS. Note that in our case the carrier-envelope offset  $f_{\text{CEO}} = 0$ , as the mid-IR comb is generated by frequency difference. Fig. 1(c) shows the RF spectrum of the signal measured at the output of detector 1 when the QCL operates in a free-running regime. Four main peaks emerge from the noise between DC and 150 MHz: the beat-note signal between the QCL mode and the nearest comb tooth at  $f_{\text{beat}} \simeq 23$  MHz, a peak at the comb repetition rate of 100 MHz, and the beat-note signals between the QCL mode and the second- and third-nearest comb teeth at  $f_{\text{rep}} \pm f_{\text{beat}}$  ( $\simeq 77$  MHz and  $\simeq 123$  MHz). The OFC/QCL beat signals are observed with a signal-to-noise ratio (carrier power to phase noise power density ratio) of  $\text{SNR} = 26$  dB at 1 MHz resolution bandwidth and are processed to either measure the frequency noise of the free-running QCL, or for phase-locking it to the OFCS. To characterize the residual phase fluctuations of the locked QCL, a second out-of-loop detector (detector 2) is used.

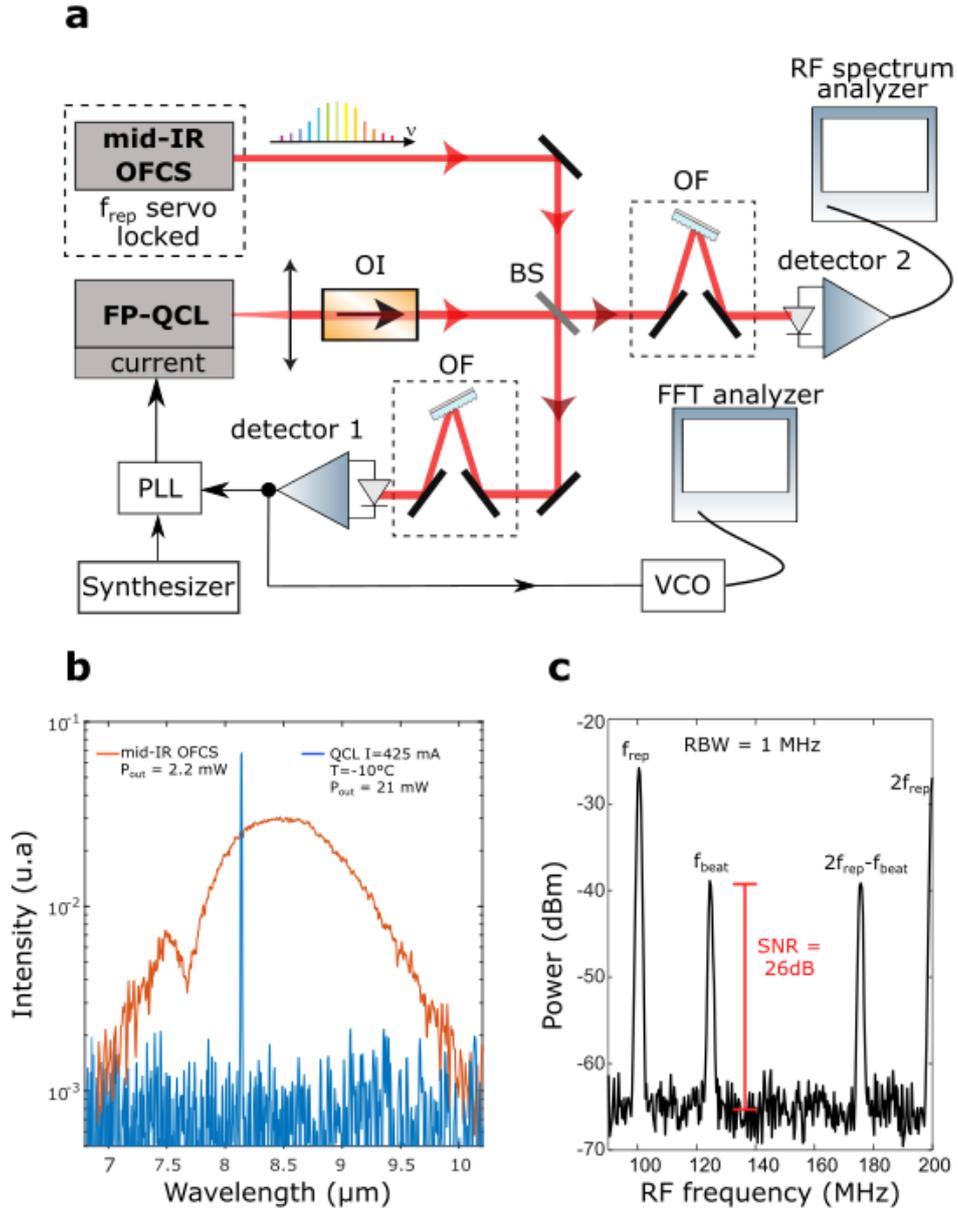


FIG. 1. (a) Experimental setup for measuring the frequency noise of the free-running QCL and for coherently phase-locking it to a low-noise mid-IR OFCS. FP-QCL, Fabry-Perot Quantum Cascade Laser; mid-IR OFCS, mid-infrared-optical frequency comb synthesizer; BS, beam splitter; OF, optical filtering monochromator build from a diffractive grating with 150 grooves/mm; PLL, phase lock loop; OI, optical isolator; VCO, voltage controlled oscillator; FFT, fast Fourier transform (b) Optical spectra of the FP-QCL and the mid-IR OFCS recorded with a 2 GHz resolution optical spectrum analyzer (the modes of the 100 MHz repetition rate OFCS are not resolved). (c) RF spectrum of the beat signal between the mid-IR OFCS and the free running QCL (1 MHz resolution bandwidth, RBW).

### 3. Free-running Fabry-Perot QCL frequency noise

The frequency noise power spectral density (FNPSD) of the free-running QCL is derived from the beat-note signal  $f_{\text{beat}} + f_{\text{rep}}$  measured on detector 1, in open-loop configuration. The latter is fine tuned to 140MHz with the QCL current

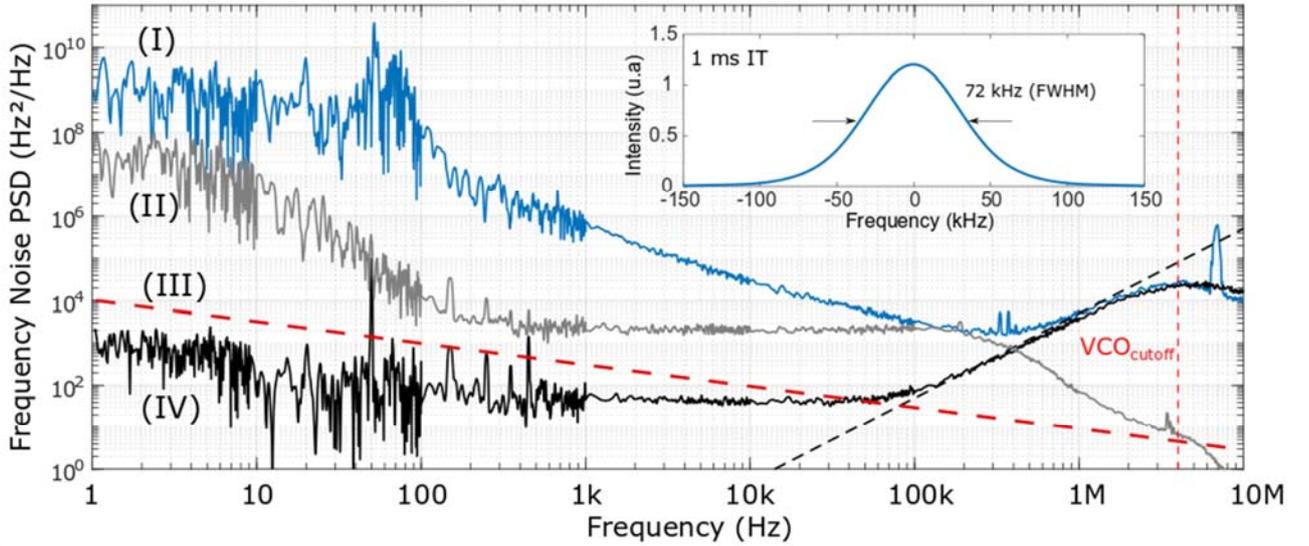
( $\Delta v_{\text{QCL}}/\Delta I = -235\text{MHz/mA}$ ) to match the frequency range of a tracking oscillator consisting of a voltage-controlled oscillator (VCO) phase-locked to the 140 MHz beat-note signal. The VCO tuning voltage then mirrors the beat-note signal's frequency noise and thus the free-running QCL frequency noise for Fourier frequencies below the system bandwidth of  $\sim 4$  MHz. To keep the beat signal frequency within the tracking range, slow drifts of the free-running QCL (few MHz/s) produced by thermal and mechanical fluctuations have to be eliminated. This is achieved by implementing a slow feedback loop (sub-Hz bandwidth) on the QCL current to keep the beat-note at 140 MHz. The power spectrum of the VCO tuning voltage is then measured using a fast Fourier transform (FFT) analyzer, and the FNPSD of the QCL is finally derived using the 4 MHz/V VCO voltage-to-frequency conversion factor.

Fig. 2(a) shows the resulting FNPSD of the free-running QCL/mid-IR comb beat-note signal (blue line (I)). It has a  $1/f$  trend at low frequency up to  $\sim 300$  kHz. Above 300 kHz, the frequency noise increases up to approximately 4 MHz, beyond which we observe a decrease due to the finite tracking oscillator bandwidth. The increase of the frequency-noise above 300 kHz is the consequence of the finite beat-note signal-to-noise ratio of 86 dB/Hz, limited by our detector background noise (see supplementary material). The corresponding white phase noise around the optical carrier gives rise to a double-sided contribution of  $(2/\text{SNR}_{1\text{Hz}}) \times f^2$  in our FNPSD measurement, with  $\text{SNR}_{1\text{Hz}}$  the SNR in a 1 Hz bandwidth. To validate this, the black curve (IV) in Fig. 2(a) shows the FNPSD obtained by blocking the mid-IR-OFCS beam and by replacing  $f_{\text{beat}}$  with a low phase noise artificial signal yielding the same  $\text{SNR}_{1\text{Hz}}$  generated by modulating the QCL current with a RF generator. The flat plateau in the range 1 Hz-100 kHz is due to the FFT-analyzer background noise, and above 100-kHz the effect of the SNR can be seen as it matches the blue curve (I). The grey line (II) in Fig. 2(a) shows the contribution of the low-noise current source, obtained by multiplying the measured driver's current noise spectrum ( $\sim 300$  pA/Hz<sup>1/2</sup> above 100Hz) by the laser DC current-to-frequency response ( $-235$  MHz/mA). Finally, the red dashed line (III) in Fig. 2(a) gives the contribution from the OFCS tooth frequency noise to the heterodyne signal. The FNPSD of this tooth at frequency  $n \times f_{\text{rep}}$  is determined from typical noise measurements of the repetition rate of the OFCS 1.55  $\mu\text{m}$  main oscillator provided by Menlo Systems. Note that this estimation does not consider the frequency noise that could be added by non-linear processes involved in the generation of the mid-IR OFCS which is assumed to be negligible.

For Fourier frequencies below 300 kHz, the blue curve (I) in Fig. 2(a) corresponds to the free-running QCL FNPSD, all other contributions being negligible. The level of frequency noise measured is similar to that reported in ref<sup>17</sup>, another measurement carried out on a Fabry-Perot QCL. Yet, the expected white frequency noise level corresponding to the QCL Schawlow-Townes limit does not seem to be reached above 300 kHz due to our SNR value. However, an upper limit of  $10^3$  Hz<sup>2</sup>/Hz (and a corresponding upper limit of  $\sim 3$  kHz on the intrinsic laser linewidth) can be inferred. The free-running QCL emission line

shape is calculated from the measured FNPSD for a 1 ms integration time (IT) following<sup>33</sup> and shows a FWHM  $\Delta\nu_{\text{QCL}} \sim 72$  kHz (see Fig. 2(a) inset). A similar calculation based on curve (III) in Fig. 2(a) leads to a linewidth  $\Delta\nu_{\text{OFCS}} = 300$  Hz (1ms IT) for the OFCS tooth, once again confirming the negligible contribution of the OFCS noise in our measurement. Fig. 2(b) shows the evolution of  $\Delta\nu_{\text{QCL}}$  calculated for different integration times. It decreases with decreasing integration time and reaches a minimum of 15 kHz at 200  $\mu\text{s}$  IT. For the shortest integration times ( $< 100 \mu\text{s}$ ), the linewidth is Fourier limited: the contribution from the frequency noise is lower than the Fourier uncertainty.

**a**



**b**

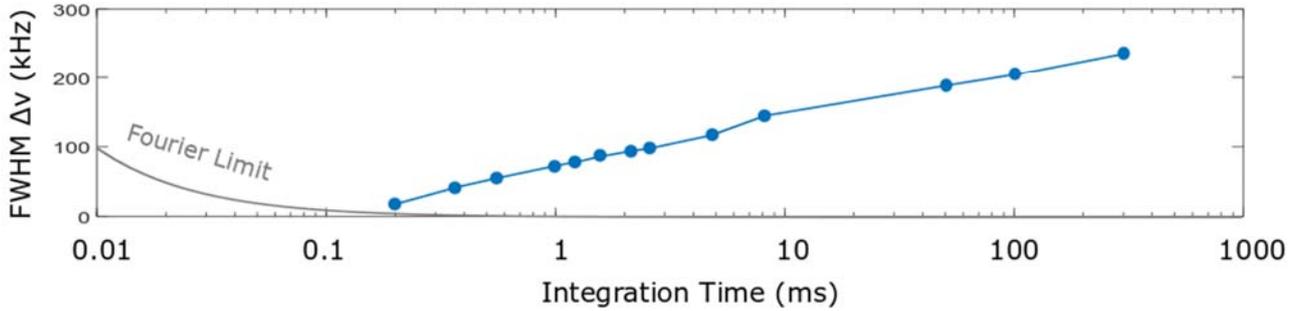


FIG. 2. (a) Frequency noise power spectral density (FNPSD) of the free-running 8.1  $\mu\text{m}$  QCL/mid-IR comb beat-note signal (blue line (I)). The contributions from the laser driver current noise (grey line (II)) and from the mid-IR OFCS tooth contributing to the beat-note signal (red dashed line (III)) are also plotted for comparison. The black line (IV) corresponds to our noise floor, see text (with the black dashed line corresponding to the contribution from the limited beat-note signal-to-noise ratio of 86 dB/Hz). The tracking oscillator bandwidth is also shown (vertical red dashed line). The inset shows the free-running QCL emission line shape calculated from the measured FNPSD (I) for a 1 ms integration time (IT). (b) Blue line: free-running QCL FWHM emission line width as a function of integration time calculated from FNPSD (I) (the slight excess of noise of technical origin visible on curve (I) between 40 Hz and 100 Hz has been purposely removed for this calculation); the grey line corresponds to the Fourier limit resulting from the resolution bandwidth.

#### 4. Fabry-Perot QCL phase locking and linewidth narrowing

As illustrated in Fig. 1(a), to coherently phase-lock the QCL to a tooth of the mid-IR-OFCS, a phase-error signal is generated by comparing the phase of the filtered and amplified beat signal with a reference signal typically at 140 MHz from a synthesizer (Zurich Instrument UHFLI). A phase-lock servo loop is used to apply a correction signal directly to the QCL's current. Note that much less than 1% of the QCL power ( $<100\mu\text{W}$ ) is used for locking, keeping most of it at disposal for different experiments

In closed-loop operation, a significant narrowing of the beat-note signal linewidth is observed and a maximum signal-to-noise ratio of about 55 dB at 1 kHz resolution-bandwidth was obtained, as shown in the inset of Fig. 3. The beat signal spectrum is recorded on a RF spectrum analyzer after detection with a second out-of-loop photodetector (detector 2 in Fig. 1(a)), similar to the one in-loop, in order to avoid errors brought by the detection setup and associated electronics. A  $\sim 250$  kHz phase-lock feedback bandwidth can be inferred from the spectral shape. Figure 3 shows the measured phase noise PSD of the beat signal between the Mid-IR-OFCS and the phase locked QCL. The latter is generated by comparing the phase of the beat signal at the output of detector 2 with a synthesized reference signal at 140 MHz (UHFLI Zurich Instrument) and processed with a FFT spectrum analyzer. A 0.39-rad rms residual phase noise is obtained in a 1 Hz to 1 MHz integration bandwidth, indicating that more than 85% of the power is concentrated in the coherent carrier of the beat signal <sup>34</sup>.

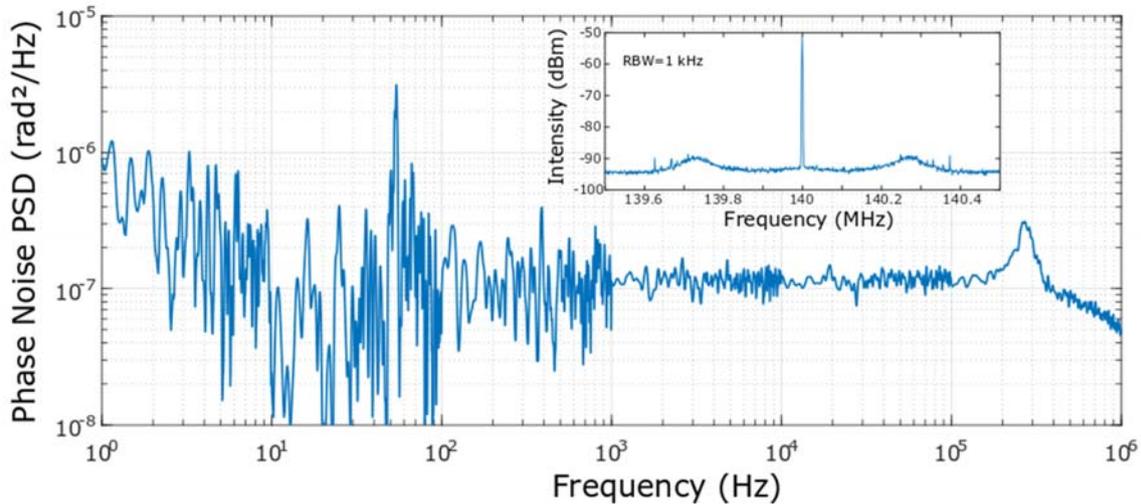


FIG. 3. Phase-noise power spectral density (PSD) of the beat signal between the phase-locked QCL and the mid-IR comb. Inset: Beat signal spectrum between the mid-IR OFC and the phase-locked QCL taken with a RF spectrum analyzer (1 kHz resolution bandwidth, RBW).

This is the signature of a highly coherent phase-lock and of the very good transfer of the mid-IR OFCS spectral features to the QCL. Therefore, this results in a QCL linewidth ultimately set by the mid-IR comb tooth linewidth. Exploiting the OFCS FNPSD displayed in Fig.2 (dashed red line (III)), we calculate a linewidth of respectively  $\sim 300$  Hz (see above) and  $\sim 800$  Hz

at 1 ms and 100 ms integration time, which is 2 to 3 orders of magnitude lower than in the free-running regime. Our phase-locked Fabry-Perot QCL shows a 2 orders of magnitude narrower linewidth compared to a similar work using a 8.6  $\mu\text{m}$  DFB QCL phase-locked to a home-built 250 MHz mid-IR comb<sup>25</sup>.

## 5. Conclusion

We characterized the frequency noise of an 8.1  $\mu\text{m}$  free-running Fabry-Perot QCL operating in single mode regime. It was then phase-locked to a low-noise commercial mid-infrared comb, itself generated from a near-infrared comb. We achieved a QCL linewidth reduction from  $\sim 100$  kHz to the few 100 Hz level, limited by the linewidth of the mid-IR comb used as a reference, improving on previous studies. Locking the comb to an ultra-stable frequency reference calibrated to the primary frequency standards of the French metrology institute<sup>31,32</sup> will eventually result in ultimate sub-Hz stabilities, accuracies and linewidths. One advantage of our method lies on the generation of a beat-note signal directly in the mid-IR without the need to pass the QCL beam through a sophisticated non-linear optical setup. As a result, much less than 1% of the QCL optical power is used for locking, allowing almost all of the QCL power to be exploited. We obtain a QCL that is both powerful and highly stable – potentially ultra-stable – to be exploited in a range of applications from fundamental research in quantum optics and high-resolution spectroscopy to quantum technologies or LiDAR. When driven at higher currents, our Fabry-Perot QCL operates in optical-frequency-comb regime (see supplementary materials). Our work thus also paves the way toward the development of powerful and fully stabilized metrology-grade QCL frequency combs.

## SUPPLEMENTARY MATERIAL

See [Supplementary material](#) for supporting content.

## ACKNOWLEDGMENTS

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